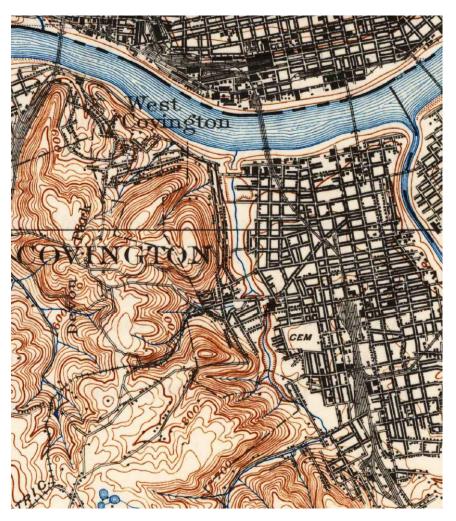
Willow Run Storm Water Separation Feasibility Study Report

I-71/I-75 (BRENT SPENCE BRIDGE PROJECT)

Kenton County, KY MP 188.6 to MP 191.4 Item No. 6-17.00



PREPARED BY:

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MARCH, 2022

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Project Scope and Background

The Willow Run watershed is the largest watershed in Sanitation District 1's (SD1) system. It drains 1,871 acres, discharges into the Ohio River, and the combined sewer system accounts for 33% of SD1's total system flow. During times of wet weather, it overflows and discharges untreated sewerage into the river and into neighborhood parks, streams and creeks. The EPA, through a consent decree, has mandated that the overflows be reduced or eliminated in the watershed.

According to SD1, there are 7 low-flow diversions in the Willow Run combined sewer. During dry weather, these divert combined flow into a parallel sanitary interceptor sewer. Flows are then carried, via gravity, to the treatment plant. During wet weather, when the flow exceeds the capacity of the diversions, a portion of the flow overtops the diversions and overflows directly into the Ohio River. Generally it takes about a $\frac{1}{2}$ " rain in the Willow Run watershed to trigger an overflow event.

During normal Ohio River levels, the Willow Run combined sewer outfall drains into the river by gravity. During high Ohio River levels (exceeding a gage height of 38 feet) the following occurs:

- 1. The Ohio River water backs up into the combined system, flows over the diversions and gets into the interceptor sewer.
- 2. A gage height of 40 feet is considered "action stage" according to the USGS National Water Dashboard.
- 3. At a gage height of 43.5 feet, the flow backs out of the Willow Run combined sewer into Goebel Park.
- 4. At a gage height of 45.9', the pumps are turned on to pump the combined system over the levee and back into the river. A 12'X12' sluice gate is lowered at this point.
- 5. A gage height of 52 feet is considered "minor flood stage" according to the USGS National Water Dashboard.

The boundary of the Willow Run watershed is located along Kyles Lane at its interchange with I-71/I-75. Therefore, all runoff from the I-71/I-75 corridor, between the Kyles Lane interchange and the Ohio River currently drains into the Willow Run combined sewer system at various points. The proposed widening of the corridor will increase runoff by increasing the impervious area in the watershed. The existing combined sewer system appears to already be experiencing problems with capacity according the City of Covington.

In a letter dated January 5, 2022 from the Covington's Mayor Meyer to Kentucky Transportation Cabinet (KYTC) Secretary Jim Gray, the City requested that KYTC resolve the storm water runoff capacity issues. It should be noted that the City has reassumed storm water responsibility from SD1. They are responsible for storm water runoff until it reaches the combined sewer system, at which point it becomes the responsibility of SD1. In that letter, the City mentioned the following specific problem areas with the existing system:

• Excessive runoff from the interstate corridor to Highland Avenue

- Flooding in Lewisburg at the end of Laurel Street
- Street and basement flooding along Euclid Avenue.

The City requested the following measures in their letter:

- Ensure the City is engaged and a part of storm water and water quality planning
- Separate the storm water from the Willow Run combined sewer system north of 16th Street
- Expand storm water removal capacity to eliminate backups on Euclid Avenue
- Improve maintenance of all storm water drains and detention areas along the interstate corridor to prevent clogging from debris.

To address the City's concerns, KYTC tasked Palmer Engineering with studying options for separating storm water runoff in the I-71/I-75 corridor within the Willow Run watershed.

Goals

Palmer's goal was to develop a feasibility study for separating interstate corridor storm water flow within the Willow Run watershed from the combined sewer system. During scoping discussions with KYTC, the project team decided to study two proposed alternatives – one which specifically addressed the City's request to separate storm water flow from the combined sewer system from 16th Street to the Ohio River, and another which went beyond their request and provided a separate storm water system from Kyles Lane to the Ohio River.

Palmer was provided files from the original preliminary drainage layout done by others, completed in approximately 2010 during the environmental assessment. These files included PDFs of the drainage layout, CADD files for the corridor, and InRoads data files. At that time, the designers did not have a goal of separating all of the corridor's storm water flow from the combined system. Their goal was to evaluate options that could achieve a net-zero effect, or better, for the storm water runoff that reached the combined system. After reviewing all of the files, Palmer determined that it would be best to start from scratch with the proposed drainage layouts to achieve the goals of this study.

Proposed Alternatives

See Appendix A and B for plan views of each proposed alternative discussed below. The following should be noted about the layout of the proposed alternatives:

- Inlets were placed using the proposed DTMs and cross sections that were provided. They account for crest and sag locations, superelevation transitions, barrier wall and retaining wall locations, and bridge locations.
- Spread calculations were not performed for each inlet location. But, some general spread calculations were used to determine if pipe length would control inlet spacing or if spread would control
- Bridge deck drains were not laid out, but bridge deck runoff was accounted for in the storm sewer system at ground level below the bridges.

• Bridge pier locations are not known at this time. They could impact the location of the proposed storm sewer or relocated existing sewers during final design.

Alternative 1

The goal of Alternative 1 was to separate the corridor's storm water runoff from the combined system from 16th Street to the Ohio River. The proposed storm sewer trunk line begins at Lt. Sta. 526+00, crosses the interstate at a sag point near Sta. 530+50, and then continues northward generally under the proposed Jillians Way pavement. Branch connections at each side road attempt to separate as much storm water runoff from the side streets as possible within the footprint of the side road reconstruction.

There are a couple of areas where the depth of the proposed Alt 1 trunk line was critical. At 9th Street, the proposed storm sewer trunk line crosses the existing 96" combined sewer just upstream from where the existing sewer joins with the 120" Willow Run trunk line. SD1's GIS data was used to check the elevations of the existing line versus the proposed. The elevation of this crossing prevented the proposed Alt 1 system from being able intercept a low area approximately 1 acre is size in the vicinity of the 12th Street and Bullock Street intersection. Intercepting the storm water runoff in this area would have pushed the proposed Alt 1 system too low and created a conflict at the crossing.

Goebel Park is also a low area where the existing combined system backs up and floods during high water events on the Ohio River. The proposed Alt 1 system was able to be raised by taking advantage of the higher Jillians Way grade, where it is being built up with a retaining wall.

There are segments of the existing Willow Run system that will require relocation due to the proposed roadway construction. These are also shown schematically in the proposed exhibits. One area is from Rt. Sta. 530+00 to Rt. Sta. 546+00, where the existing Willow Run trunk line is proposed to be relocated adjacent to the proposed Alt 1 storm sewer trunk line. Another is from Lt. Sta. 524+00 to Lt. Sta. 544+00, where a significant existing branch line to the Willow Run system is proposed to be relocated along Bullock Street. And, as the project nears the Ohio River, the existing Willow Run trunk line and the low-flow diversion sanitary sewer is proposed to be relocated north of Rt. Sta. 561+00.

The proposed Alt 1 trunk line and the relocated Willow Run system are proposed to tie back into the existing system at, or just upstream from, the existing pump station. Alt 1 does not propose a new pump station or new outfall to the Ohio River. Rather, it would utilize the existing system from the existing outfall/pump station to the river. Modifications to the pump station itself may be needed.

Alternative 2

The goal of Alternative 2 was to separate the corridor's storm water runoff from the combined system from Kyles Lane to the Ohio River. The proposed storm sewer trunk line begins at Lt. Sta. 449+00, crosses to the right side of the interstate at Rt. Sta. 453+00, continues along the right side of the interstate until crossing to the left side at Sta. 466+00, and then remains on the left side until joining with the beginning of the proposed layout of Alternative 1.

There is an existing 42" pipe that crosses the interstate near Sta. 456+50. This pipe conveys offsite drainage which eventually ends up in a detention basin near Rt. Sta. 470+00. This pipe is proposed to remain in service and the offset drainage is not proposed to be intercepted. The proposed Alt 2 trunk line avoided impacting this pipe by going around it to the right side.

There are 5 existing detention basins along the corridor for Alt 2.

- Rt. Sta. 470+00 The outlet for this basin drains away from the interstate. Alt 2 reduces the flow that reaches the basin by intercepting some storm runoff that currently reaches it.
- Lt. Sta. 477+00 The outlet for this basin drains into the left roadside ditch for the interstate. There is an existing pipe crossing the interstate that currently conveys the left roadside ditch across the interstate just upstream from where the basin outlets into the left roadside ditch. Alt 2 captures the outlet flow from the basin, and captures the upstream roadside ditch flow described above. This eliminates the existing pipe crossing, and thus reduces the flow that reaches the problematic Highland Avenue area.
- Lt. Sta. 490+00 The outlet for this basin drains into the left roadside ditch for the interstate. Alt 2 captures the outlet flow from the basin.
- Lt. Sta. 518+00 The outlet for this basin is a junction where existing sanitary and storm flow join, beginning a combined sewer line. Alt 2 proposes to separate the storm water flow, and create a new storm-only outlet structure for the basin. This will reduce the flow that enters into the combined sewer system.
- Rt. Sta. 520+00 This basin captures runoff from the right interstate roadside ditch and cut area, along with runoff from St. Elizabeth Covington Hospital. The outlet for this basin drains away from the interstate and toward the problematic Euclid Avenue area. Alt 2 proposes to capture the interstate roadside ditch before it reaches the basin, thereby reducing flows that eventually reach the Euclid Avenue area.

The details of the detention basin outlet flows are not known at this time, and proposed outlet flows were assumed for this study. Detailed design of the basins during final design could affect downstream pipe sizes. Each basin that is impacted by the roadway widening is being modified by the roadway team to replace any lost volume. The proposed outflow from the basins along the left side of the interstate will not be as critical to control, since they will all flow into the proposed separate storm sewer. The proposed outflow from the basins on the right side of the interstate will each be reduced by the proposed storm sewer system intercepting some of the runoff that currently reaches the existing basins.

Downstream from the detention basin at Lt. Sta. 518+00, the layout of Alt 2 is the same as Alt 1 except for pipe sizes along the trunk line.

At the Project Team's Alternative Review Meeting on February 21, 2022, KYTC decided that Alternative 2 was the preferred option. Alt 2 would be advanced with a cost estimate, a summary of drainage areas separated from the Willow Run combined sewer, and presented to the City of Covington and SD1. The project team presented Alt 2 to local officials including the City of Covington and SD1 on March 3, 2022. See Appendix D for documentation of all pertinent meetings.

Alternative 2 separates a total of 467 acres (25% of the total Willow Run watershed area) from the existing Willow Run combined sewer system. This area is comprised of 170 acres of impervious area and 297 acres of pervious area.

The preliminary cost of Alternate 2 is estimated to be \$15.1 million. This includes the estimated cost for relocated portions of the existing Willow Run combined sewer and its low-flow diversion line, along with some connections to each. The preliminary estimate does not include a cost for potential modifications to the existing pump station.

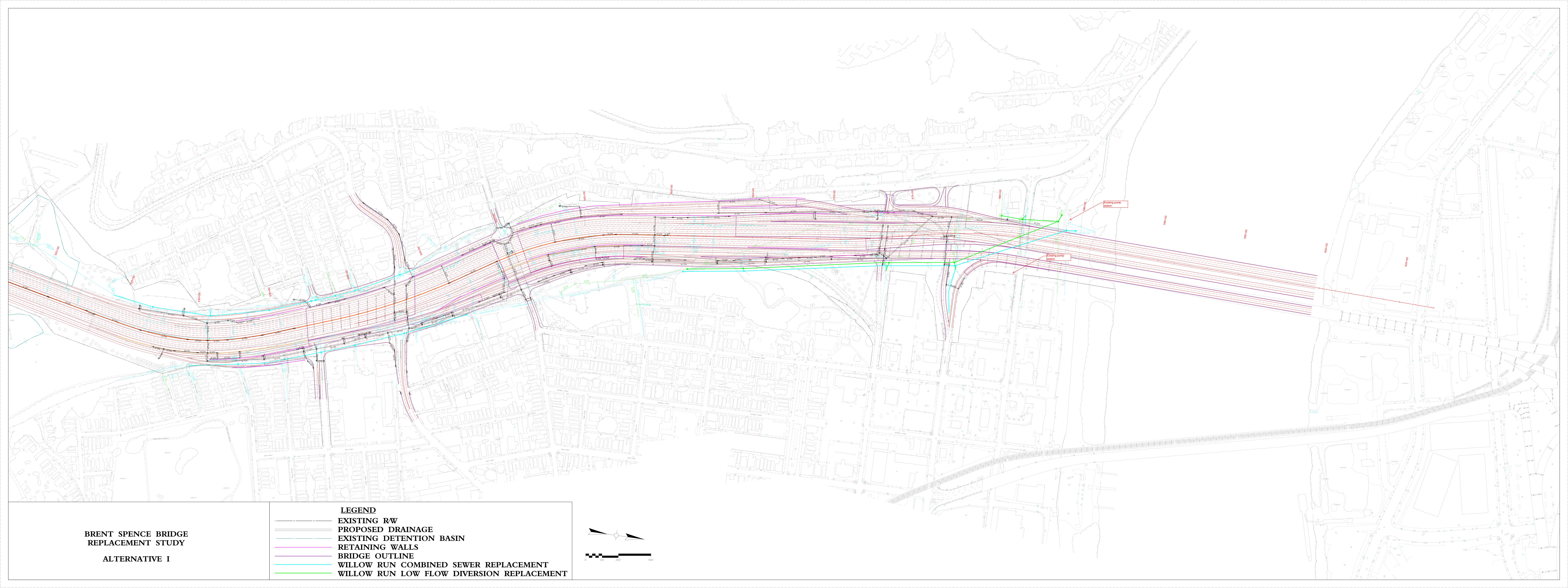
Pump Station

The existing pump station is planned to remain in service with the proposed Alternative 2. See Appendix C for record plans for the pump station. The relocated Willow Run combined sewer and the proposed separated Alt 2 storm sewer are proposed to connect to the existing outfall/pump station system just upstream from the pump station. The general operation of the pump station is not proposed to change, but the pumps will need to be evaluated to determine if modifications are needed in the proposed condition. The total area of watershed that drains to the pump station will not change in the proposed condition versus the existing condition. However, the flow rate could change due to increased impervious area, changes to the operation of the detention ponds, or the timing of runoff reaching the pump station.

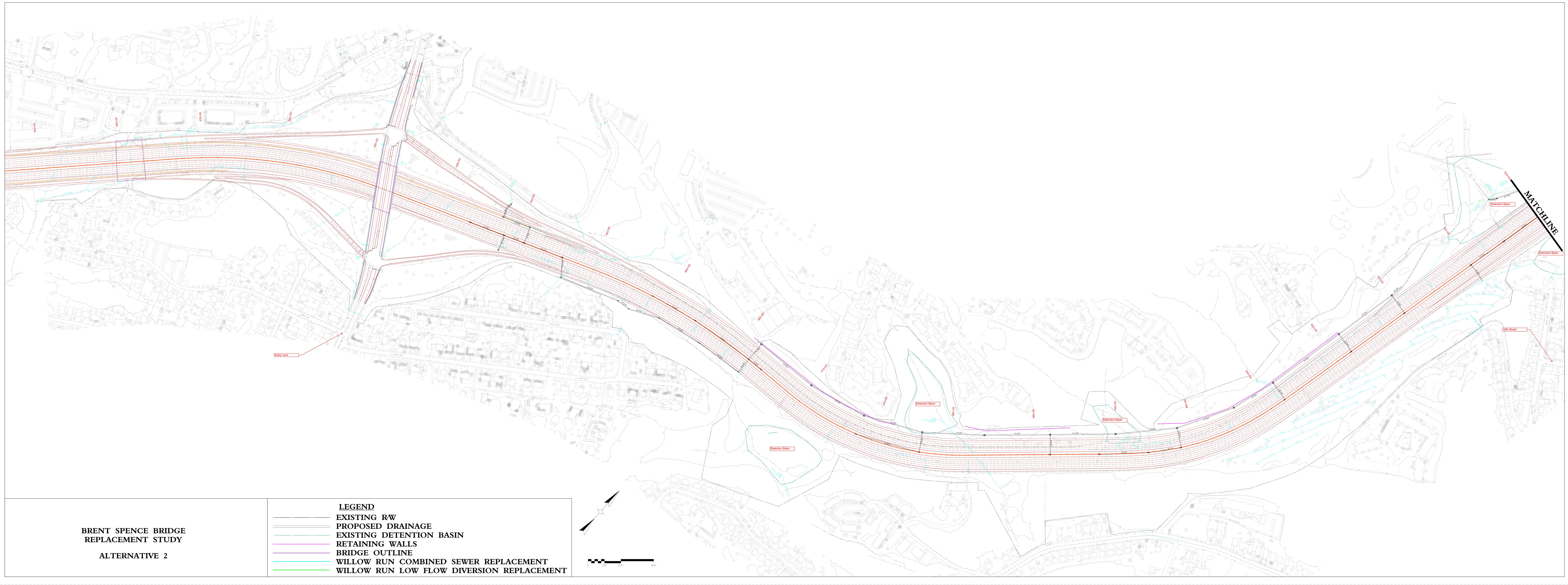
This was discussed with SD1 at the project team's Local Officials Meeting (See Appendix D), and SD1 requested the proposed Alt 2 layout for the purpose of evaluating its impact in their system's hydrologic and hydraulic model. The project team will continue to coordinate with SD1 to determine if the changes to their model indicate a need to modify the pumps at the pump station. An addendum to this report will be submitted upon the conclusion of that coordination.

The project team also met with the U.S. Army Corps of Engineers and the City of Covington on March 17, 2022 to discuss the Section 408 permitting process. The Corps advised the project team about what items would be required for the Section 408 permit and the review time to expect. It was also recommended that the selected design-build team should continue to coordinate with the City of Covington and SD1 regarding the flood control system. The levee, floodwall, and pump station system are owned by the City of Covington, and they are operated and maintained by SD1.





Alternative 2 Plan, Cost, and Drainage Area Summary





PRELIMINARY COST ESTIMATE

CONSTRUCTION

Road Name:I-71/I-75From:16th Street

To: Ohio River

Willow Run Storm Water Separation - ALT 2

ITEM NO.	ITEM	QUANTITIES	UNIT	UNIT PRICE	COST
		DRAINAGE			
522	18" STORM SEWER PIPE	15100	LF	\$54	\$815,40
524	24" STORM SEWER PIPE	2788	LF	\$85	\$236,98
526	30" STORM SEWER PIPE	1138	LF	\$98	\$111,52
528	36" STORM SEWER PIPE		LF	\$122	\$
529	42" STORM SEWER PIPE		LF	\$135	\$
530	48" STORM SEWER PIPE	947	LF	\$163	\$154,36
531	54" STORM SEWER PIPE	4370	LF	\$175	\$764,75
532	60" STORM SEWER PIPE	1263	LF	\$215	\$271,54
533	66" STORM SEWER PIPE	2055	LF	\$230	\$472 <i>,</i> 65
534	72" STORM SEWER PIPE	3425	LF	\$375	\$1,284,37
1456	CURB BOX INLET TYPE A	90	EACH	\$5,200	\$468,00
1480	CURB BOX INLET TYPE B	3	EACH	\$4,800	\$14,40
1490	DROP BOX INLET TYPE 1	18	EACH	\$4,600	\$82,80
1490	DROP BOX INLET TYPE 2	2	EACH	\$4,100	\$8,20
1490	DROP BOX INLET TYPE 7	12	EACH	\$9,500	\$114,00
1559	DROP BOXINLET TYPE 13G	22	EACH	\$4,100	\$90,20
1568	DROP BOXINLET TYPE 13S	6	EACH	\$4,500	\$27,00
1614	CMBBI TY 14	55	EACH	\$3,700	\$203,50
1761	MANHOLE TY B	2	EACH	\$4,500	\$9,00
1767	MANHOLE TY C	28	EACH	\$6,100	\$170,80
ELOCATED V	VILLOW RUN SEWER				
528	36" STORM SEWER PIPE	356	LF	\$122	\$43,43
531	54" STORM SEWER PIPE	289	LF	\$175	\$50,57
532	60" STORM SEWER PIPE	380	LF	\$215	\$81,70
	108" STORM SEWER PIPE	1736	LF	\$1,100	\$1,909,60
	120" STORM SEWER PIPE	2380	LF	\$1,300	\$3,094,00
	36" EQUIV. STORM SEWER PIPE	2670	LF	\$150	\$400,50
1767	MANHOLE TY C	27	EACH	\$6,100	\$164,70
	DETENTION BASIN RECONSTR	3	EACH	\$100,000	\$300,00
	PUMP STATION	1	LS		\$
				SUBTOTAL	\$11,343,992
2568	Mobillization (5%)	1	5.0%		\$567,200
2569	Demobillization (1.5%)	1	1.5%		\$170,160
			PROJ	ECT SUBTOTAL	\$12,081,351
			25%	Contingency	\$3,020,338
				,	
				TION TOTAL	\$15,101,689

Drainage Reports

Drainage Data File: BSB Willow Run - ALT 2

					Area	Area
		Total Area			impervious	pervious
ID (cfs)	AttachTo	(Ac)	% impervious	% pervious	(Ac)	(Ac)
A1	IN42	0.5	100%	0%	0.5	0.0
A2	IN40	0.8	100%	0%	0.8	0.0
A3	IN41	0.3	100%	0%	0.3	0.0
A4	IN39	0.4	100%	0%	0.4	0.0
A7	IN38	0.5	100%	0%	0.5	0.0
A5	IN30	3.6	29%	71%	1.0	2.6
A6	IN46	1.9	27%	73%	0.5	1.4
A8	IN23	1.8	100%	0%	1.8	0.0
A9	IN31	0.5	100%	0%	0.5	0.0
A10	IN20	0.4	100%	0%	0.4	0.0
A11	IN151	0.9	100%	0%	0.9	0.0
A12	IN36	0.2	100%	0%	0.2	0.0
A13	IN21	0.1	100%	0%	0.1	0.0
A14	IN34	0.1	100%	0%	0.1	0.0
A15	IN22	0.0	100%	0%	0.0	0.0
A16	IN35	0.1	100%	0%	0.1	0.0
A17	IN37	0.5	100%	0%	0.5	0.0
A18	IN161	0.0	100%	0%	0.0	0.0
A19	IN160	0.0	100%	0%	0.0	0.0
A20	IN48	0.4	100%	0%	0.4	0.0
A21	IN162	0.1	100%	0%	0.1	0.0
A22	IN163	0.3	100%	0%	0.3	0.0
A23	IN32	0.4	100%	0%	0.4	0.0
A24	IN26	0.1	100%	0%	0.1	0.0
A25	IN29	0.2	100%	0%	0.2	0.0
A26	IN28	0.6	100%	0%	0.6	0.0
A27	IN24	0.2	100%	0%	0.2	0.0
A28	IN33	0.4	100%	0%	0.4	0.0
A29	IN49	0.3	100%	0%	0.3	0.0
A30	IN50	0.3	100%	0%	0.3	0.0
A31	IN84	0.1	100%	0%	0.1	0.0
A32	P164	0.1	100%	0%	0.1	0.0
A33	P164	0.2	100%	0%	0.2	0.0
A34	P164	1.7	100%	0%	1.7	0.0
A35	IN52	0.2	100%	0%	0.2	0.0
A36	IN53	0.2	100%	0%	0.2	0.0
A37	IN51	0.1	100%	0%	0.1	0.0
A38	IN51	0.2	100%	0%	0.2	0.0
A39	IN54	0.3	100%	0%	0.3	0.0

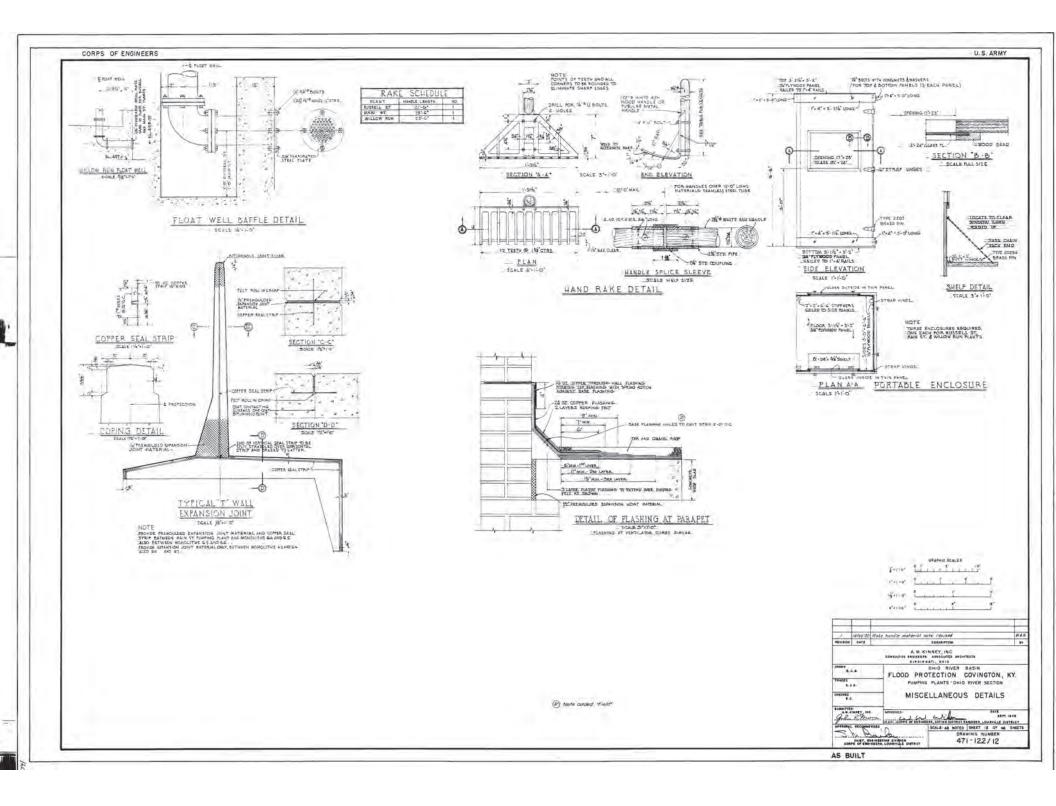
AreaAreaID (cfs)AttachTo(Ac)% impervious% pervious(Ac)(Ac)A40IN540.2100%0%0.20.2A41IN970.0100%0%0.00.0A42IN980.0100%0%0.00.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0
ID (cfs) AttachTo (Ac) % impervious % pervious (Ac) (Ac) A40 IN54 0.2 100% 0% 0.2 A41 IN97 0.0 100% 0% 0.0 A42 IN98 0.0 100% 0% 0.0	0.0 0.0 0.0 0.0 0.0
A40 IN54 0.2 100% 0% 0.2 A41 IN97 0.0 100% 0% 0.0 A42 IN98 0.0 100% 0% 0.0	0.0 0.0 0.0 0.0 0.0
A41IN970.0100%0%0.0A42IN980.0100%0%0.0	0.0 0.0 0.0 0.0 0.0
A42 IN98 0.0 100% 0% 0.0	0.0 0.0 0.0 0.0
	0.0 0.0 0.0
A43 IN97 0.1 100% 0% 0.1	0.0 0.0
A44 IN100 0.1 100% 0% 0.1	0.0
A45 IN104 0.1 100% 0% 0.1	
A46 IN102 0.1 100% 0% 0.1	
A47 IN105 0.2 100% 0% 0.2	0.0
A48 IN55 0.3 100% 0% 0.3	0.0
A49 IN51 1.3 100% 0% 1.3	0.0
A50 IN166 0.2 100% 0% 0.2	0.0
A51 IN96 0.3 100% 0% 0.3	0.0
A52 IN87 0.0 100% 0% 0.0	0.0
A53 IN88 0.1 100% 0% 0.1	0.0
A54 IN89 0.1 100% 0% 0.1	0.0
A55 IN90 0.1 100% 0% 0.1	0.0
A56 IN92 0.1 100% 0% 0.1	0.0
A57 IN91 0.1 100% 0% 0.1	0.0
A58 IN95 0.1 100% 0% 0.1	0.0
A59 IN94 0.9 100% 0% 0.9	0.0
A60 IN14 0.5 100% 0% 0.5	0.0
A61 IN15 0.5 100% 0% 0.5	0.0
A62 IN13 0.5 100% 0% 0.5	0.0
A63 IN19 0.4 100% 0% 0.4	0.0
A64 IN18 0.2 100% 0% 0.2	0.0
A65 IN143 0.5 100% 0% 0.5	0.0
A66 IN18 0.2 100% 0% 0.2 A67 IN142 0.3 100% 0% 0.3	0.0
A67 IN142 0.3 100% 0% 0.3 A68 IN142 0.2 100% 0% 0.2	0.0 0.0
A68 IN142 0.2 100% 0% 0.2 A69 IN142 0.1 100% 0% 0.1	0.0
A70 IN55 0.3 100% 0% 0.3	0.0
A71 IN98 0.1 100% 0% 0.1	0.0
A72 IN56 0.9 100% 0% 0.9	0.0
A73 IN56 0.1 100% 0% 0.1	0.0
A74 IN57 0.1 100% 0% 0.1	0.0
A75 IN58 0.1 100% 0% 0.1	0.0
A76 IN61 0.2 100% 0% 0.2	0.0
A77 IN61 0.2 100% 0% 0.2	0.0
A78 IN59 0.1 100% 0% 0.1	0.0
A79 IN61 0.1 100% 0% 0.1	0.0
A80 IN60 0.2 100% 0% 0.2	0.0
A81 IN148 0.1 100% 0% 0.1	0.0
A82 IN149 0.1 100% 0% 0.1	0.0
A83 IN62 0.1 100% 0% 0.1	0.0

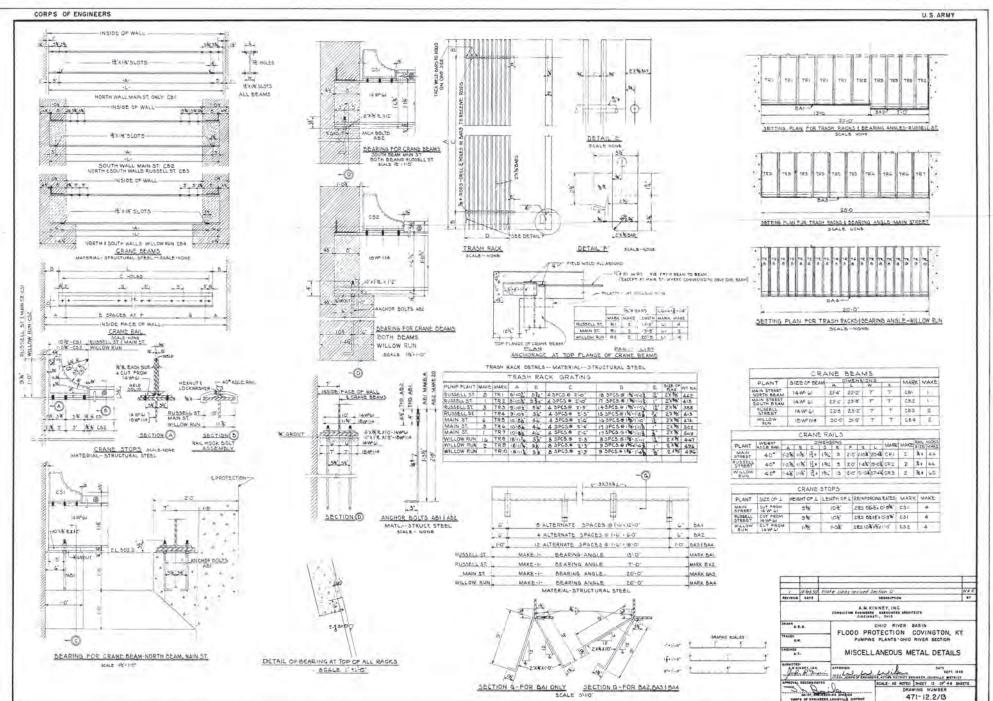
					A	A
					Area	Area
ID (efc)		Total Area		0/	impervious	pervious
ID (cfs)	AttachTo	(Ac) 0.2	% impervious 100%	% pervious	(Ac) 0.2	(Ac) 0.0
A84 A85	IN106 IN107	0.2	100%		0.2	0.0
A85 A86	IN107 IN108	0.2			0.2	0.0
A80 A87	IN108 IN109	0.2	100%		0.2	0.0
A87 A88	IN109 IN110	0.1	100%		0.1	0.0
A89	IN110 IN144	0.1	100%		0.1	0.0
A90	IN145	0.0			0.0	0.0
A91	IN113	0.1	100%		0.1	0.0
A92	IN112	0.2	100%		0.2	0.0
A93	IN12	1.1	0%		0.0	1.1
A94	IN167	2.8			0.0	2.8
A95	IN113	0.1			0.1	0.0
A96	IN114	0.3	100%		0.3	0.0
A97	IN10	0.0			0.0	0.0
A98	IN11	0.1	100%	0%	0.1	0.0
A99	IN115	0.2	100%	0%	0.2	0.0
A100	IN116	0.4	100%	0%	0.4	0.0
A101	IN5	0.5	100%	0%	0.5	0.0
A102	IN9	0.8	100%	0%	0.8	0.0
A103	IN8	0.7	100%	0%	0.7	0.0
A104	IN1	0.3	100%	0%	0.3	0.0
A105	IN3	0.4	100%	0%	0.4	0.0
A106	IN45	0.5	100%	0%	0.5	0.0
A107	IN16	0.4	100%		0.4	0.0
A108	IN7	0.4	100%		0.4	0.0
A109	IN2	0.2	100%		0.2	0.0
A110	IN43	0.1	100%		0.1	0.0
A111	IN152	0.1	100%		0.1	0.0
A112	IN153	0.1			0.1	0.0
A113	IN64	0.1			0.1	
A114	IN64	0.3			0.3	0.0
A115	IN63	0.1			0.1	0.0
A116	IN64	0.1			0.1	0.0
A117	IN155	0.2			0.2	0.0
A118	IN157	0.1 0.2			0.1 0.2	0.0
A119 A120	IN155 IN156	0.2			0.2	0.0 0.0
A120 A121	IN150 IN65	0.1			0.1	0.0
A121 A122	IN65 IN66	0.1			0.1	0.0
A122 A123	IN66	0.2			0.2	0.0
A123 A124	IN66	0.0			0.0	0.0
A124 A125	IN67	0.0			0.0	0.0
A125 A126	IN67 IN67	0.0			0.0	0.0
A120 A127	IN69	0.0				
,,,,		5.7	100/0	0/0	0.7	0.0

					A	A
		T . I . I . A			Area	Area
		Total Area	0/ :	0/	impervious	pervious
ID (cfs)	AttachTo	(Ac)	% impervious	% pervious	(Ac)	(Ac)
A128	IN71	0.6	100%		0.6	0.0
A129	IN70	0.9	100%		0.9	0.0
A130	IN72	0.5	100%		0.5	0.0
A131	IN159	0.7	100%		0.7	0.0
A132 A133	IN159 IN154	0.5 2.1	100% 100%		0.5 2.1	0.0 0.0
A135 A134	IN154 IN158	1.6	100%		1.6	0.0
A134 A135	IN138 IN127	0.1	100%		0.1	0.0
A135 A136	IN127 IN117	0.1	100%		0.1	0.0
A130 A137	IN117 IN118	0.3	100%		0.3	0.0
A137 A138	IN118 IN126	0.4	100%		0.4	0.0
A138 A139	IN120 IN125	0.2	100%		0.2	0.0
A135 A140	IN125 IN119	0.2	100%		0.2	0.0
A140	IN115 IN120	0.1	100%		0.1	0.0
A142	IN120 IN121	0.1	100%		0.1	0.0
A143	IN121	0.1	100%		0.1	0.0
A144	IN124	0.7	30%		0.2	0.5
A145	IN123	0.3	100%		0.3	0.0
A146	IN123	1.2	29%		0.3	0.8
A147	IN130	0.4	100%		0.4	0.0
A148	IN78	0.5	100%		0.5	0.0
A149	IN79	0.4	100%		0.4	0.0
A150	IN132	0.0			0.0	0.0
A151	IN133	0.1	100%		0.1	0.0
A152	IN168	2.1	100%		2.1	0.0
A153	IN124	0.3	100%		0.3	0.0
A154	IN134	0.2	100%		0.2	0.0
A155	IN169	3.0	100%	0%	3.0	0.0
A156	IN135	0.1	100%	0%	0.1	0.0
A157	IN136	0.0	100%	0%	0.0	0.0
A158	IN137	0.3	31%	69%	0.1	0.2
A159	IN138	0.3	52%	48%	0.2	0.1
A160	IN140	0.1	100%	0%	0.1	0.0
A161	IN141	0.0	100%	0%	0.0	0.0
A162	IN189	0.6	69%	31%	0.4	0.2
A163	IN189	0.4	46%	54%	0.2	0.2
A164	IN190	2.4	35%	65%	0.8	1.6
A165	IN195	0.8	100%		0.8	0.0
A166	IN186	1.8	100%	0%	1.8	0.0
A167	IN196	0.5	100%		0.5	0.0
A168	IN187	0.2	100%		0.2	0.0
A169	IN194	0.3	100%		0.3	0.0
A170	IN191	3.7	32%		1.2	2.5
A171	IN188	0.6	100%	0%	0.6	0.0

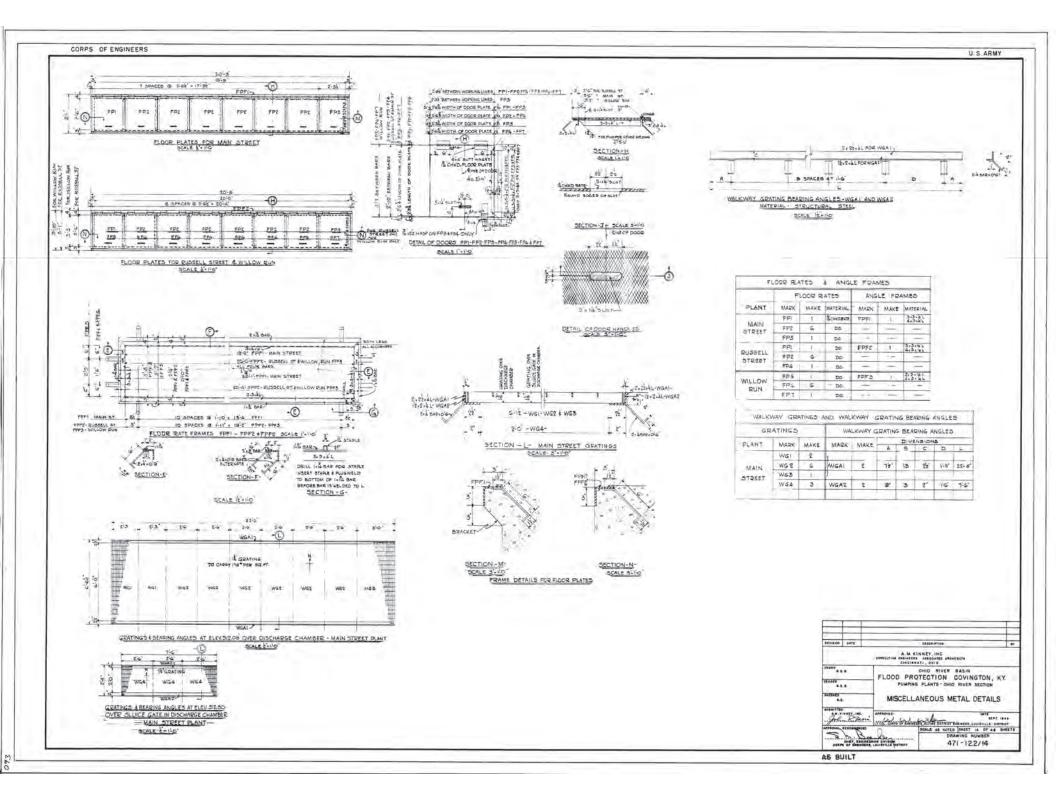
					Area	Area
		Total Area			impervious	pervious
ID (cfs)	AttachTo	(Ac)	% impervious	% pervious	(Ac)	(Ac)
A172	IN182	1.7	100%	0%	1.7	0.0
A173	IN183	0.7	100%	0%	0.7	0.0
A174	IN193	4.0	55%	45%	2.2	1.8
A175	IN192	5.3	22%	78%	1.2	4.1
A176	IN192	4.2	43%	57%	1.8	2.4
A177	IN181	0.7	100%	0%	0.7	0.0
A178	IN184	0.7	100%	0%	0.7	0.0
A179	IN180	0.9	100%	0%	0.9	0.0
A180	IN185	0.7	100%	0%	0.7	0.0
A181	IN179	0.2	100%	0%	0.2	0.0
A182	IN177	1.4	100%	0%	1.4	0.0
A183	IN178	2.6	52%	48%	1.3	1.2
A184	IN197	3.3	44%	56%	1.4	1.8
A185	IN198	37.9	38%	62%	14.4	23.5
A186	IN176	0.9	100%	0%	0.9	0.0
A187	IN174	1.4	100%	0%	1.4	0.0
A188	IN174	0.4	100%	0%	0.4	0.0
A189	IN199	2.5	37%	63%	0.9	1.6
A190	IN201	2.1	28%	72%	0.6	1.5
A191	IN173	0.3	100%	0%	0.3	0.0
A192	IN173	0.4	100%	0%	0.4	0.0
A193	IN25	0.7	100%	0%	0.7	0.0
A194	IN44	0.5	100%	0%	0.5	0.0
A195	IN170	1.5	100%	0%	1.5	0.0
A196	IN202	28.6	21%	79%	6.0	22.6
A197	IN203	0.9	41%	59%	0.4	0.6
A198	IN204	2.6	46%	54%	1.2	1.4
A199	IN205	29.2	19%	81%	5.5	23.6
A200	IN171	0.7	100%	0%	0.7	0.0
A201	IN171	0.5	100%	0%	0.5	0.0
A202	IN172	0.5	100%	0%	0.5	0.0
A203	IN172	0.5	100%	0%	0.5	0.0
A204	IN200	0.6	100%	0%	0.6	0.0
A205	IN200	0.6	100%	0%	0.6	0.0
A206	IN206	3.6	29%	71%	1.0	2.5
A207	IN207	3.8	21%	79%	0.8	3.0
A208	P232	21.7	21%	79%	4.5	17.1
A209	IN175	4.9	61%	39%	3.0	1.9
A210	IN6	221.0	22%	78%	48.6	172.4
		466.6			169.5	297.1
		+00.0			105.5	237.1

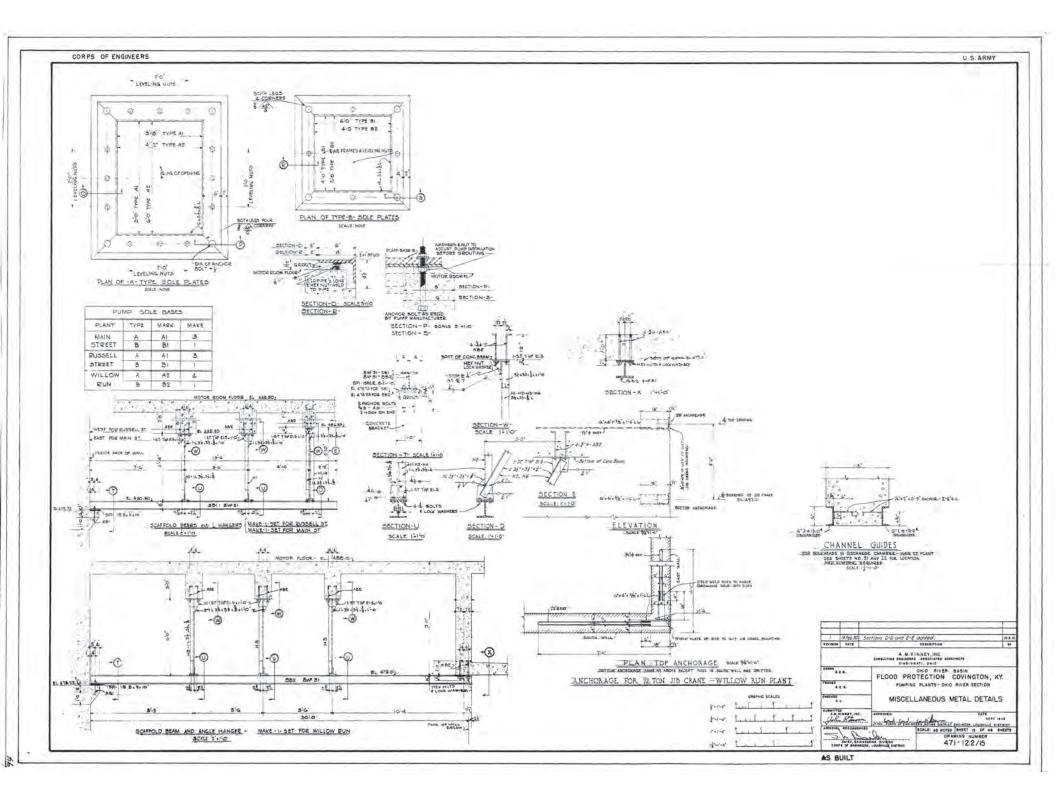
APPENDIX C Pump Station Record Plans

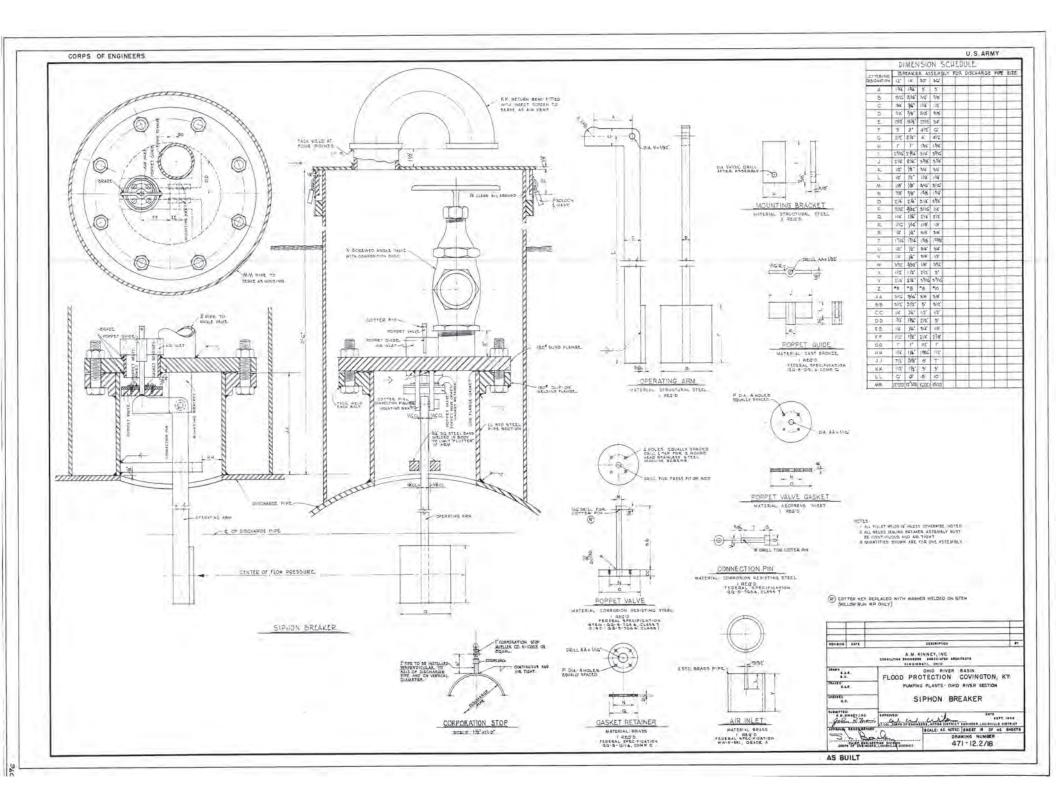


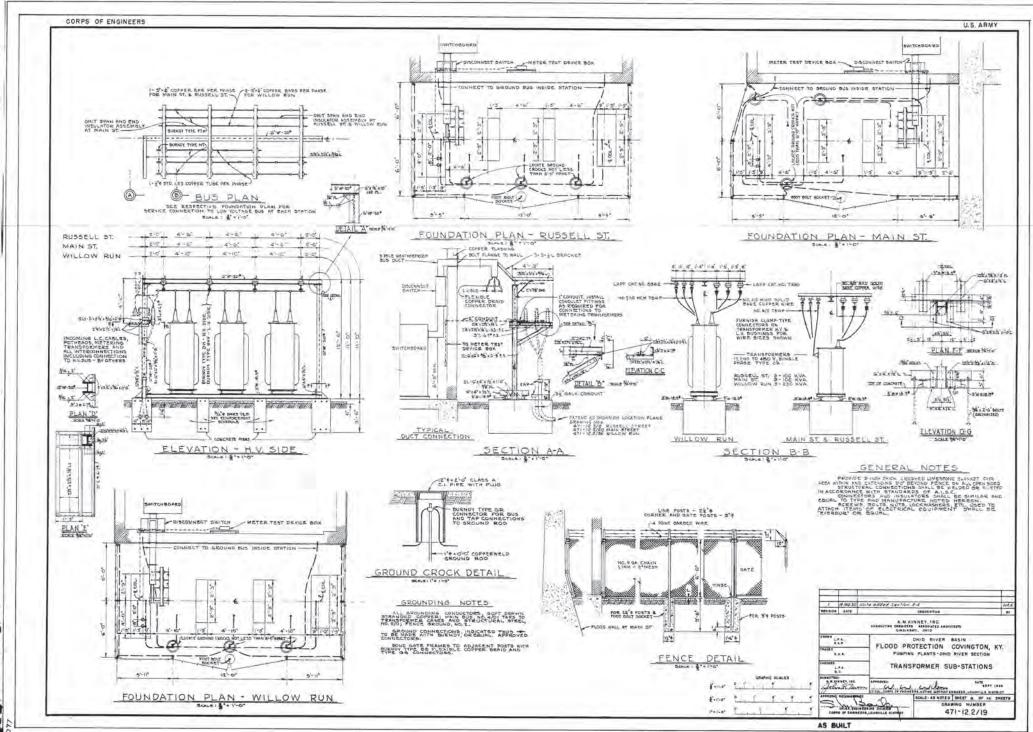


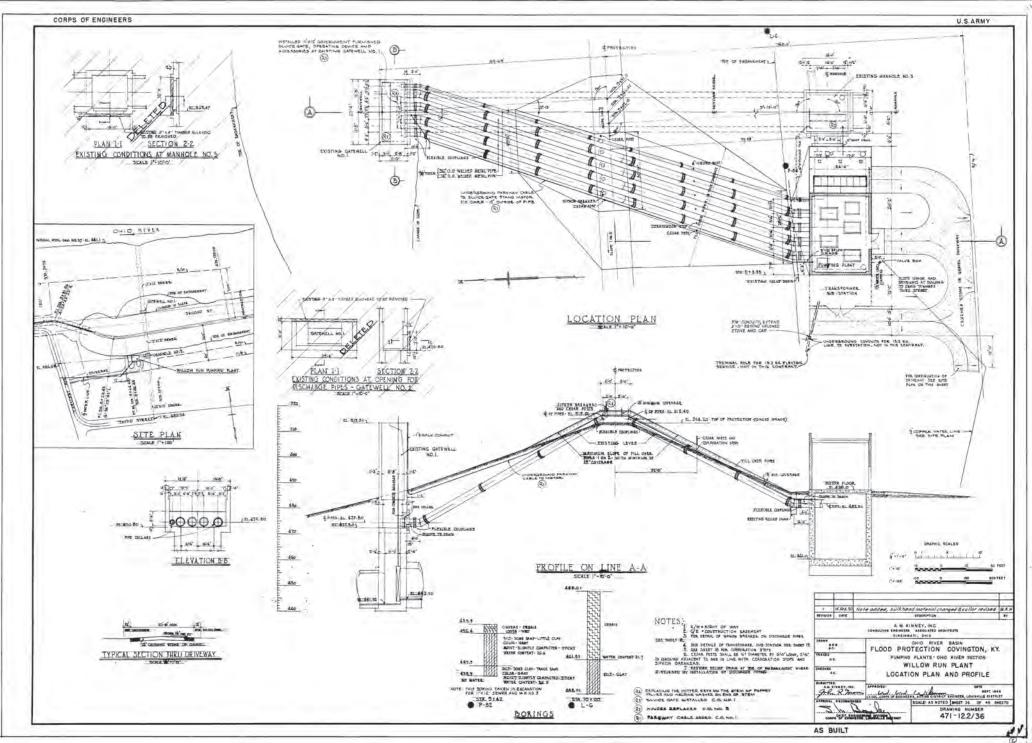
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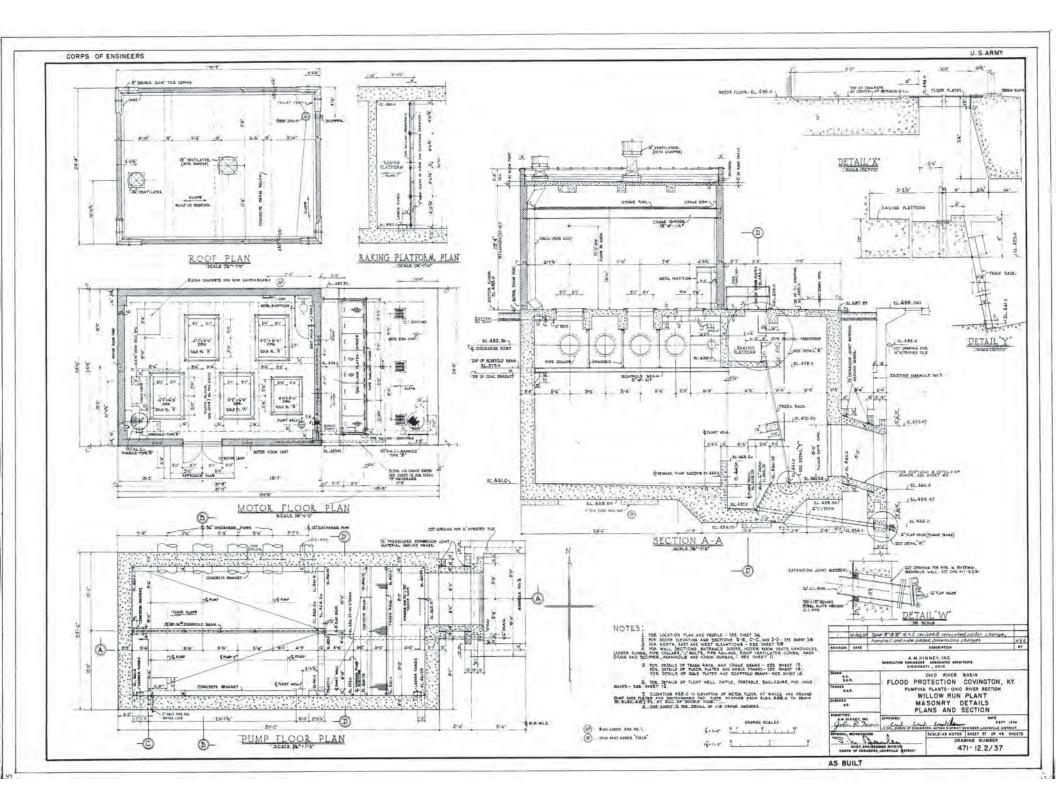


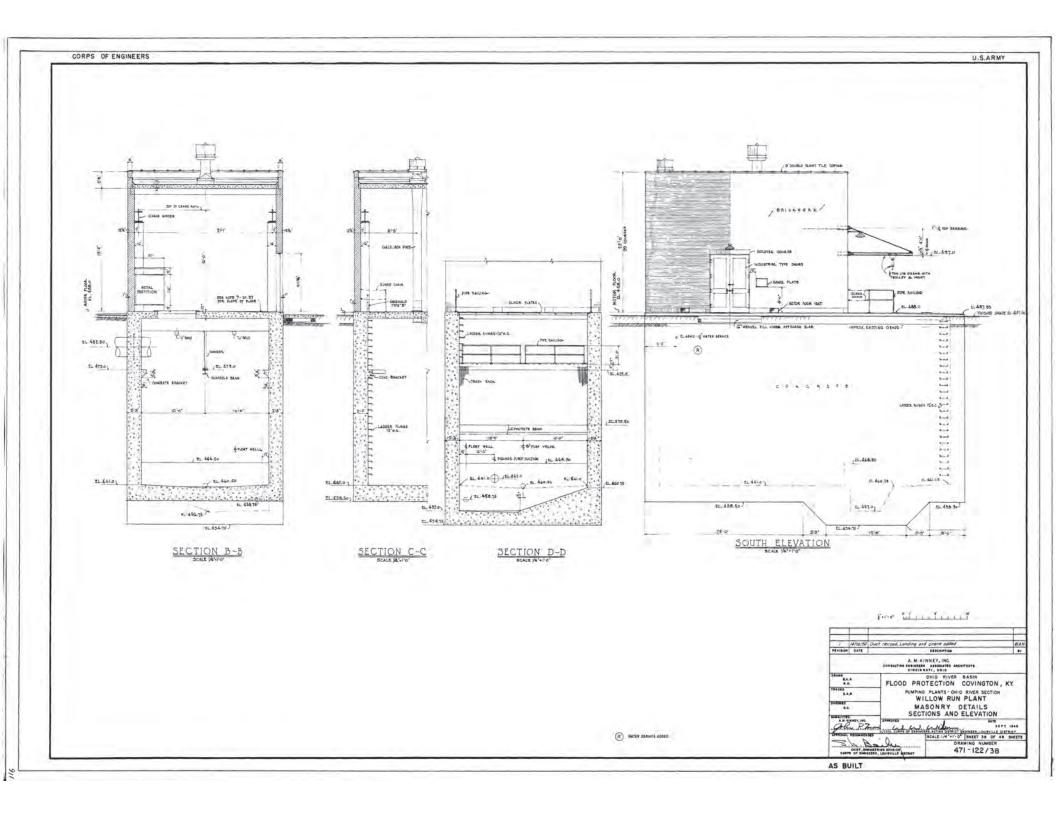


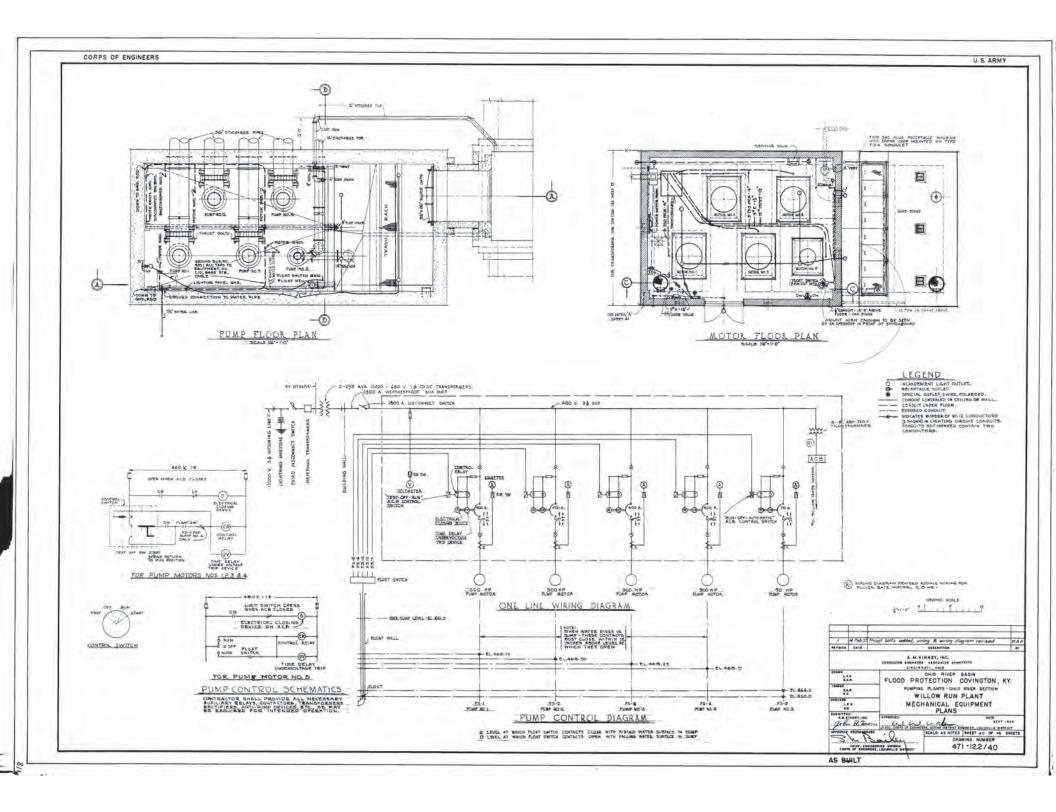


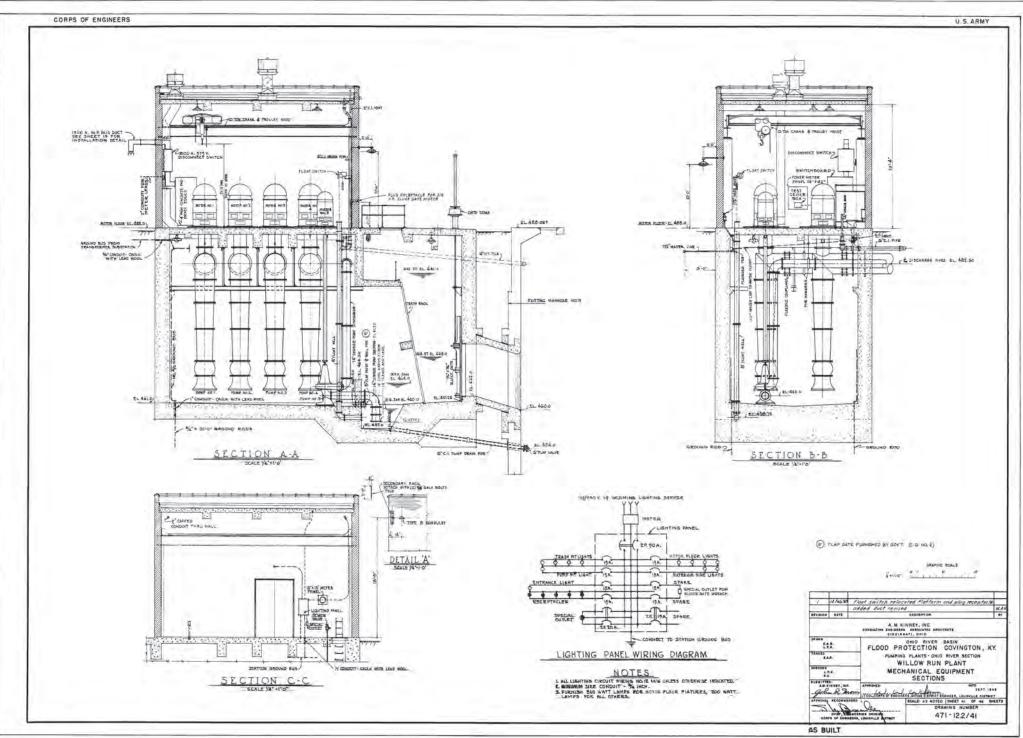
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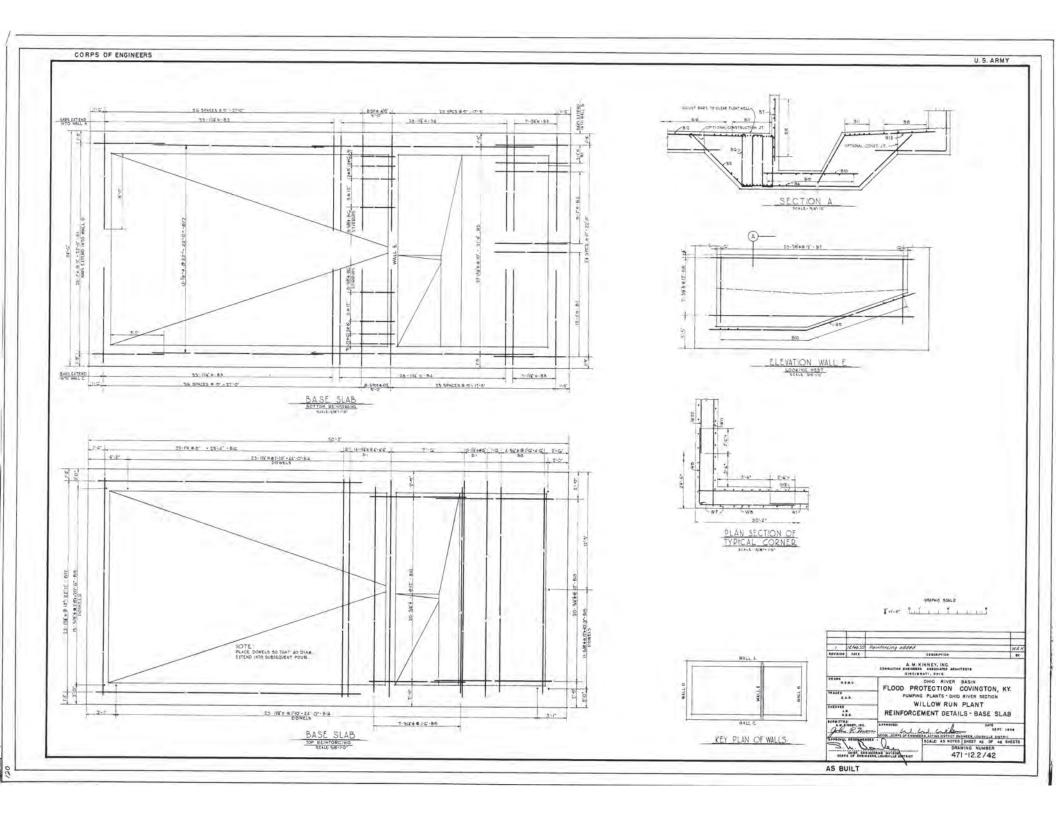
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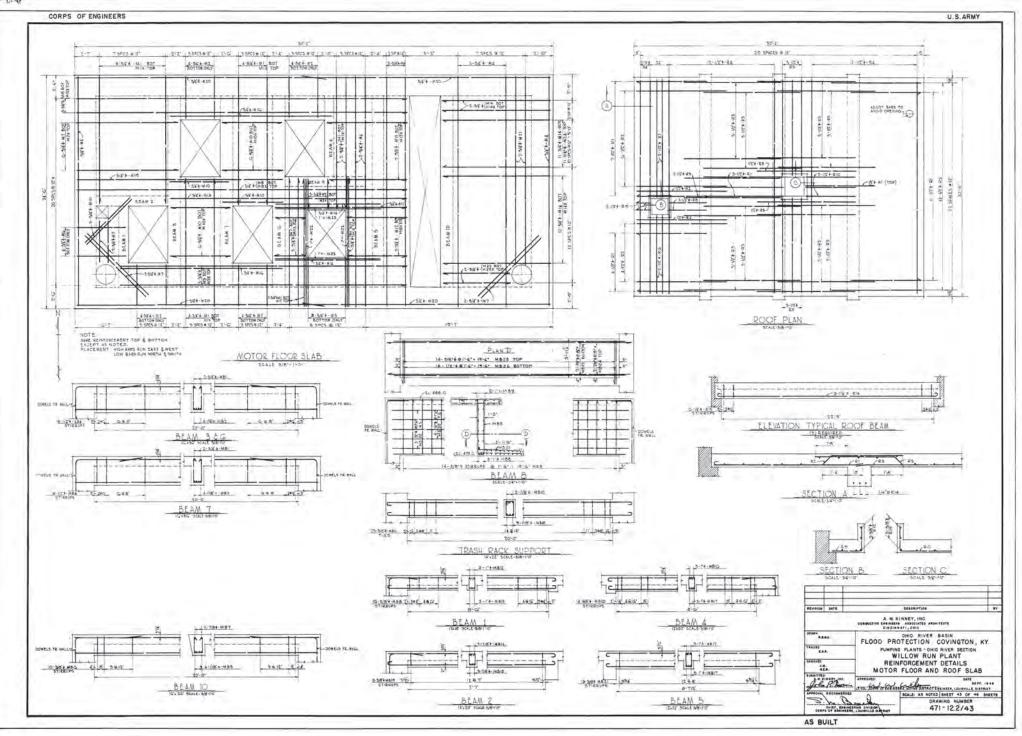






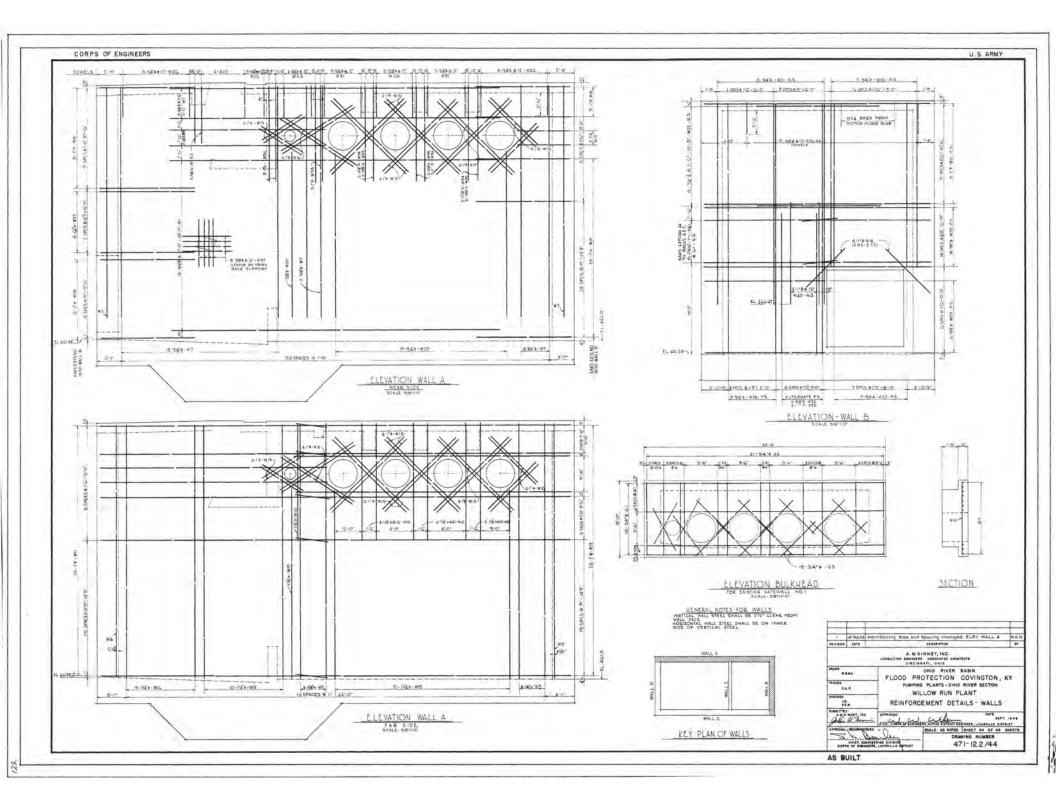


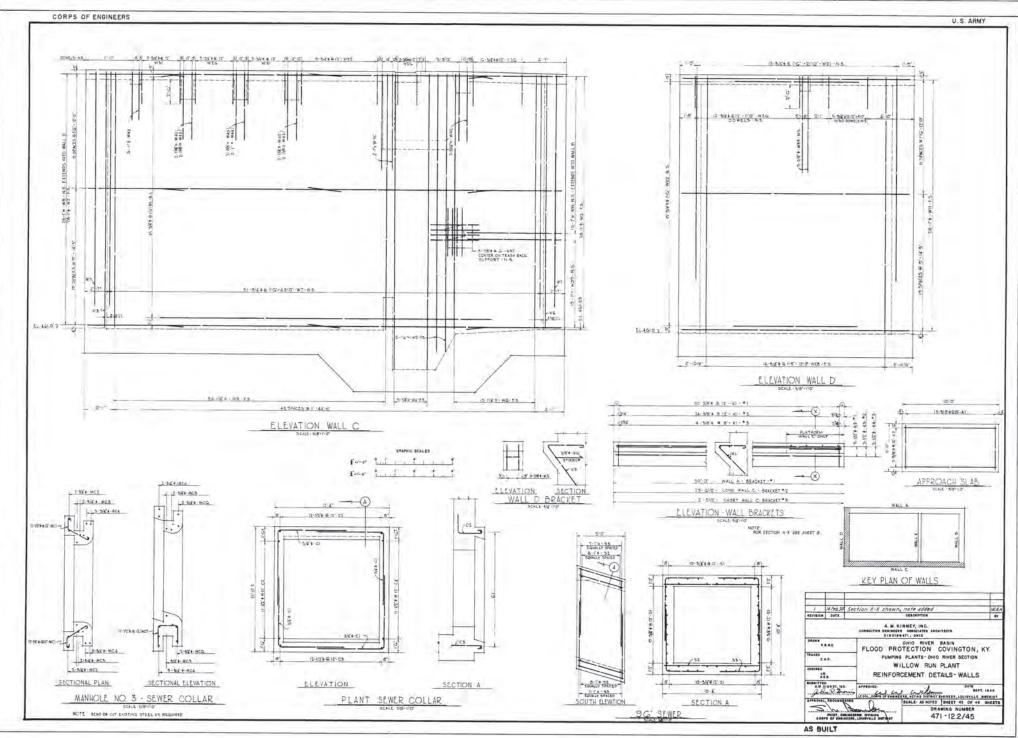




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3





CORPS OF ENGINEERS

U.S. ARMY

	40	312.6	LENGTH	BENDING DIAGRAM	WEIGHT	TOTAL
-	HEQ:	0	100 Samp		BAGH	WEIGHT
1		1.000	1	BASE SLAB		
80	41)*#	121-31	1 10-12	403	2414.4
	15		1	7.471		1
BZ.	9	1**	111-7-	J 7-11	39.57	354
	1			2-7-	1	1
85	80	1-1/4" 0	17-2	17-2	91.22	7297.0
20	1	1		10-0-	1	14290
84	54	6-1/47 8	211.00		11.51	6247.9
-	-	-	-	10.00	100.83	9413
BS	27	Ist dates	28'-11"	And Sora	(53.5)	1.000
	61	10.14.0	+D -11"	are are	153.5	4148.0
-	10			1 - Walter - 1	1	-
86	16	2/0.4	25' - 5'	1 E.P 15-9	26.5	4243
-			-	1-1 1-1	1	1.1
87	20		4 · B'	<u><u> </u></u>	15.65	272.6
55	.16		211-4"	STRAIGHT	32.04	352.4
80	7	3/4"4	22' - D*		33.9	2313
-					- 1	1
810	20	3/4 4	101-04	STRAIGHT	15.02	300.4
BH.	20	1-1/4*8		Y	119.34	2990.8
812	28	1-174.8	27'- B*		1470	\$587.2
ērē.	20		15'- 6'	dree	1518	1055
	-			2.0. 2		
814	50	1-1/4-=	71- 7	0.01	ines	20/55
815	24	5/8*9		4.11.5	40.27	
512	39	2/6-9	4'-10"	4-3-3	5,04	121.0
	13			STRAIGHT	74.60	1917.2
BIT .	18	3/6'+	180"		27.04	35.5
-	-					1.2.1
_			_			
1			-			
	1	1.1.1			1.1	20.11
	-				-	-
			-		-	
		1	-		-	
	-		-		-	
-					-	-
M	22	1.01	Mote	R FLOOR BLAD	-	
-		3/4**	187 - 4*	STRAIGHT	20.02	440.4
HZ	20	3/4" 0	4- 4"		6.50	(50.0
MS.	3		3'- 11		643	18.5
		3/4. 4				
	20	3/4. 4	24" - 1"		36.17	940.4
NS		3/4*¢ 3/4*¢	24" + 1* 4" +10*	-		
NS	20 5 4	3/4. 4	24" + 1* 4" +10*		36.17	940.4
NS	29 5	3/4*¢ 3/4*¢	24' - 1* 4' - 10* 5'- 3*		36.17 725	940.4
NS NG N7	20 5 4	3/4*¢ 3/4*¢ 3/4*¢	24" - 1" 4" + 10" 5" - 3" 10" - 9"		36.17 7.25 7.69 %15	940.4 34.5 31.6
N5 N6 H7 H8	5 4	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	24' - 1* 4' - 10* 5'- 3* 10'- 9* 34'- 9*		56.17 725 769 46.15 57.10	940.4 34,3 31.6 2261 2088
NS NG N7 NB	20 5 4 14 4	3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4	24' - 1" 4' + 10" 5' - 3" 10' - 9" 54' - 0"	-	56.17 125 109 46.19 57.19 45.51	940.4 54.5 51.6 2261
N5 N6 N7 H8 H10	20 5 4 14 4 3	3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4	24' - 1" 4' +10" 5'- 3" 10' - 9" 54'- 9" 54'- 9" 50' - 6"	:	56.17 725 769 4619 57.19 6551 46551	940.4 36.5 31.6 226.1 206.6 57.4 192.5
NS NF NF NF NF NF NF NF NF NF NF NF NF NF	5 4 14 4 3 50 5	3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 5/4*4 5/4*4	24' - 1* 4' + 10* 5' - 3* 10* - 9* 54' - 9* 54' - 9* 54' - 9* 54' - 9* 54' - 9*		56.17 725 769 6515 57.10 6551 364 4.58	940.4 54.5 51.6 2251 2068 157.4 102.6 544
NS NG H7 H8 H10 H10 H10 H10 H10 H12	20 5 4 14 4 3 20 5 5 5	3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4	24' = 1* 4'+10* 5'- 3* 10'- 3* 54'- 0* 54'- 0* 6'- 5* 5'- 5* 6'- 5*	*	5617 725 769 615 57.0 455 364 455 364 4.58 931	940.4 34,3 31.6 222) 2088 157,4 102,0 244 47,5
N5 R6 N7 H8 H10 H10 H10 H10 H10 H10 H10 H10 H10	20 5 14 14 3 20 5 5 7	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	24' = 1* 4'+10* 5'- 3* 10'- 3* 34'- 9* 34'- 9* 5'- 5* 5'- 5* 6'- 4* 8'- 4*	*	56.17 725 769 6315 87.19 6351 764 7.64 7.64 7.61 7.64 7.61 7.61 7.61 7.61 7.61 7.61 7.61 7.61	940.4 36.5 31.6 2261 2068 157.4 102.0 244 47.5 89.4
N5 R6 N7 H8 H10 H10 H10 H10 H10 H10 H10 H10 H10	20 5 4 14 4 3 20 5 5 5	3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4 3/4*4	24' = 1* 4'+10* 5'- 3* 10'- 3* 34'- 9* 34'- 9* 5'- 5* 5'- 5* 6'- 4* 8'- 4*	*	5617 725 769 615 57.0 455 364 455 364 4.58 931	940.4 34,3 31.6 222) 2088 157,4 102,0 244 47,5
NS N6 H7 H8 H10 H10 H10 H11 H10 H11 H12 H13	20 5 4 34 3 20 5 5 7 27	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	24' - 1" 4' + 10" 5' - 9" 6' - 9" 54' - 9" 50' - 6" 5' - 5" 6' - 4" 8' - 6" H' - 4"	* * * * * *	56.17 7.25 7.69 45.15 57.15 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 1.27 7.25 57.17 7.25 57.17 7.25 57.17 7.25 57.17 5	9404 343 316 3261 2068 574 1025 244 475 894 4555
N5 N6 H7 H8 H10 H11 H10 H11 H12 H13 H14 H14 H14	20 5 14 14 3 20 5 5 7	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24^{\circ} = 1^{\circ}$ $4^{\circ} + 10^{\circ}$ $5^{\circ} = 3^{\circ}$ $0^{\circ} = 3^{\circ}$ $54^{\circ} = 9^{\circ}$ $50^{\circ} = 6^{\circ}$ $5^{\circ} = 5^{\circ}$ $6^{\circ} = 4^{\circ}$ $8^{\circ} = 6^{\circ}$ $11^{\circ} = 4^{\circ}$ $17^{\circ} = 1^{\circ}$	*	56.17 725 769 6315 87.19 6351 764 7.64 7.64 7.61 7.64 7.61 7.61 7.61 7.61 7.61 7.61 7.61 7.61	940.4 36.5 31.6 2261 2068 157.4 102.0 244 47.5 89.4
N5 N6 H7 H8 H10 H11 H10 H11 H12 H13 H14 H14 H14	20 5 4 34 3 20 5 5 7 27	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24^{\circ} = 1^{\circ}$ $4^{\circ} + 10^{\circ}$ $5^{\circ} = 3^{\circ}$ $0^{\circ} = 3^{\circ}$ $54^{\circ} = 9^{\circ}$ $50^{\circ} = 6^{\circ}$ $5^{\circ} = 5^{\circ}$ $6^{\circ} = 4^{\circ}$ $8^{\circ} = 6^{\circ}$ $11^{\circ} = 4^{\circ}$ $17^{\circ} = 1^{\circ}$	* * * * * *	56.17 7.25 7.69 45.15 57.15 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 45.51 1.27 7.25 57.17 7.25 57.17 7.25 57.17 7.25 57.17 5	9404 343 316 3261 2068 574 1025 244 475 894 4555
NS NG HT HB HT HT HT HT HT HT HT HT HT HT HT HT HT	299 5 4 14 14 3 20 5 5 5 7 27 27 4	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24^{\circ} = 1^{\circ}$ $4^{\circ} \pm 10^{\circ}$ $5^{\circ} = 3^{\circ}$ $5^{\circ} = 5^{\circ}$ $5^{\circ} = 5^{\circ}$ $5^{\circ} = 5^{\circ}$ $5^{\circ} = 5^{\circ}$ $6^{\circ} = 4^{\circ}$ $8^{\circ} = 6^{\circ}$ $11^{\circ} = 4^{\circ}$ $17^{\circ} = 1^{\circ}$ $14^{\circ} = 6^{\circ}$	e e e e e e e e e e e e e e e e e e e	56.17 7.25 7.69 45.19 57.19 45.51 3.64 4.58 9.81 (2.17 7.02) 2.5.46	940.4 34.3 31.6 3221 2088 157.4 102.0 244 47.5 87.4 4575 102.6
N5 N6 H7 H8 H10 H10 H10 H10 H11 H12 H12 H13 H14 H14 H15 H14 H15 H14 H15 H14 H15 H15 H15 H15 H15 H15 H15 H15	299 5 4 14 4 5 5 5 5 7 27 27 4 2	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{+}$ $4' \pm 10^{+}$ $3' = 3^{+}$ $34' = 9^{+}$ $34' = 9^{+}$ $50' = 6^{+}$ $5' = 5^{+}$ $6' = 4^{+}$ $8' = 6^{+}$ $11' = 4^{+}$ $17' = 1^{+}$ $14' = 6^{+}$ $15' = 6^{+}$	* * * * * * * * * * * * * * * * * * *	56.17 725 769 6515 5719 4551 764 4551 764 4551 764 4551 764 4551 764 4551 764 764 764 764 764 764 764 765 765 765 765 765 765 765 765 765 765	940.4 36.3 31.6 226.8 157.4 102.0 244 47.5 80.4 450.5 102.6 44.1 77.1
NS NG NT HB HID HID HID HID HID HID HID HID HID	299 5 4 14 4 5 5 5 5 7 27 4 2 2 2	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{*}$ $4' \pm 10^{*}$ $3' = 3^{*}$ $10' = 3^{*}$ $34' = 0^{*}$ $50' = 6^{*}$ $5' = 5^{*}$ $6' = 4^{*}$ $8' = 6^{*}$ $11' = 4^{*}$ $17' = 1^{*}$ $14' = 6^{*}$ $15' = 6^{*}$ $14' = 6^{*}$ $15' = 6^{*}$	а 	56.17 725 769 4615 87.19 4551 364 4551 7.64 4.58 9.81 12.77 7.02 25.45 22.45 36.56 32.67	940.4 36.3 31.6 226.1 2068 157.4 102.6 244 47.5 80.4 450.5 102.6 44.1 TT.1 655
N5 R6 H7 H8 H10 H11 H12 H13 H13 H14 H13 H14 H15 H15 H15 H15 H15 H15 H15 H15	29 5 4 14 4 5 5 7 27 4 2 2 2 2 2 2	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{+}$ $4' + 10^{+}$ 5' = 5' 10' - 5' 4' - 0' 5' - 5' 5' - 5' 6' - 4' 5' - 5' 11' - 4' 11' - 4' 11' - 5' 15' - 5' 11'	а 	56.17 125 7.69 6.19 57.10 6.59 35.10 4.59 7.64 6.59 1.277 7.02 25.65 72.03 36.56 32.67 35.17	940.4 36.3 31.6 2221 2088 157.4 102.6 244 47.5 85.4 4555 102.6 44.1 77.1 655 318.4
N5 N6 N7 H8 H10 H11 H12 H13 H14 H13 H14 N16 N16 H15 H20 H20 H21	297 5 4 14 4 5 5 5 5 5 7 27 27 4 2 2 2 2 8 4 2 2 2 8 4	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{+}$ $4' + 10^{+}$ 5' = 5' 0' - 5' 5' - 5' 5' - 5' 5' - 5' 6' - 4' 8' - 6' 1' - 4' 1' - 4' 1' - 5' 5' - 6' 1' - 5' 5' - 5' 5' - 5' 1' - 5' 5' - 5' - 5' 5' - 5'	а 	36.17 125 769 6515 87.19 4551 364 4551 364 4551 1277 702 2546 22546 22546 3856 3267 3257 2256	940.4 36.3 31.6 2221 2088 157.4 102.6 244 47.5 85.4 102.6 44.1 77.1 655 318.4 117.2
NS NG NT HB HID HID HID HID HID HID HID HID HID HID	29 5 4 14 4 5 5 5 5 7 27 4 2 2 2 8 4 4 2 2 2 8 4 4 4 4 4	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{*}$ $4' + 10^{*}$ $5' = 9^{*}$ $10' - 9^{*}$ $54' - 0^{*}$ $50' - 6^{*}$ $6' - 8^{*}$ $8' - 6^{*}$ $11' - 4^{*}$ $17' = 1^{*}$ $14' - 6^{*}$ $14' - 6^{*}$ $14' - 6^{*}$ $15'' - 6^{*}$ $10' - 2^{*}$ $10' - 2^{*}$ 10' -	4 3 3 4 4 4 4 6 8 7 8 7 8 8 7 8 8 7 8 8 8 8 8 8 8 8 8	36,17 725 769 6515 87.0 4551 364 4551 364 4551 1277 702 25,45 22,45 38,56 32,47 38,56 32,47 38,77 23,29 45,32	940.4 36.3 31.6 226.1 2068 157.4 102.6 244 47.5 80.4 4505 102.6 44.1 177.1 655 318.4 117.2 181.3
N5 N6 N7 H8 H10 H11 M12 H10 H11 M12 H13 M14 M15 M16 M15 M20 M21 W21 W22 A23	200 5 4 14 4 3 20 5 5 7 7 27 4 2 7 27 4 2 2 2 2 8 4 4 4 4 4 4 4	3/4* ¢ 3/4* ¢	$24' = 1^{+}$ $4' + 10^{+}$ $5' - 9^{+}$ $10' - 9^{+}$ $54' - 0^{+}$ $50' - 6^{+}$ $6' - 8^{+}$ $8' - 6^{+}$ $8' - 6^{+}$ $11' - 4^{+}$ $17' - 1^{+}$ $14' - 6^{+}$ $15' - 6^{+}$ $11' - 4^{+}$ $11' - 4^{+}$	а 	56.17 125 169 4515 57.10 4515 36.45 6.85 93.10 1.02 1.02 1.02 25.45 22.03 36.56 32.65 35.67 35.17 27.29 45.32 36.52	9404 36,5 31,6 2261 2066 57,4 102,6 57,4 102,6 57,4 44,1 77,1 102,6 44,1 177,2 180,3 318,4 117,2 (54,1
N5 N6 N7 H8 H10 H11 M12 H10 H11 M12 H13 M14 M15 M16 M15 M20 M21 W21 W22 A23	29 5 4 14 4 5 5 5 5 7 27 4 2 2 2 8 4 4 2 2 2 8 4 4 4 4 4	3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢ 3/4*¢	$24' = 1^{+}$ $4' + 10^{+}$ $5' - 9^{+}$ $10' - 9^{+}$ $54' - 0^{+}$ $50' - 6^{+}$ $6' - 8^{+}$ $8' - 6^{+}$ $8' - 6^{+}$ $11' - 4^{+}$ $17' - 1^{+}$ $14' - 6^{+}$ $15' - 6^{+}$ $11' - 4^{+}$ $11' - 4^{+}$	а 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	36,17 725 769 6515 87.0 4551 364 4551 364 4551 1277 702 25,45 22,45 38,56 32,47 38,56 32,47 38,77 23,29 45,32	940.4 36.3 31.6 226.1 2068 157.4 102.6 244 47.5 80.4 4505 102.6 44.1 177.1 655 318.4 117.2 181.3
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H4 N5 N6 N7 H8 H10 H11 H10 H13 H12 H13 H12 H13 H14 M18 M14 M18 M18 M20 M21 M22 A23 A23 A24 H25	200 5 4 14 4 3 20 5 5 5 7 27 27 4 2 2 2 2 4 2 2 2 2 8 6 4 4 4 4 11 11 2 2 2 2 2 2 2 2 2 3 6 4 4 11 2 7 12 7 12 7 12 7 12 7 12 7 12	3/4*6 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426	$24t + 1^{+}$ $4^{+} - 10^{+}$ $5^{+} - 9^{+}$ $10^{+} - 9^{+}$ $10^{+} - 9^{+}$ $30^{+} - 9^{+}$ $30^{+} - 9^{+}$ $5^{+} - 3^{+}$ $5^{+} - 3^{+}$ 5	а 	56.17 125 169 4515 57.10 4515 36.45 6.85 93.10 1.02 1.02 1.02 25.45 22.03 36.56 32.65 35.67 35.17 27.29 45.32 36.52	9404 36,5 31,6 2261 2066 57,4 102,6 57,4 102,6 57,4 44,1 77,1 102,6 44,1 177,2 180,3 318,4 117,2 (54,1
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NS NS NS NS NS NS NS NS NS NS	200 5 4 14 4 3 20 5 5 5 7 27 27 4 2 2 2 2 4 2 2 2 2 8 6 4 4 4 4 11 11 2 2 2 2 2 2 2 2 2 3 6 4 4 11 2 7 12 7 12 7 12 7 12 7 12 7 12	3/4*6 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426 3/426	$24t + 1^{+}$ $4^{+} - 10^{+}$ $5^{+} - 9^{+}$ $10^{+} - 9^{+}$ $10^{+} - 9^{+}$ $30^{+} - 9^{+}$ $30^{+} - 9^{+}$ $5^{+} - 3^{+}$ $5^{+} - 3^{+}$ 5	а 	56.17 725 769 64.16 57.96 57.96 57.96 54.95 54.44 4.58 93.44 4.58 93.44 1.67 72.63 36.54 72.63 36.54 72.63 36.54 72.63 25.46 52.47 25.25 27.04	9404 38,5 51,6 225,1 208,8 51,4 192,6 54,4 41,5 54,4 455,5 102,6 44,1 TT,1 102,6 44,1 TT,1 102,6 (34,1) 117,2 (34,1) 117,2 (34,1) 209,4
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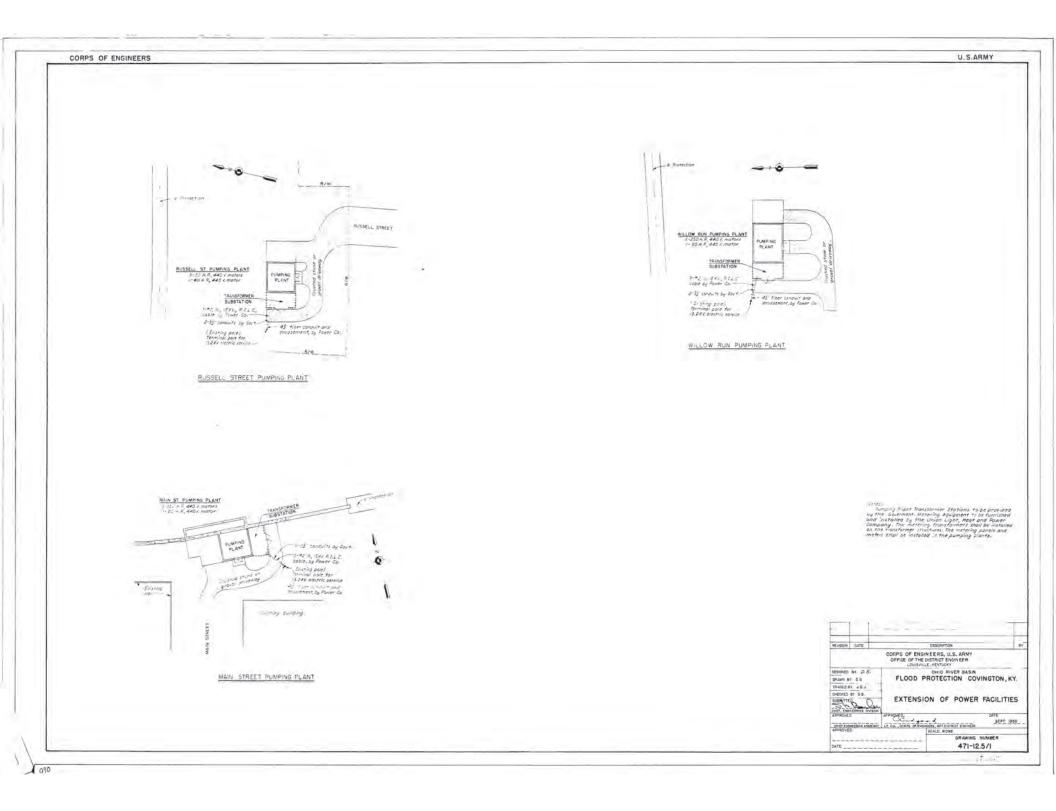
1	HO.	AIZE	LENGTH	BEHDING DIAGRAM	WEIGHT EACH	WEISH
	100		MOTOR	FLOOR BEAMS	1.2.3	100
Att	6	3/4" \$	151-04	STRAIGHT	2255	159.5
162	8	1-1/4*=	241 - 01		27.51	1620.
HBS	8		24"- 0"		103.27	67.6.1
MBA	54		71-81	[r-c] 2-6%	5/2	276.5
MBS	14	s/0 \$	19*- 4*	6.855	2016	282.3
MRG	10			- 10		1.1
			5'- 8'	Har- H-IOVE	2.3	21.3
MBT		7/8-4	24'- 0"	STRAIGHT	4906	56.
MB	9	114	24'- 0"		44.00	101.
MB	2	4°0	24' - 01		9150	165.2
наю	6	1-1/8-9	26-7	284-1 ->	114.38	6863
MBI	23		510*		219	50.4
1	-	ave 4		115	F.(3)	30.0
HBIZ	3	1-4	12-50	Ure at in	53.(3)	99.5
MBIS	3		15 6-	c 11.4.0	36.05	ID6.2
MB-4	3		111+ 7"	10-9"		
				10-9-5	23.67	71.0
MBIS	3		12-5	C 10-9-3	22:30	76,2
PIBIE	3	110	12 - 4"	11-2-3	32.92	96.8
MB 17	3	17 4	19 5"	C 11-3-3	35.85	322.5
15-6	14		41-01	2. 1-2%	1.50	24.0
Hilb	ia	3/8.4	4-2"	P 1 - 34	157	20.6
M820	14	3/614	4.10	7 7 7 - 4M	163	22.8
				92		
Hiszi	13	3/0-0	4-5	9.	166	21.6
10 22		1/2-4	23-07	STRAIGHT	15.84	196.2
-	.9.	7/8-4	22-0-		44.01	404.7
48.74		7/8"+	25'- 8*		#14.01 #2.41	472.2
40.25		5/81-4	7.4.	C 244055	105	
				C 41-9+		107.1
4926	14	1/2" #	996	STRAIGHT	4,62	GAT
-	-		2			
-					-	
				1007		
	1	-	1			
	2.5	1/2.4	8-0-	7-6-7	5.84	122.0
	29 74		8 - 0* 9* - 9*	7-6-3 52 3-ing	5.84 6,51	122.6
22			8 - 0 9 - 9'	7-5'		
22	74	1/2-4	8 - 0" 9" - 9"	-7-6- 3 52 3-102 3-8 8 5-8 8 5-8 8 5-8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6.51 6.%	156.2 506.2
R2 R5	74 44 26	1/2" \$ 1/2" \$ 1/2" \$ 1	8 - 0* 9* - 9* 0* - 5* 22: - 6*	7-5'	6,51 6,%	156.2 506.2 575.6
R2 R5	74	1/2-4	8 - 0* 9* - 9* 0* - 5* 22: - 6*	7-6-3- 52-52-52-174 3-4 3-4 3-4 5-8 5-6-4 5-85- 4 5-85- 4 5-85- 57EA(6)-17 57EA(6)-17	6.51 6.%	156.2 506.2
25 25 24 25	74 44 26	1/2" \$ 1/2" \$ 1/2" \$ 1	8 - 0 9 - 9 1 0 - 5 1 1 22 - 8	7-5' 3 5' 3' 10' 5'-5' 4' 5'-5' 4' 5'-5' 4' 5'-5' 4' 5'-5' 4' 5'-5' 1' 5'-5'	6,51 6,%	156.2 506.2 579.6 450
22 25 25 26	74 44 26 8 2	1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$	8 - 0" 9" - 94 1 0" - 5" 22(- 6" 1' - 5) 3' - 6"	7-6-3- 52-52-52-174 3-4 3-4 3-4 5-8 5-6-4 5-85- 4 5-85- 4 5-85- 57EA(6)-17 57EA(6)-17	6,51 6,% (5,14 7,63 6,%	1562 5062 5756 456 12.7
22 25 25 26	74 44 24 8	1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$	8 - 0" 9" - 94 1 0" - 5" 22(- 6" 1' - 5) 3' - 6"	7-52-3 52-4-37-102 3-4-37-102 5-6-5-14 57EA1647 57EA17 57EA167 57EA167 57EA167 57EA167 57EA17	6,51 6.% 15.14 763	156.2 506.2 579.6 450
25 25 25 25 26 27	74 44 26 8 2	1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$ 1/2" \$	8 - 0 9 - 5 0 - 5 1 22 - 6 1 - 9 9 - 6 3 - 9	7-55-5 52-27-101 2-27-47 8-10-7 8-10-7 5-55-17-57 6-57- 1-57- 6-57- 1-	6,51 6,% (5,14 7,63 6,%	156.2 506.2 575.6 458 12.7
82 85 84 25 86 86 86	74 44 26 8 2 2 2 2	1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$	8 - 0 9 - 5 9 - 5 9 - 5 1 22 - 6 1 9 - 5 9 - 5 1 9 - 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7-50-5 50-20-100 50-20-100 50-20-10 50-20-	6,51 6,% 15,14 7,63 6,95 9,19 3,45	156-2 506-2 505-2 505-2 45-0 12:7 10:4 6/9
82 85 84 25 86 86 86	74 44 25 8 2 2	1/2* \$ 1/2* \$	8 - 0 9 - 94 0 - 54 12 - 87 11 - 99 91 - 64 91 - 64	7-5-5- 5-2-702 # 5-2-702 # 1-52 # 1-52# 1-52 # 1-52 #	6,51 6,96 15.14 763 435 9.19	156.2 506.2 575.6 45.8 12:7
222 23 24 25 26 27 27 28 26 27 27 29	74 44 26 8 2 2 2 2	1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$ 1/2* \$	8 - 0 9 - 94 0 - 54 12 - 87 11 - 99 91 - 64 91 - 64	7.5 € .5 32 20105 32 20105 32 20105 32 20105 312 20105 312 20105 312 20105 312 1-32 3-22 1-32 3-25 1-32 3-25 1-32 3-20 1-32 3-20 1-32 3-20 1-32 3-20 1-32 3-20 1-32	6,51 6,% 15,14 7,63 6,95 9,19 3,45	156-2 506-2 505-2 505-2 45-0 12:7 10:4 6/9
222 25 24 25 26 27 27 29 29 20	74 44 6 2 2 2 2 2 2	1/2* \$ 1/2* \$ 1/	8 - 0 9 - 5 1 0 - 5 1 22 - 6 1 - 5 3 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5	7:50:5 50:00 50:00 30:00	6.51 6.96 15.14 7.63 4.35 3.45 2.12 4.26	156.2 506.2 573.6 450 12.7 10.4 69 4.2 12.6
222 235 24 25 26 27 27 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	74 44 6 2 2 2 2 2 3 3	1/2* \$ 1/2* \$	8 - 0 9' - 8' 1' - 5' 1' - 5' 9' - 6' 5' - 2' 3' - 2' 8' - 5' 8' - 5' 7 - 6'	7.5 € .5 32 20105 32 20105 32 20105 32 20105 312 20105 312 20105 312 20105 312 1-32 3-22 1-32 3-25 1-32 3-25 1-32 3-20 1-32 3-20 1-32 3-20 1-32 3-20 1-32 3-20 1-32	6.51 6.96 5.14 7.63 6.35 7.19 3.45 2.12 4.26 6.46	1562 5062 575.6 458 12.7 18.4 69 42 12.6 15.4
23	74 44 6 2 2 2 2 2 3 3	1/2* \$ 1/2* \$ 1/	8 - 0 9' - 8' 1' - 5' 1' - 5' 9' - 6' 5' - 2' 3' - 2' 8' - 5' 8' - 5' 7 - 6'	7:52:5 30/ 2000 2000 <td>6.51 6.96 15.14 7.63 4.35 3.45 2.12 4.26</td> <td>156.2 506.2 579.6 450 12.7 10.4 6/9 4.2 12.6</td>	6.51 6.96 15.14 7.63 4.35 3.45 2.12 4.26	156.2 506.2 579.6 450 12.7 10.4 6/9 4.2 12.6
222 235 24 25 26 27 27 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	74 44 6 2 2 2 2 2 3 3	1/2* \$ 1/2* \$	$\theta = 0^{-1}$ $\theta = 0^{-1}$	7:50 - 5 30 g ≠ 0.000 10 g ≠ 0.000	6.51 6.96 5.14 7.63 6.35 7.19 3.45 2.12 4.26 6.46	1562 5062 575.6 458 12.7 18.4 69 42 12.6 15.4
222 225 226 226 227 229 229 229 229 229 229 229 229 229	74 44 6 2 2 2 2 2 3 3 3 3 3 3	1/2* \$ 1/2* \$ 1/	$\hat{\mathcal{C}} = 0^{\circ}$ $\hat{\mathcal{C}} = -5^{\circ}$ $\hat{\mathcal{C}} = -5^{\circ}$ $\mathcal{C$	7:52:5 90 20:001 20:001 20:001 20:001 20:001 20:001 20:001 90:001 10:97 <td< td=""><td>6.51 6.% 5.14 763 9.16 3.45 2.12 4.25 6.46 3.20 2.320</td><td>1562 3062 573.6 450 12.7 16.4 450 42. 12.4 42. 12.4 2.6 7.4</td></td<>	6.51 6.% 5.14 763 9.16 3.45 2.12 4.25 6.46 3.20 2.320	1562 3062 573.6 450 12.7 16.4 450 42. 12.4 42. 12.4 2.6 7.4
222 25 26 26 27 29 29 29 29 29 29 29 29 29 29 29 29 29	74 44 6 2 2 2 2 2 3 3 3 3 3 3	1/2* ¢ 1/2* ¢ 1/	E = 0 5 = 5 ⁴ (0 = 5 ⁴) (0 = 5 ⁴) (1 = 5 ⁴) (7:50 - 5 30 g ≠ 0.000 10 g ≠ 0.000	6,51 6,96 16,14 763 9,19 3,45 2,12 4,26 6,46 3,20 3,30	156-2 306-2 309-6 459 12:7 10:4 699 4.2 12:4 10:4 10:4 10:4 10:4 10:4 10:4 10:4 10

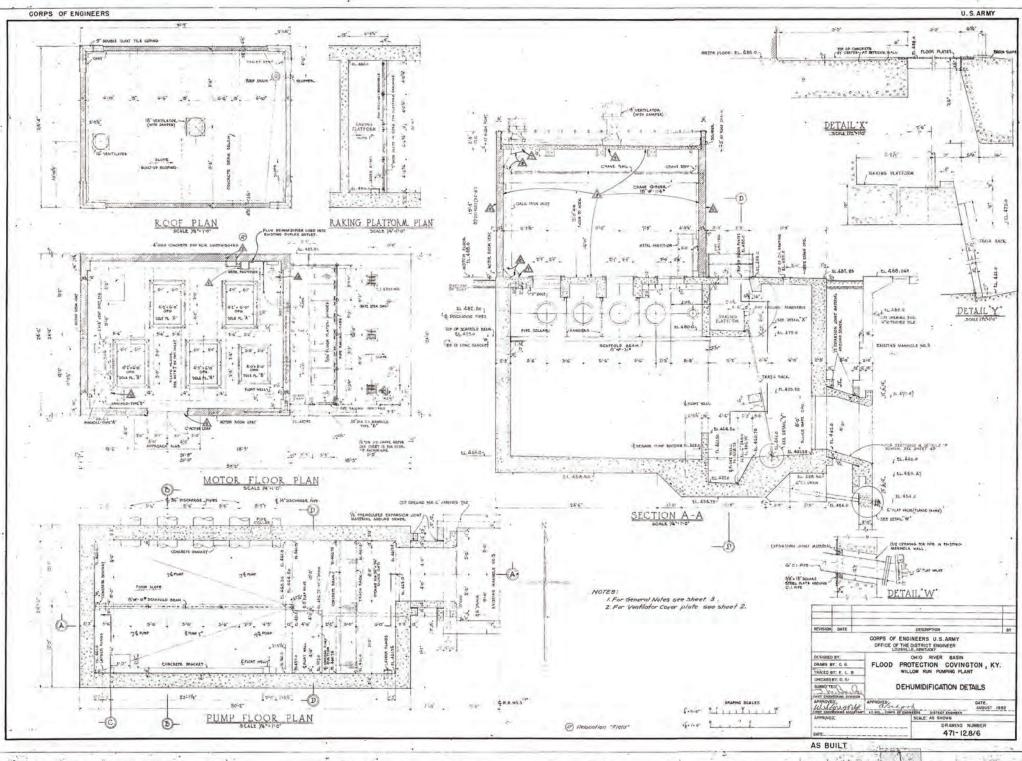
RAT	NO REG		LEMETH	BENDINA DIAS	CAM	WENH	TOTAL WELANT
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_	_	-	1		_		
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wi	3,		9 34'- 8*	STRAIGHT		52.0	11710.
WZ.	.54		¢ 29' - 10*			70.76	
W3	38		26'- 9-		-	142.12	7500.5
W4	- 2		s 30' - 8!			162.95	848
мS	3		= 28·- (0*			153,17	306.5
46	21	1-1/4"	0 26'- 5'		-	140.37	
W7	55	3/44	24 - 3		1.1	36,42	1930.0
WB	77	1.0	181- 01	3-0-	0	61.20	4712.4
1.1	1	-	1	10'-0*			
W9	22	1+1/4	19-3	STEALGHT	-	104.93	25085
WID	13	1-1/4*	12'- 2'			64,65	840.5
wii	64	7.44	24 - 2"			64.08	
W12	28	1.4	29-01			71.45	
WIB	8	10		· · · ·		3.35	106.8
NI4	8	143				2409	192.2
115	24	140			-	29.87	794.9
NIG	iz	1-1		*		18.07	224.9
NI7	Z	142		18-	-	4675	93.5
-	-			5-9-	-	4-01-	
ANS.	12	1.154	131-10	9.2.	-	47.02	3642
	1	-	1	10-0-	-	411-4	
(m)	2	5.44%	10:01	STRAKENT	- 1	24.70	49.6
V20	28	3/4 1	17-31	S. Color	+	25.91	715.5
124	27	2/11	PH		-	3180	058.6
NZZ	26	242.4	21' - 2' 13' - 0" 14'- 9'	*	-	19.55	507.6
		0/4*9	13 - Qu		-		
123	4	1.9	14-91		-	50.15	200.6
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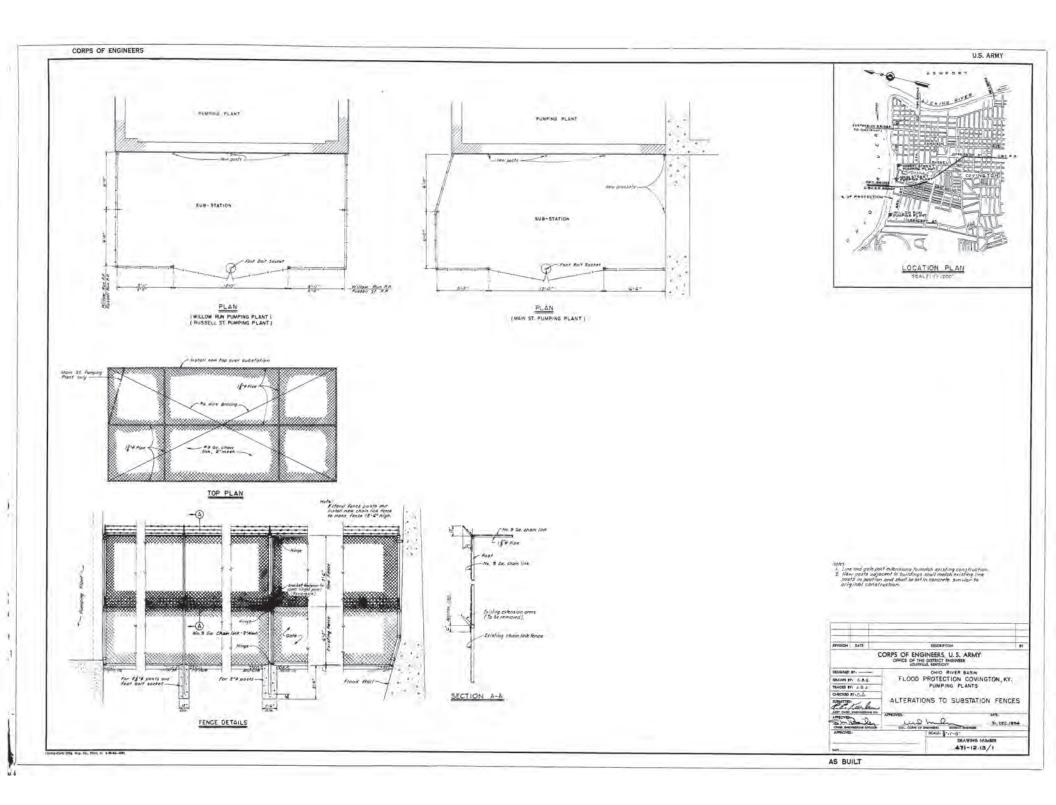
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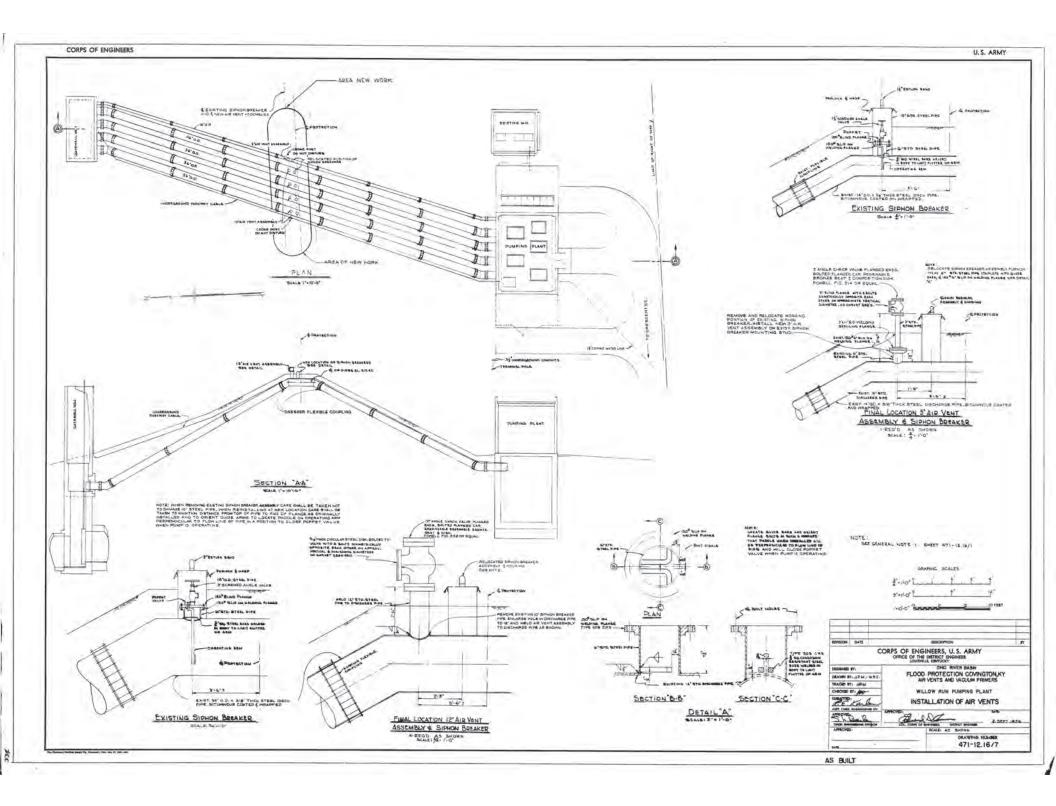
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MEETING DOCUMENTATION

Project: I-71/I-75 (Brent Spence Br.) Willow Run Storm Water Separation Study

Location: Virtual – Teams Meeting

Meeting Date: February 21, 2022

Subject: Alternative Review Meeting

ATTENDEES

Gary Valentine Stacee Hans Tim Robinson David Lanham Janet Woods KYTC – CO KYTC – D6 KYTC – CO Palmer Engineering Palmer Engineering gvalentine@ky.gov Stacee.hans@ky.gov tims.robinson@ky.gov dlanham@palmernet.com JWoods@palmernet.com

EXHIBITS

• Microstation DGN files

MEETING SUMMARY

David Lanham gave an overview of the study area. He reviewed the existing drainage system from the Kyles Lane interchange to the Ohio River, including detention basins, where storm water leaves the interstate drainage system, the location and operation of the Willow Run combined sewer trunk line, its major branches, and its low-flow diversion system.

David then reviewed the proposed alternatives. Alt 1 constructs a separate storm sewer system from approximately 16th Street northward toward the river. Alt 2 builds upon Alt 1, and it constructs a separate storm sewer system from the Kyles Lane interchange northward toward the river. The roadway drainage inlets were all placed based on the proposed DTMs and proposed cross sections, using actual low points, super transitions, etc. Judgements were made on spread, but in many areas, the maximum length of pipe controlled the spacing of inlets. Exact locations of bridge deck drains were not determined, but runoff from bridge decks was accounted for in the flow calculations.

There is a low area, approximately 1 acre in size near the intersection of Bullock and 12th Street that is not be intercepted by the proposed separate storm sewer system. Doing so would have caused the proposed storm sewer to be too low and would create a conflict with the Willow Run combined sewer downstream, where it was necessary to cross the existing Willow Run combined sewer with the proposed storm sewer trunk line

The trunk line in Alt 1 is located primarily under Jillians Way, which also helps navigate the low area of Goebel Park since that section of Jillians Way will be built up with retaining wall. The exact layout of where it cross back to the west side of the interstate, near the floodwall, will have to be fine-tuned during later design phases based on bridge pier locations.

Segments of the existing combined sewer and its low-flow diversion will need to be reconstructed to avoid conflicts with the proposed roadway and bridge layout. Side streets will need to be reconnected to these relocated systems

The designed outflows from the existing basins are unknown. After discussing with Tim prior to this meeting, it was decided to roughly assume that the detention basins may attenuate 25% of the peak flow as compared to no basin at all. This may still be overly conservative, considering the size of the pipes in the outflow structures at the basins. But, that approach was used to size the pipes downstream of the basins at Lt Sta 478+00 and Lt Sta 490+00. For the basin at Lt Sta 518+00, that approach was determined to be too conservative. The size of that watershed (221 acres plus the upstream interchange watershed flowing to it) yielded flows that were far too high for the existing 36" pipe in the outflow system. Therefore, at that location an outflow was assumed, and it was based on the capacity of the existing 36" pipe at its existing slope. This assumption may be revisited, since Alt 2 sends more of the upstream watershed toward this basin.

Both Alts tie into the existing pump station and assume that it will need to be modified. The thinking at this point, although it is not known for certain, is that modifying the pump station versus constructing a separate one just for the proposed separate storm sewer system may make it easier to work through the Section 408 permitting process. This will be discussed in more detail with SD1 during a subsequent meeting.

Gary said that Palmer should focus the efforts going forward on Alt 2, as the preferred alternative to present to the City of Covington and SD1.

Next Steps:

- Palmer will prepare a cost estimate for Alt 2.
 - Note: this needs to also account for the relocated existing sewers.
- Palmer will quantify the area that Alt 2 removes from the Willow Run combined sewer system, to help with presenting the information to the City and SD1; and Palmer will quantify the interstate area that currently drains into the exiting combined sewer system.
- Stacee will set up a meeting with the City and SD1.



MEETING DOCUMENTATION

Project: I-71/I-75 (Brent Spence Br.) Willow Run Storm Water Separation Study
Location: Hybrid – KYTC District 6, 1st Floor Conference Room; and Virtual Option – Teams
Meeting Date: March 3, 2022
Subject: Local Officials Review Meeting

ATTENDEES

Joe Meyer
Stacee Hans
Tim Robinson
Gary Valentine
David Lanham
Diana Martin
Rick Record
Phil Sebastian
Lydia Watkins
Juan Carrizo
Josh Epperson

City of Covington - Mayor KYTC - D6 KYTC - C.O. Drainage KYTC - C.O. – Exec. Advisor Palmer Engineering RL Record RL Record SD1 SD1 VS Engineering VS Engineering

jumeyer@covingtonky.gov Stacee.Hans@ky.gov tims.robinson@ky.gov gvalentine@ky.gov dlanham@palmernet.com dmartin@rlrecord.com rrecord@rlrecord.com psebastian@sd1.org lwatkins@sd1.org jcarrizo@vsengineering.com jepperson@vsengineering.com

EXHIBITS

• Microstation DGN files

MEETING SUMMARY

After introductions, Gary reviewed the City's concerns with the 2012 drainage layout. The goal at that time was a net-zero flow change in the existing Willow Run combined sewer system. The Cabinet's goal with our updated layout was to address the City's concerns by developing a new drainage layout. Palmer Engineering was contracted to study the area and develop the revised drainage layout.

David Lanham reviewed the City's specific requests detailed in their Jan. 5, 2022 letter to the Cabinet, and then highlighted those areas in Google Earth for reference. One of the main points was the City's request to separate storm water from the combined sewer system from 16th Street north to the Ohio River along the I-75 corridor. The Cabinet developed a proposed drainage layout that not only achieved that goal, but went beyond by extending the separation concept upstream to the Willow Run watershed boundary at Kyles Lane.

David gave an overview of the study area. He reviewed the existing drainage system from the Kyles Lane interchange to the Ohio River, including detention basins, where storm water leaves the interstate drainage system and flows eventually into the combined system; the location and operation of the Willow Run combined sewer trunk line, its major branches, and its low-flow diversion system.

David then reviewed the proposed drainage alternative, which would construct a separate storm sewer system from the Kyles Lane interchange northward toward the river. The roadway drainage inlets were all placed based on the proposed DTMs and proposed cross sections, using actual low points, super transitions, etc. Exact locations of bridge deck drains were not determined, but runoff from bridge decks was accounted for in the flow calculations.

There is a low area, approximately 1 acre in size near the intersection of Bullock and 12th Street that is not being intercepted by the proposed separate storm sewer system. Doing so would have caused the proposed storm sewer to be too low and would create a conflict with the Willow Run combined sewer downstream, where it was necessary to cross the existing Willow Run combined sewer with the proposed storm sewer trunk line

The trunk line is located mostly along the west side of the interstate from Kyles Lane to just south of 12th Street, where it crosses to the east side. It then is located under Jillians Way, which also helps navigate the low area of Goebel Park since that section of Jillians Way will be built up with a retaining wall. The exact layout of where it cross back to the west side of the interstate, near the floodwall, will have to be fine-tuned during later design phases based on bridge pier locations.

Segments of the existing combined sewer and its low-flow diversion will need to be reconstructed to avoid conflicts with the proposed roadway and bridge layout. Side streets will need to be reconnected to these relocated systems. Gary stated that the Cabinet would be willing to partner with SD1 for relocation and sizing of the relocated segments.

The existing basins are proposed to be modified when impacted by the project, to replace any lost storage. The designed outflows from the existing basins are not known, and some assumptions were made to assume an outflow for the purpose of sizing the proposed pipes. But, for the basins where the outflow leaves the interstate area, the proposed flows are reduced because of area being removed from their watershed. And for the basins where the outflow is contained in the proposed separate storm sewer, the outflow from the basin will only affect the proposed pipe sizes.

The total acreage removed from the combined sewer system, which would now be drainage via the proposed separate storm sewer system is estimated to be 467 acres (170 acres of impervious area and 297 acres of pervious area).

The proposed storm sewer system ties into the existing pump station and assumes that it may need to be modified. However, we are not changing the total watershed that drains to the pump station. We only be redirecting the separated storm sewer runoff to reach the pump station, rather than it reaching the pump station via the combined sewer system. Subsequent to the meeting, the project team decided to set up a meeting with the USACE and SD1 to discuss potential modifications to the pump station, and to discuss the Section 408 permitting process.

Josh asked if SD1 has a hydraulic model for the existing system. Lydia and Phil said it is a part of the Bromley model, and also that SD1 has record plans for the pump station.

SD1 currently is planning to install real-time controls in the basins along the interstate to regulate flows differently for low-flow and high-flow events. Our proposed drainage could be a benefit to SD1 by negating the need for that in basins that would be separated from the combined sewer system, and by reducing flows to those that would still drain toward the combined sewer system.

It is not expected that the construction will directly impact the pump station, besides the potential modifications mentioned above.

Mayor Meyer asked if this plan would help with the flooding along Highland and Euclid. The team discussed how the proposed plan would reduce the storm water runoff that reaches those problem areas.

Josh asked if DGN files could be shared, which the Cabinet agreed to. Josh and David will coordinate about that.

Subsequent to the meeting, Rick asked for the PDF plots of the proposed layout.

Next Steps:

- Palmer will provide PDFs to Rick and DGNs to Josh.
- Palmer will contact SD1 to obtain the record plans, and any other pertinent info, for the existing pump station.
- Palmer will contact the USACE and work to set up a meeting with them, SD1, and the project's permitting team.

Page 3 of 3



MEETING DOCUMENTATION

Project: I-71/I-75 (Brent Spence Br.) Willow Run Storm Water Separation Study

Location: Virtual – Teams

Meeting Date: March 17, 2022

Subject: Section 408 Coordination Meeting

ATTENDEES

Richard Anthony
Andrew Brooks
Stacee Hans
David Lanham
Gary Valentine
David Waldner

City of Covington USACE (Levee Safety POC) KYTC - D6 Palmer Engineering KYTC - C.O. – Exec. Advisor Palmer Engineering <u>Oliver.Anthony@covingtonky.gov</u> <u>Andrew.T.Brooks@usace.army.mil</u> <u>Stacee.Hans@ky.gov</u> <u>dlanham@palmernet.com</u> <u>gvalentine@ky.gov</u> dwaldner@palmernet.com

EXHIBITS

• N/A

MEETING SUMMARY

After introductions, David gave a brief overview of the project and its history. The goal of this meeting is to discuss the requirements for obtaining a Section 408 permit, since KYTC's project team is unfamiliar with the process.

The current layout for the project does not directly impact the floodwall, as it will be spanned by bridges similar to the existing condition. Impacts to the associated pump station are possible, however. The proposed separated storm sewer trunk line will tie in at the pump station. The exact details of that tie-in have not been developed at this time. Flow rates at the pump station could be affected by the separated storm water, by changing the timing of runoff reaching the pump station. However, the total watershed boundary for the pump station is not changing.

The levee, floodwall, and pump station system are owned by the City of Covington. They are operated and maintained by SD1.

The Section 408 application package will consist of the permit application, plans (showing easements), specifications, and an H&H report. The H&H report should focus on the flows as they reach the pump station and the criteria used to determine that. The application form should include a summary of the project. The form will require Richard's signature for the City of

Covington as the sponsor, a signature by KYTC as the applicant, and then a signature by the Corps when approved.

During their review, the Corps will be interested in seeing that there are no impacts that cause additional ponding on the landside of the system. Their ROW section will also review access, staging areas, etc. in the vicinity of the floodwall as part of the application package. It is preferable to maintain a 15-foot buffer from the levee and floodwall during construction.

The review process should be expected to take at least 120 days. There is an initial 30-day introductory review period. After the completion of the review period, the technical review begins and takes 90 days. However, any questions, requests for clarification/information, or general back-and-forth correspondence pauses the clock for the technical review period. So, that could cause the review period to take longer than 90 days.

Richard requested a copy of the preliminary drainage layout, which David provided by email after the meeting.

Also after the meeting, Andrew provided a copy of the 408 application form and the document that goes into detail about the levee alteration process. David will include those documents with this meeting summary for KYTC.

Next Steps:

- The information from this meeting will be used to develop the design-build RFP
- During final design, the H&H team should coordinate with the City of Covington and SD1 regarding design flow rates, their effect on the H&H model for the levee system, and potential modifications to the pump station.