

Brent Spence Bridge Replacement/Rehabilitation Project



Air Quality Technical Report: Carbon Monoxide

PID No. 75119
HAM-71/75-0.00/0.22
KYTC Project Item No. 6-17

November 2010



Prepared by:



Disposition of Comments
Air Quality Technical Report
Brent Spence Bridge Replacement/Rehabilitation Project

No.	Comment	Response
1	<p>Because the design year ADT is >140,000, this project is in the “higher potential of MSAT effect” category and a Quantitative MSAT Analysis is required. Please have the consultant follow the guidance found on the following link. http://www.dot.state.oh.us/Divisions/TransssSysDev/Environment/NEPA_policy_issues/AIR_QUALITY/Documents/ODOT%20Technical%20Guidance%20for%20Analysis%20Mobile%20Source%20Air%20Toxics.PDF</p>	<p>The link provides references to FHWA’s February 3, 2006 guidance. FHWA issues an Interim Guidance Update on MSAT analysis in NEPA documents on September 30, 2009. The link to this guidance can be found at: http://www.fhwa.dot.gov/environment/airtoxic/100109guidmem.htm</p> <p>While many aspects of the updated guidance echoes the 2006 guidance there are a few important differences. They include: MSAT to be analyzed – The 2006 guidance listed 6 priority MSAT, as defined by EPA. EPA no longer supports this. The new FHWA guidance refers to 7 compounds that EPA identified as having significant contributions from mobile sources. The FHWA considers these the priority mobile source air toxics.</p> <ul style="list-style-type: none"> • Reference language and figures have been updated to reflect impacts of the new EPA rules on future MSAT emissions and VMT growth. <p>It has been our experience that running FHWA’s EMIT model on regional traffic data is the appropriate analysis procedure for projects with “higher potential of MSAT effects”. EMIT however, does not currently reflect all the MSAT referenced in the 2009 update. To estimate all the MSAT of concern, MOBILE6 will be run outside of the EMIT model to obtain emission factors for POM (which requires the summation of 15 individual MSAT) and naphthalene. These emission factors will be applied to the regional VMT to obtain build and no build emission burden estimates.</p>
2	<p>Because the project involves design year ADT>125,000 and diesel truck volume > 8% of the ADT, a PM2.5 Hotspot Analysis is required to be prepared for the project.</p>	<p>A PM2.5 Hotspot Analysis was completed for the project.</p>

No.	Comment	Response
3	Relative to CO, state that a CO analysis was conducted because "The constructed project will result in an increase in the ADT of more than 10,000 vehicles within 10 years of project completion date. Also, the project involves a new project right-of-way that will have an ADT of more than 20,000 vehicles within 10 years of construction. Hence, a carbon monoxide analysis is required." CO analysis should be a separate report under a separate cover.	The text was revised as requested. A separate report was prepared for the CO analysis.
4	CO, PM2.5 and MSAT analyses should be separate reports under separate covers. Please have the consultant separate these out and resubmit.	The report was revised into three separate reports for CO, PM2.5 and MSAT.

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1.0 INTRODUCTION

This Air Quality Technical Report has been prepared in support of the Brent Spence Bridge Replacement/Rehabilitation Project. The objective of this report is to evaluate the project's potential air quality impacts within the study area. This includes the following:

- Evaluate the project's impact on regional air quality levels;
- Evaluate whether this project will cause or contribute to a new localized exceedance of carbon monoxide (CO) ambient air quality standards ; and
- Evaluate the construction emissions of the project.

1.1 Project Description

Interstate 75 (I-75) within the Greater Cincinnati/Northern Kentucky region; is a major thoroughfare for local and regional mobility. Locally, it connects to I-71, I-74 and US Route 50. The Brent Spence Bridge provides an interstate connection over the Ohio River and carries both I-71 and I-75 traffic (Exhibit 1). The bridge also facilitates local travel by providing access to downtown Cincinnati, Ohio and Covington, Kentucky. Safety, congestion and geometric problems exist on the structure and its approaches. The Brent Spence Bridge, which opened to traffic in 1963, was designed to carry 80,000 vehicles per day. Currently, approximately 160,000 vehicles per day use the Brent Spence Bridge and traffic volumes are projected to increase to 200,000 vehicles per day in 2035.

The I-75 corridor within the Greater Cincinnati/Northern Kentucky region is experiencing problems, which threaten the overall efficiency and flexibility of this vital trade corridor. Areas of concern include, but are not limited to, growing demand and congestion, land use pressures, environmental concerns, adequate safety margins, and maintaining linkage in key mobility, trade, and national defense highways.

The I-75 corridor has been the subject of numerous planning and engineering studies over the years and is a strategic link in the region's and the nation's highway network. As such, the Ohio Department of Transportation (ODOT) and the Kentucky Transportation Cabinet (KYTC), in cooperation with the Federal Highway Administration (FHWA), are proposing to improve the operational characteristics of I-75 and the Brent Spence Bridge in the Greater Cincinnati/Northern Kentucky region through a major transportation project.

1.2 Purpose and Need

The Brent Spence Bridge Replacement/Rehabilitation Project is intended to improve the operational characteristics within the I-71/I-75 corridor for both local and through traffic. In the Greater Cincinnati/Northern Kentucky region, the I-71/I-75 corridor suffers from congestion and safety-related issues as a result of inadequate capacity to accommodate current traffic demand. The objectives of this project are to:

- Improve traffic flow and level of service;
- Improve safety;
- Correct geometric deficiencies; and
- Maintain connections to key regional and national transportation corridors.

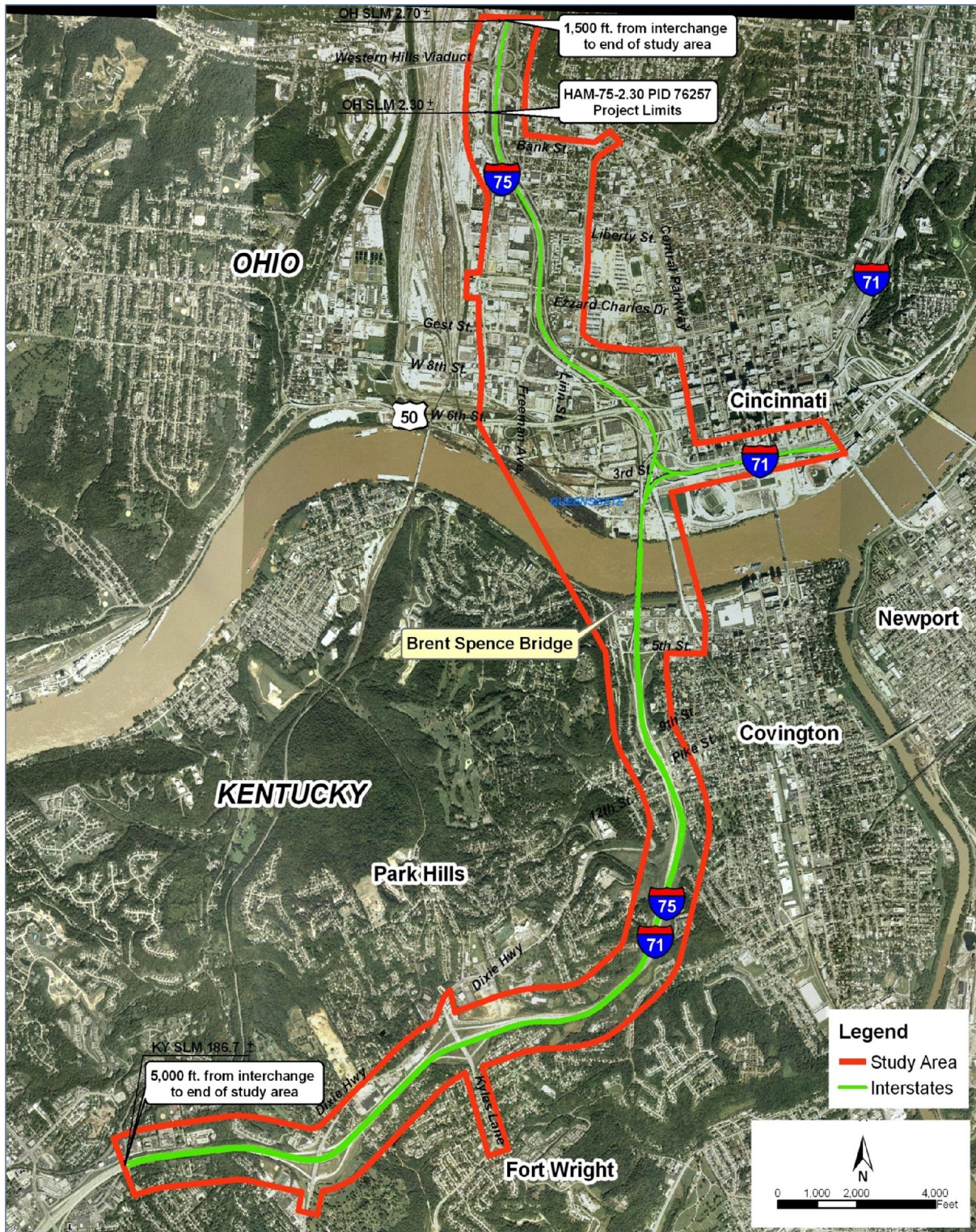


Exhibit 1. Project Study Area Limits

1.3 Study Corridor

The overall project corridor is located along a 7.8-mile segment of I-75 within the Commonwealth of Kentucky (state line mile 186.7) and the State of Ohio (state line mile 2.7). The southern limit of the project is 5,000 feet south of the midpoint of the Dixie Highway Interchange on I-71/I-75 in Fort Wright, south of Covington, Kentucky. The northern limit of the project is 1,500 feet north of the midpoint of the Western Hills Viaduct Interchange on I-75 in Cincinnati, Ohio. The eastern and western limits of the study area generally follow the existing alignment of I-75. The project study area limits for which the air analysis was completed is depicted in Exhibit 1.

1.4 Feasible Alternatives

The Brent Spence Bridge Rehabilitation/Reconstruction project is currently in Steps 6 and 7 of ODOT's Project Development Process (PDP). Two feasible alternatives and the No Build Alternative are being developed and studied in more detail. The two alternatives selected for the Step 6 and 7 are Alternative E and Alternative I, which is a combination of Conceptual Alternatives C and D from Step 5 of the PDP.

1.4.1 Alternative E

Alternative E utilizes the existing I-71/I-75 alignment from the southern project limits at the Dixie Highway Interchange north to the Kyles Lane Interchange. The Dixie Highway and Kyles Lane interchanges will be modified slightly to accommodate a Collector-Distributor (C-D) roadway, which will be constructed along both sides of I-71/I-75 between the two interchanges. North of the Kyles Lane Interchange, the alignment shifts to the west to accommodate additional I-71/I-75 travel lanes. Between Kyles Lane and KY 12th Street, six lanes will be provided in each direction for a total of 12 travel lanes.

Near KY 12th Street, the northbound alignment separates into two routes; one for interstate traffic and one for a local C-D roadway. Between Pike Street and KY 9th Street, the interstate separates into I-71 and I-75 only routes. The C-D roadway will carry local traffic northbound and provide access to Covington at KY 12th and 5th streets and access from KY 9th and 4th streets. The southbound C-D roadway will carry traffic from Ohio over I-71/I-75 and provide access to both the interstate and into Covington at KY 9th Street.

A new double deck bridge will be built just west of the existing Brent Spence Bridge to carry northbound and southbound I-71 and I-75 traffic. On the upper deck, I-71 southbound will have three lanes and I-71 northbound will have two lanes. On the lower deck, I-75 will have three northbound and three southbound lanes. The existing Brent Spence Bridge will be rehabilitated to carry northbound and southbound local traffic with two lanes in the southbound direction and three lanes in the northbound direction.

In Ohio, Alternative E reconfigures I-75 through the I-71/I-75/US 50 Interchange and eliminates some of the existing access points along I-75. Existing ramps to I-71, US 50 and downtown Cincinnati will be reconfigured. The existing direct connections between I-75 to westbound and from eastbound US 50 will be maintained in Alternative E. US 50 will be reconfigured to eliminate left-hand entrances and exits. The OH 5th Street overpass will be eliminated and the 6th Street Expressway will be reconfigured as a two-way, six-lane elevated roadway with a new signalized intersection for US 50 access and egress. Access between southbound I-71 (Fort

Washington Way) and northbound I-75 will be provided near OH 9th Street as a direct connection. Both I-75 southbound and US 50 (Sixth Street Expressway) will have access to northbound I-71 (Fort Washington Way). Access to OH 3rd Street at the Clay Wade Bailey Bridge intersection will also be available via the I-75 southbound to northbound I-71 (Fort Washington Way) connection.

A local C-D roadway will carry local traffic northbound from the existing Brent Spence Bridge and provide access to OH 2nd, 5th, and 9th streets, Winchell Avenue and access from OH 4th before reconnecting to I-75 just south of the Linn Street overpass. The northbound ramps from OH 6th and 9th Street to I-75 will be removed requiring traffic from these points to utilize a new local roadway parallel to I-75 and access the interstate at Bank Street. Southbound I-75 traffic will separate from the local C-D roadway near Ezzard Charles Drive. The southbound C-D roadway will carry traffic over I-75 to OH 7th Street, allowing traffic to either; access downtown at 7th Street, travel south to OH 5th and 2nd streets, or travel across the existing Brent Spence Bridge into Covington. Access to the local southbound C-D roadway will be provided at Western Avenue and at OH 4th and 8th streets.

Alternative E also improves Western and Winchell avenues to facilitate traffic flow and increase capacity. The ramps to Western Avenue and from Winchell Avenue just north of Ezzard Charles Drive will be removed. The ramp from Freeman Avenue to I-75 northbound and the ramp from I-75 southbound to Freeman will remain. Between Ezzard Charles Drive and Western Hills Viaduct, southbound I-75 will have six lanes, northbound I-75 will have five lanes, and one auxiliary lane to the Western Hills Viaduct. The Western Hills Viaduct Interchange will be reconfigured to provide a full movement interchange. The improved interchange will be a Single Point Urban Interchange (SPUI) design.

1.4.2 Alternative I

Alternative I utilizes the existing I-71/I-75 alignment from the southern project limits at the Dixie Highway Interchange north to the Kyles Lane Interchange. The Dixie Highway and Kyles Lane interchanges will be modified slightly to accommodate a connector-distributor (C-D) roadway, which will be constructed along both sides of I-71/I-75 between the two interchanges. North of the Kyles Lane Interchange, the alignment shifts to the west to accommodate additional I-71/I-75 travel lanes. Between Kyles Lane and KY 12th Street, six lanes will be provided in each direction for a total of 12 travel lanes. Near KY 12th Street, the alignment separates into three routes for I-71, I-75 and a local C-D roadway.

In Alternative I, access into Covington from the interstate will be provided by the local C-D roadway; at KY 12th Street for northbound traffic and at KY 5th and 9th streets for southbound traffic. Direct access to I-71 from Covington will be provided at KY 9th Street with traffic to I-75 northbound using the C-D roadway through downtown Cincinnati and connecting at the Ezzard Charles merge. Access for southbound interstate traffic is located at KY 12th Street. Access from Covington to downtown Cincinnati will be provided by the C-D roadway from KY 9th and 4th streets. Bullock Street will be extended north from Pike Street to KY 9th, 5th, and 4th streets and Jillian's Way will be extended north from Pike Street to KY 9th and 5th streets.

A new double deck bridge will be built just west of the existing Brent Spence Bridge to carry northbound and southbound I-75 (three lanes in each direction), two lanes for southbound I-71 and three lanes for southbound local traffic. The existing Brent Spence Bridge will be rehabilitated to carry two lanes for northbound I-71 and three lanes for northbound local traffic.

Alternative I re-configures I-75 through the I-71/I-75/US 50 Interchange and eliminates all access to and from I-75 from KY 12th Street to the US 50/6th Street overpass in the northbound direction. Alternative I also eliminates access to and from I-75 southbound between KY 12th Street and the Freeman Avenue exit.

In Ohio, a local C-D roadway will be constructed along both sides of I-75. The local northbound C-D roadway will carry local traffic from the existing bridge and provide access ramps to OH 2nd Street, I-71 northbound, US 50 westbound, OH 5th Street, and Winchell Avenue before reconnecting to I-75 just south of Ezzard Charles Drive. The northbound ramps from OH 6th and 9th streets to I-75 will be removed requiring traffic from these three points to utilize a new local roadway parallel to the northbound C-D roadway for access to I-75 around the Western Hills Viaduct Interchange. The northbound ramps from OH 4th Street will utilize the new local northbound C-D roadway for access to I-75. The southbound C-D roadway begins near the Ezzard Charles Drive overpass and carries both downtown Covington and Cincinnati traffic. The southbound C-D roadway will provide access to OH 7th, 5th, 3rd, and 2nd streets, as well as connecting to access ramps from Western Avenue, OH 9th Street, and US 50 eastbound. The C-D roadway will continue south over the new bridge into Covington.

Between Ezzard Charles Drive and the Western Hills Viaduct, northbound I-75 will have five lanes and southbound I-75 will have six lanes, for a total of 11 travel lanes. The ramps to Western Avenue and from Winchell Avenue just north of Ezzard Charles Drive to the Interstate will be eliminated. The southbound ramp to Freeman Avenue and the northbound ramp from Freeman Avenue to I-75 will remain. Alternative I also improves Western and Winchell avenues to facilitate traffic flow and increase capacity. Ramps to Western Avenue and from Winchell Avenue will be provided around the Western Hills Viaduct Interchange, which will be reconfigured to be a tight diamond design.

1.4.3 No Build Alternative

The No Build Alternative consists of minor, short-term safety and maintenance improvements to the Brent Spence Bridge and I-75 corridor, which would maintain continuing operations. The No Build Alternative does not meet the Purpose and Need goals; however, this alternative will be carried forward as a baseline for evaluation of the feasible alternatives.

2.0 EXISTING CONDITIONS

“Air Pollution” is a general term that refers to one or more chemical substances that degrade the quality of the atmosphere. Individual air pollutants degrade the atmosphere by reducing visibility, damaging property, reducing the productivity or vigor of crops or natural vegetation, and/or reducing human or animal health. Air quality is a term used to describe the amount of air pollution the public is exposed to.

Air quality in the United States is governed by the Federal Clean Air Act (CAA) and is administered by the United States Environmental Protection Agency (USEPA).

2.1 United States Environmental Protection Agency

The USEPA is responsible for establishing the National Ambient Air Quality Standards (NAAQS) and enforcing the CAA, and regulates emission sources, such as aircraft, ships, and certain types of locomotives, under the exclusive authority of the federal government. The USEPA also has jurisdiction over emission sources outside state waters (e.g., beyond the outer continental shelf) and establishes various emission standards.

2.2 Clean Air Act Amendments of 1990

The Clean Air Act Amendments (CAAA) of 1990 direct the USEPA to implement environmental policies and regulations that will ensure acceptable levels of air quality.

Under the CAAA, a project cannot:

- Cause or contribute to any new violation of any NAAQS in any area;
- Increase the frequency or severity of any existing violation of any NAAQS in any area; or
- Delay timely attainment of any NAAQS or any required interim emission reductions or other milestones in any area.

2.3 National and State Ambient Air Quality Standards

As required by the CAA, NAAQS have been established for six major air pollutants. These pollutants are: CO, nitrogen dioxide (NO₂), ozone (O₃), particulate matter (PM₁₀ and PM_{2.5}), sulfur dioxide (SO₂), and lead (Pb). These standards are summarized in Table 1. The “primary” standards have been established to protect the public health. The “secondary” standards are intended to protect the nation's welfare and account for air pollutant effects on soil, water, visibility, materials, vegetation and other aspects of the general welfare.

2.4 Ambient Air Quality Data

2.4.1 Local Meteorology

The proposed project is located in the Greater Cincinnati / Northern Kentucky region. The study area is located within the northern limit of the humid subtropical climate and the southern limit of

Table 1. National Ambient Air Quality Standards.

Pollutant	Primary Standards		Secondary Standards	
	Level	Averaging Time	Level	Averaging Time
Carbon Monoxide	9 ppm (10 mg/m ³)	8-hour ⁽¹⁾	None	
	35 ppm (40 mg/m ³)	1-hour ⁽¹⁾		
Lead	0.15 µg/m ³ ⁽²⁾	Rolling 3-Month Average	Same as Primary	
	1.5 µg/m ³	Quarterly Average	Same as Primary	
Nitrogen Dioxide	0.053 ppm (100 µg/m ³)	Annual (Arithmetic Mean)	Same as Primary	
	0.100 ppm	1-hour ⁽³⁾	None	
Particulate Matter (PM ₁₀)	150 µg/m ³	24-hour ⁽⁴⁾	Same as Primary	
Particulate Matter (PM _{2.5})	15.0 µg/m ³	Annual ⁽⁵⁾ (Arithmetic Mean)	Same as Primary	
	35 µg/m ³	24-hour ⁽⁶⁾	Same as Primary	
Ozone	0.075 ppm (2008 std)	8-hour ⁽⁷⁾	Same as Primary	
	0.08 ppm (1997 std)	8-hour ⁽⁸⁾	Same as Primary	
	0.12 ppm	1-hour ⁽⁹⁾	Same as Primary	
Sulfur Dioxide	0.03 ppm	Annual (Arithmetic Mean)	0.5 ppm (1300 µg/m ³)	3-hour ⁽¹⁾
	0.14 ppm	24-hour ⁽¹⁾		

⁽¹⁾ Not to be exceeded more than once per year.

⁽²⁾ Final rule signed October 15, 2008.

⁽³⁾ To attain this standard, the 3-year average of the 98th percentile of the daily maximum 1-hour average at each monitor within an area must not exceed 0.100 ppm (effective January 22, 2010).

⁽⁴⁾ Not to be exceeded more than once per year on average over 3 years.

⁽⁵⁾ To attain this standard, the 3-year average of the weighted annual mean PM_{2.5} concentrations from single or multiple community-oriented monitors must not exceed 15.0 µg/m³.

⁽⁶⁾ To attain this standard, the 3-year average of the 98th percentile of 24-hour concentrations at each population-oriented monitor within an area must not exceed 35 µg/m³ (effective December 17, 2006).

⁽⁷⁾ To attain this standard, the 3-year average of the fourth-highest daily maximum 8-hour average ozone concentrations measured at each monitor within an area over each year must not exceed 0.075 ppm. (effective May 27, 2008)

⁽⁸⁾ (a) To attain this standard, the 3-year average of the fourth-highest daily maximum 8-hour average ozone concentrations measured at each monitor within an area over each year must not exceed 0.08 ppm.

(b) The 1997 standard—and the implementation rules for that standard—will remain in place for implementation purposes as USEPA undertakes rulemaking to address the transition from the 1997 ozone standard to the 2008 ozone standard.

(c) USEPA is in the process of reconsidering these standards (set in March 2008).

⁽⁹⁾ (a) USEPA revoked the 1-hour ozone standard in all areas, although some areas have continuing obligations under that standard (“anti-backsliding”).

(b) The standard is attained when the expected number of days per calendar year with maximum hourly average concentrations above 0.12 ppm is ≤1.

Source: <http://www.epa.gov/air/criteria.html>

the humid continental climate zone, with average temperatures by US standards. Summers are hot, humid and wet. July is the warmest month, with an average high of 87°F (31°C) and an average low of 68°F (20°C). Winters are generally cool to cold, with occasional snowfall. January is the coldest month, with an average high of 38°F (3°C) and an average low of 21°F (-6°C). Precipitation is fairly evenly distributed each month, averaging 41 inches of rainfall and 14 inches of snowfall annually.

2.4.2 Local Monitored Air Quality

The monitored information for the three monitoring stations nearest the study area—two in Cincinnati, Ohio and one in Highland Heights, Kentucky—are presented in Table 2. This table presents the last three years of available monitored at each of these stations in order to illustrate the study area's general air quality trends. Detailed monitored data can be found Appendix A.

2.5 Pollutant Description

2.5.1 Criteria Pollutants

Pollutants that have established national standards are referred to as “criteria pollutants.” The sources of these pollutants, their effects on human health and the nation's welfare, and their final deposition in the atmosphere vary considerably. A brief description of each pollutant is provided below.

2.5.1.1 Ozone

Ozone (O₃) is a colorless toxic gas. As shown in (Exhibit 2), O₃ is found in both the Earth's upper and lower atmospheric levels. In the upper atmosphere, O₃ is a naturally occurring gas that helps to prevent the sun's harmful ultraviolet rays from reaching the earth. In the lower layer of the atmosphere, O₃ is human-made.

Although O₃ is not directly emitted, it forms in the lower atmosphere through a chemical reaction between hydrocarbons (HC), also referred to as Volatile Organic Compounds (VOC), and nitrogen oxides (NO_x), which are emitted from industrial sources and from automobiles. HC are compounds comprised primarily of atoms of hydrogen and carbon. Total organic gases (TOG) and reactive organic gases (ROG) are the two classes of HC that are inventoried by CARB and SCAQMD. ROG have relatively high photochemical reactivity. The principal nonreactive HC is methane (CH₄), which is also a greenhouse gas. The major source of ROG is the incomplete combustion of fossil fuels in internal combustion engines. Other sources of ROG include the evaporative emissions associated with the use of paints and solvents, the application of asphalt paving, and the use of household consumer products. Adverse effects on human health are not caused directly by ROG, but rather by reactions of ROG to form secondary pollutants. ROG are also transformed into organic aerosols in the atmosphere, contributing to higher levels of fine particulate matter and lower visibility. The term “ROG” is used by CARB for air quality analysis, and is defined the same as the Federal term VOC.



Table 2. Air Quality Summary for Study Area Monitoring Station.

Air Pollutant	Standard/ Exceedance	100 E. 5 th Street Cincinnati, OH			250 Wm Howard Taft Road Cincinnati, OH			524a John Hill Road Highland Heights, KY		
		2006	2007	2008	2006	2007	2008	2006	2007	2008
Carbon Monoxide	Maximum 1-hour Concentration (ppm)	10.6	4.9	5.9	NM	NM	NM	NM	NM	NM
	Maximum 8-hour Concentration (ppm)	4.3	3.1	3.6	NM	NM	NM	NM	NM	NM
	# Days>Federal 1-hour Standard of >35 ppm	0	0	0	NM	NM	NM	NM	NM	NM
	# Days>Federal 8-hour Standard of >9 ppm	0	0	0	NM	NM	NM	NM	NM	NM
Ozone	Maximum 1-hour Concentration (ppm)	NM	NM	NM	0.101	0.118	0.101	NM	0.105	0.090
	Maximum 8-hour Concentration (ppm)	NM	NM	NM	0.089	0.097	0.086	NM	0.095	0.084
	# Days>Federal 8-hour Standard Of >0.075 ppm	NM	NM	NM	8	15	7	NM	19	2
Nitrogen Dioxide	Maximum 1-hour Concentration (ppm)	NM	NM	NM	0.061	0.081	0.079	NM	0.044	0.044
	Annual Average (ppm)	NM	NM	NM	0.018	0.017	0.016	NM	0.006	0.006
Sulfur Dioxide	Maximum 24-hour Concentration (ppm)	NM	NM	NM	NM	NM	NM	NM	0.020	0.017
	Annual Average (ppm)	NM	NM	NM	NM	NM	NM	NM	0.004	0.003
	# Days>Federal 24-hour Standard of >0.14 ppm	NM	NM	NM	NM	NM	NM	NM	0	0
Suspended Particulates (PM ₁₀)	Maximum 24-hour Concentration (µg/m ³)	NM	NM	NM	58.0	46.0	46.0	NM	NM	NM
	#Days>Fed. 24-hour Standard of>150 µg/m ³	NM	NM	NM	0	0	0	NM	NM	NM
Suspended Particulates (PM _{2.5})	Maximum 24-hour Concentration (µg/m ³)	NM	NM	NM	34.5	41.9	31.5	NM	34.0	30.5
	#Days>Fed. 24-hour Standard of>35 µg/m ³	NM	NM	NM	0	0	0	NM	0	0
	National Annual Average (µg/m ³)	NM	NM	NM	13.57	15.09	12.13	NM	14.36	11.98
	#Days>Fed. Annual Standard of>15.0 µg/m ³	NM	NM	NM	0	1	0	NM	0	0
Lead	Maximum Monthly Concentration (µg/m ³)	NM	NM	NM	NM	NM	NM	NM	NM	NM
	# Months Exceeding Federal Standard	NM	NM	NM	NM	NM	NM	NM	NM	NM

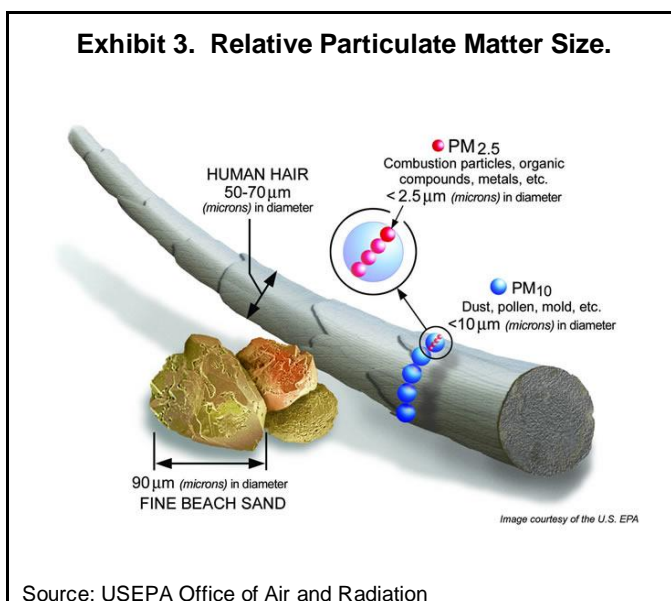
Source: USEPA AIRSData: <http://www.epa.gov/air/data/geosel.html>
 NM = not measured

Substantial O₃ formations generally require a stable atmosphere with strong sunlight; thus high levels of O₃ are generally a concern in the summer. O₃ is the main ingredient of smog. O₃ enters the bloodstream through the respiratory system and interferes with the transfer of oxygen, depriving sensitive tissues in the heart and brain of oxygen. O₃ also damages vegetation by inhibiting its growth. The effects of changes in VOC and NO_x emissions for the proposed project are examined on a regional and statewide level.

2.5.1.2 Particulate Matter (PM)

Particulate pollution is composed of solid particles or liquid droplets that are small enough to remain suspended in the air. In general, particulate pollution can include dust, soot, salts, acids, metals, and smoke; these can be irritating but usually are not poisonous. Particulate pollution also can include bits of solid or liquid substances that can be highly toxic. Of particular concern are those particles that are smaller than, or equal to, 10 microns (PM₁₀) or 2.5 microns (PM_{2.5}) in size.

PM₁₀ refers to PM less than 10 microns in diameter, about one-seventh the thickness of a human hair (Exhibit 3). PM also forms when gases emitted from motor vehicles undergo chemical reactions in the atmosphere.



Major sources of PM₁₀ include motor vehicles; wood-burning stoves and fireplaces; dust from construction, landfills, and agriculture; wildfires and brush/waste burning; industrial sources; windblown dust from open lands; and atmospheric chemical and photochemical reactions. Suspended particulates produce haze and reduce visibility.

Data collected through numerous nationwide studies indicate that most of the PM₁₀ comes from the following:

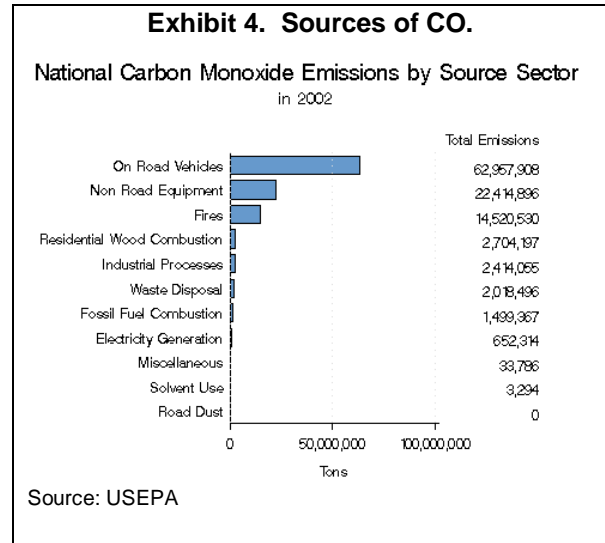
- Fugitive dust
- Wind erosion
- Agricultural and forestry sources

A small portion of PM is the product of fuel combustion processes. In the case of PM_{2.5}, the combustion of fossil fuels accounts for a significant portion of this pollutant. The main health effect of airborne particulate matter is on the respiratory system. PM_{2.5} refers to particulates that are 2.5 microns or less in diameter, roughly 1/28th the diameter of a human hair. PM_{2.5} results from fuel combustion (from motor vehicles, power generation, and industrial facilities), residential fireplaces, and wood stoves. In addition, PM_{2.5} can be formed in the atmosphere from gases such as SO₂, NO_x, and VOCs. Like PM₁₀, PM_{2.5} can penetrate the human respiratory system's natural defenses and damage the respiratory tract when inhaled. Whereas particles 2.5 to 10 microns in diameter tend to collect in the upper portion of the respiratory system,

particles 2.5 microns or less are so tiny that they can penetrate deeper into the lungs and damage lung tissues. The effects of PM₁₀ and PM_{2.5} emissions for the project are examined on a localized, or microscale, basis, a regional basis and a statewide basis.

2.5.1.3 Carbon Monoxide

Carbon monoxide (CO) is a colorless gas that interferes with the transfer of oxygen to the brain. CO is emitted almost exclusively from the incomplete combustion of fossil fuels. As shown in (Exhibit 4), on-road motor vehicle exhaust is the primary source of CO. In cities, 85 to 95 percent of all CO emissions may come from motor vehicle exhaust. Prolonged exposure to high levels of CO can cause headaches, drowsiness, loss of equilibrium, or heart disease. CO levels are generally highest in the colder months of the year when inversion conditions (when warmer air traps colder air near the ground) are more frequent.



CO concentrations can vary greatly over relatively short distances. Relatively high concentrations of CO are typically found near congested intersections, along heavily used roadways carrying slow-moving traffic, and in areas where atmospheric dispersion is inhibited by urban “street canyon” conditions. Consequently, CO concentrations must be predicted on a microscale basis.

2.5.1.4 Nitrogen Dioxide

Nitrogen dioxide (NO₂) is a brownish gas that irritates the lungs. It can cause breathing difficulties at high concentrations. As with O₃, NO₂ is not directly emitted but is formed through a reaction between nitric oxide (NO) and atmospheric oxygen. NO and NO₂ are collectively referred to as nitrogen oxides (NO_x) and are major contributors to O₃ formation. NO₂ also contributes to the formation of PM₁₀. At atmospheric concentrations, NO₂ can be potentially irritating. In high concentrations, the result is a brownish-red cast to the atmosphere and reduced visibility. There is some indication of a relationship between NO₂ and chronic pulmonary fibrosis. An increase in bronchitis in children (two and three years old) has also been observed at concentrations below 0.3 parts per million (ppm).

2.5.1.5 Lead

Lead (Pb) is a stable element that persists and accumulates both in the environment and in animals. Its principal effects in humans are on the blood-forming, nervous, and renal systems. Pb levels from mobile sources in the urban environment have decreased significantly due to the federally-mandated switch to lead-free gasoline, and they are expected to continually decrease. An analysis of lead emissions from transportation projects is therefore not warranted.

2.5.1.6 Sulfur Dioxide

Sulfur Dioxide (SO₂) is a product of high-sulfur fuel combustion. The main sources of SO₂ are coal and oil used in power stations, industry, and domestic heating. Industrial chemical manufacturing is another source of SO₂. SO₂ is an irritant gas that attacks the throat and lungs.

It can cause acute respiratory symptoms and diminished ventilator function in children. SO₂ can also yellow plant leaves and corrode iron and steel. Although diesel-fueled heavy duty vehicles emit SO₂, transportation sources are not considered by USEPA (and other regulatory agencies) to be significant sources of this pollutant, thus an analysis of emissions from transportation projects is not warranted.

2.6 Attainment Status

Section 107 of the 1977 CAAA requires that the USEPA publish a list of all geographic areas in compliance with the NAAQS, plus those not attaining the NAAQS. Areas not in NAAQS compliance are deemed non-attainment areas. Areas that have insufficient data to make a determination are deemed unclassified, and are treated as being attainment areas until proven otherwise. An area's designation is based on the data collected by the state monitoring network on a pollutant-by-pollutant basis.

The study area is located in Hamilton County, Ohio and Kenton County, Kentucky. As shown Table 3, the USEPA has classified both counties as nonattainment areas for O₃ and for PM_{2.5}.

Table 3. Study Area Attainment Status.

Pollutant	Federal Attainment Status Hamilton County, OH	Federal Attainment Status Kenton County, KY
Ozone (O ₃)	Nonattainment	Nonattainment
Nitrogen Dioxide (NO ₂)	Attainment	Attainment
Carbon Monoxide (CO)	Attainment	Attainment
Particulate Matter (PM ₁₀)	Attainment	Attainment
Particulate Matter (PM _{2.5})	Nonattainment	Nonattainment
Lead (Pb)	Attainment	Attainment

Source: USEPA, 2010

2.7 State Implementation Plan and Transportation Improvement Program Status

Under the CAAA, the Intermodal Surface Transportation Efficiency Act of 1991 (ISTEA), and the Transportation Equity Act for the 21st Century (TEA-21), proposed transportation projects must be derived from a long-range transportation plan (LRP) or Regional Transportation Plan (RTP) that conforms with the state air quality plans as outlined in the SIP. The SIP sets forth the state's strategies for achieving air quality standards. Projects must also be included in a Transportation Improvement Program (TIP) that conforms with the SIP, and localized impacts from proposed projects must conform to state air quality plans in non-attainment and maintenance areas.

The Ohio-Kentucky-Indiana Regional Council of Governments (OKI) is the Metropolitan Planning Organization for the greater Cincinnati area. Every four years, OKI updates the OKI 2030 Regional Transportation Plan. The Plan is the long-range, comprehensive transportation-planning document for the three-state, eight-county Greater Cincinnati region. It defines the overarching goals for transportation in the region, establishes existing and future transportation needs of the region and allocates projected revenue to transportation programs and projects that address those needs.

The latest regional emissions and air quality conformity analysis was completed in June 2008 with the adoption of OKI's 2030 Regional Transportation Plan and amended FY 2008-FY 2011 Transportation Improvement Program. With the Plan's local adoption, it has been submitted to the federal highway and federal transit administrations for their review and approval. The Brent Spence Bridge Rehabilitation/Replacement project, identified as KYTC Project ID #6-17.03, 6-17.04, and ODOT PID 75119, was included in this analysis. This analysis found that the plan and, therefore, the individual projects contained in the plan, are conforming projects, and will have air quality impacts consistent with those identified in the SIPs for achieving the NAAQS.

3.0 ENVIRONMENTAL IMPACT/ENVIRONMENTAL CONSEQUENCES

Pollutants that can be traced principally to motor vehicles are relevant to the evaluation of the project's impacts; these pollutants include carbon monoxide (CO), hydrocarbons (HC), nitrous oxides (NO_x), ozone (O₃), Particulate Matter (PM₁₀ and PM_{2.5}), and mobile source air toxics (MSAT). Transportation sources account for a small percentage of regional emissions of sulfur oxide (SO_x) and lead (Pb); thus, a detailed analysis is not required.

HC volatile organic compounds (VOC) and NO_x emissions from automotive sources are a concern primarily because they are precursors in the formation of O₃ and PM. Ozone is formed through a series of reactions that occur in the atmosphere in the presence of sunlight. Since the reactions are slow and occur as the pollutants are diffusing downwind, elevated O₃ levels often are found many miles from the sources of the precursor pollutants. Therefore, the effects of HC and NO_x emissions generally are examined on a regional or "mesoscale" basis.

PM₁₀ and PM_{2.5} impacts are both regional and local. A significant portion of particulate matter, especially PM₁₀, comes from disturbed vacant land, construction activity, and paved road dust. PM_{2.5} also comes from these sources. Motor vehicle exhaust, particularly from diesel vehicles, is also a source of PM₁₀ and PM_{2.5}. PM₁₀, and especially PM_{2.5}, can also be created by secondary formation from precursor elements such as sulfur dioxide (SO₂), NO_x, VOCs, and ammonia (NH₃). Secondary formation occurs due to chemical reaction in the atmosphere generally downwind some distance from the original emission source. Thus it is appropriate to predict concentrations of PM₁₀ and PM_{2.5} on both a regional and a localized basis.

CO impacts are generally localized. Even under the worst meteorological conditions and most congested traffic conditions, high concentrations are limited to a relatively short distance (300 to 600 feet) of heavily traveled roadways. Vehicle emissions are the major sources of CO. The project could change traffic patterns within the study area. Consequently, it is appropriate to predict concentrations of CO on both a regional and a localized or "microscale" basis.

MSAT impacts are both regional and local. On February 3, 2006, the Federal Highway Administration (FHWA) released *Interim Guidance on Air Toxic Analysis in NEPA Documents*. This guidance was superseded on September 30, 2009 by FHWA's *Interim Guidance Update on Air Toxic Analysis in NEPA Documents*. According to these documents, regardless of the alternative chosen, MSAT emissions will likely be lower than present levels in the design year as a result of the United States Environmental Protection Agency's (USEPA) national control programs that are projected to reduce annual MSAT emissions by 72 percent between 1999 and 2050. Local conditions may differ from these national projections in terms of fleet mix and turnover, vehicle miles traveled (VMT) growth rates, and local control measures. However, the magnitude of the USEPA-projected reductions is so great (even after accounting for VMT growth) that MSAT emissions in the study area are likely to be lower in the future in nearly all cases.

3.1 Regional Emissions Analysis

The regional (or mesoscale) analysis of a project determines a project's overall impact on regional air quality levels. A transportation project is analyzed as part of a regional transportation network developed by the County or State. Projects included in this network are

found in the area's Transportation Improvement Plan (TIP). The TIP is the basis for the regional analysis which utilizes VMT and vehicle hours traveled (VHT) within the region to estimate daily "pollutant burden" levels. The results of this analysis determine if an area is in conformity with regulations set forth in the Final Conformity Rule.

The Brent Spence Bridge Replacement/Rehabilitation project, identified as KYTC Project ID #6-17.03, 6-17.04, and ODOT PID 75119, was included in the regional emissions analysis conducted by the Ohio Kentucky Indiana Regional Council of Governments (OKI) for the 2030 Regional Transportation Plan and the Fiscal Year 2008-2011 TIP, dated June 2008. This analysis found that the plan and, therefore, the individual projects contained in the plan, are conforming projects, and will have air quality impacts consistent with those identified in the state implementation plans (SIPs) for achieving the National Ambient Air Quality Standards (NAAQS).

Though the conformity analysis conducted by OKI determined that the project conforms to the air quality goals of the area, a project level regional analysis was conducted to highlight the project's impact on regional air quality levels. The regional analysis utilizes VMT and VHT within the region, with corresponding emission factors for HC, NO_x, CO, PM₁₀ and PM_{2.5} from USEPA's latest emission factor program, MOBILE6.2, to determine daily "pollutant burden" levels under each alternative.

The regional emissions analysis was conducted for the No Build and two Build Alternatives (Alternative E and Alternative I). The analysis was based on regional VMT estimates by roadway type along with associated VHT estimates. Emission factors were obtained using USEPA's MOBILE6.2 emission factor program with area specific data supplied by OKI. The results for the study area are shown in Table 4. The project is predicted to reduce overall VMT and emissions of VOC, PM₁₀ and PM_{2.5} by approximately 0.1 percent. It is expected to increase CO and NO_x emissions by approximately 0.1 to 0.2 percent. These increases are due to increased speeds under the Build Alternatives which increase emission rates for these particular pollutants. The overall effect of the project on regional pollutant levels, however, is less than 0.5 percent and will likely result in no measurable increase or decrease in regional pollutant levels.

3.1.1 Carbon Monoxide (CO)

The localized assessment of air quality was conducted to address CO, PM₁₀ and PM_{2.5} impacts, as well as mobile source air toxics (MSAT). This report focuses on the CO analysis.

A CO analysis was conducted because the constructed project will result in an increase in the ADT of more than 10,000 vehicles within 10 years of project completion date. Also, the project involves a new project right-of-way that will have an ADT of more than 20,000 vehicles within 10 years of construction. Hence, a carbon monoxide analysis is required.

Microscale air quality modeling was performed using the most recent version of the USEPA mobile source emission factor model (MOBILE6.2) and the CAL3QHC version 2.0 air quality dispersion model to estimate future No Build Alternative and the Build Alternatives, CO levels at selected locations in the study area.

3.1.2 Site Selection and Receptor Locations

The sites chosen for the CO analysis were selected using a screening analysis based on overall intersection volume, changes in intersection volume, and changes in traffic level of service

Table 4. Regional Emission Burden Assessment.

Alternative	Vehicle Miles Travelled (miles)	Average Speed (mph)	Emission Burden (Tons per Day)					Percent Change from No Build						
			CO	VOC	NO _x	PM ₁₀	PM _{2.5}	VMT	CO	VOC	NO _x	PM ₁₀	PM _{2.5}	
No Build	89,731,288	32.0	1,230	33.6	32.5	2.7	1.3	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Alternative E	89,667,285	32.0	1,231	33.5	32.6	2.7	1.3	-0.1%	-0.1%	0.1%	-0.1%	-0.1%	-0.1%	-0.1%
Alternative I	89,667,285	32.0	1,231	33.5	32.6	2.7	1.3	-0.1%	-0.1%	0.2%	-0.1%	-0.1%	-0.1%	-0.1%

(LOS). Intersections that demonstrate a LOS of A, B, or C are not expected to cause a violation of the NAAQS. Intersections that the project causes to operate at or below LOS D, increase delay of an intersection with a LOS of worse than D, or increase overall traffic volumes, have the potential to cause a violation of the NAAQS, and therefore fail the screening analysis.

As shown in Table 5, a total of 70 intersections within the study corridor were screened based on this methodology. Seven sites in Kentucky and nine sites in Ohio failed the screening analysis. These sites are highlighted in Table 5. Of these 16 sites, seven intersections, represented by four analysis sites, were chosen for detailed analysis. These four modeled sites are representative of the worst-case conditions and, therefore, the highest CO levels in the project area. These sites are:

- **Kentucky**
 - ▶ **Kyles Lane and Dixie Highway** – This site has the highest traffic volume and worst LOS and delay of all the intersections screened in Kentucky.
 - ▶ **KY 5th Street and Bakewell Street** – This site is predicted to operate at LOS F in the AM peak period under Alternative I. Given the close proximity of this site to the intersections of **KY 5th Street & Philadelphia Street** and **KY 5th Street & Main Street** (which also failed the screening analysis), these additional two intersections were included in the microscale analysis for this location.
- **Ohio**
 - ▶ **OH 4th Street and Central Avenue** - This site has the worst LOS under the Build Alternatives (Alternative E, PM peak) of all the intersections screened in Ohio. In Alternative E OH 4th Street will also be connecting with the C-D Roadway (intersection of **OH 4th Street and C-D Roadway**), which is also a high volume site that failed the screening analysis.
 - ▶ **Western Hills and I-75 Southbound ramp** - This intersection has the highest traffic volume of all the intersections in Ohio that failed the screening analysis. It is close to the intersection of **Central Parkway and McMillan Street**, which has the highest non-ramp intersection volumes of all the Ohio intersections screened. Given the distance from this site to the nearest sensitive receptors, the intersections of **Central Parkway and McMillan Street** and **Western Hills and the I-75 Northbound ramp** were also included in this analysis location.

The sites chosen for detailed analysis are shown in (Exhibit 5) and listed in Table 6. Receptors were chosen at each site in accordance with the guidelines found in the USEPA's *Guideline for Modeling Carbon Monoxide from Roadway Intersections* (USEPA-454/R-92-005). Microscale CO levels were modeled at these locations using the USEPA-authorized MOBILE6.2 program to develop emissions and the CAL3QHC dispersion program to calculate concentrations.

3.1.2.1 Emission Model

Vehicular emissions were estimated using the USEPA MOBILE6.2 vehicular emission factor model. (*User's Guide to MOBILE6.2, Mobile Source Emission Factor Model, Ann Arbor, Michigan, USEPA420-R-02-028, October 2002*). Input parameters were provided by OKI.

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Table 5. CO Site Selection Screening Analysis.

Intersection	No Build (2035)						Alternative E						Alternative I					
	AM			PM			AM			PM			AM			PM		
	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume
Ohio																		
Bank Street & Dalton Avenue	B	12.6	1,270	B	15.6	1,950	B	12.9	1,410	B	15.9	2,200	B	13.1	1,430	B	19.7	2,280
Bank Street & Winchell Avenue	B	12.0	610	B	12.7	1,070	B	11.6	530	B	12.1	910	B	12.6	710	B	13.2	1,180
Central Parkway & Linn Street	B	15.2	2,060	B	15.6	2,710	B	18.5	3,080	C	25.2	3,910	B	15.2	2,060	B	15.6	2,710
Bank Street & Linn Street	B	10.0	430	B	11.3	710	B	10.6	550	B	12.6	910	B	10.5	540	B	13.4	910
Dalton Avenue & Findlay Street	B	12.6	1,210	B	13.3	1,620	B	12.6	1,380	B	13.7	1,870	B	12.8	1,340	B	14.1	1,800
Findlay Street & Western Avenue	B	11.9	950	B	11.6	770	B	11.3	610	B	11.3	620	B	11.5	800	B	11.6	820
Findlay Street & Winchell Avenue	B	11.6	690	B	11.9	890	B	11.4	550	B	11.7	730	B	11.8	800	B	12.5	1,110
Dalton Avenue & Liberty Street	B	12.9	1,050	B	14.4	1,830	B	12.9	1,510	B	14.3	2,050	B	13.3	1,420	B	14.6	1,900
Western Avenue & Liberty Street	C	20.2	950	B	12.1	1,000	B	19.9	720	B	19.7	760	C	20.3	960	C	20.2	900
Liberty Street & Winchell Avenue	B	12.5	1,090	B	12.8	1,270	B	12.1	830	B	12.4	990	B	13.0	1,090	B	13.2	1,280
Liberty Avenue & Linn Street	B	12.4	1,440	B	13.1	1,930	B	12.2	1,230	B	12.8	1,690	B	12.3	1,230	B	12.9	1,670
Ezzard Charles Drive (WB) & Western Avenue	B	11.2	940	B	11.3	900	B	10.7	440	B	10.9	620	B	10.7	480	B	10.6	400
Ezzard Charles Drive (WB) & Winchell Avenue	B	10.9	570	B	11.7	1,050	B	10.9	540	B	11.5	900	B	11.1	670	B	12.3	1,350
Ezzard Charles Drive (EB) & Western Avenue	B	11.3	910	B	11.4	930	B	11.0	410	B	11.0	660	B	10.7	430	B	10.7	430
Ezzard Charles Drive (EB) & Winchell Avenue	B	12.1	1,030	B	11.2	800	B	11.6	910	B	11.3	680	B	11.8	1,050	B	11.6	1,130
Ezzard Charles Drive & Linn Street	B	12.5	1,430	B	12.4	1,900	B	12.2	1,380	B	12.3	1,760	B	12.1	1,340	B	12.3	1,710
Geat Street & Dalton Avenue	B	11.9	1,410	B	12.7	1,730	B	12.0	1,400	B	12.7	1,720	B	11.9	1,420	B	12.8	1,800

Table 5. CO Site Selection Screening Analysis (continued).

Intersection	No Build (2035)						Alternative E						Alternative I					
	AM			PM			AM			PM			AM			PM		
	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume
Ohio																		
West Street & Western Avenue	B	11.3	670	B	11.2	740	B	11.3	820	B	11.5	880	B	10.9	510	B	11.2	640
West Street & Freeman Avenue	C	29.0	1,810	C	20.2	1,690	C	22.5	1,940	C	21.2	1,920	C	31.1	1,980	C	21.0	1,870
Linn Street & Gest Street	B	12.1	850	B	12.6	1,180	B	12.0	800	B	12.9	1,120	B	12.0	810	B	12.4	1,100
Court Street & Linn Street	C	16.8	950	C	23.2	1,200	B	14.0	750	C	23.5	1,100	B	11.4	520	B	14.9	740
8 th Street & Dalton Avenue	B	12.5	1,860	B	12.9	2,090	B	12.5	1,730	B	12.8	1,920	B	12.5	1,860	B	12.9	2,110
8 th Street & Freeman Avenue	B	13.2	2,450	B	13.3	2,520	B	13.4	2,630	B	13.6	2,500	B	13.1	2,400	B	13.5	2,540
8 th Street & Linn Street	B	13.6	1,850	C	20.2	2,430	B	13.7	2,170	B	16.2	2,820	B	13.6	1,930	B	18.9	2,470
Western Hills Viaduct & Spring Grove Avenue	B	14.0	1,860	B	19.3	2,750	B	19.1	2,230	C	21.9	3,480	B	14.0	1,860	B	19.3	2,750
Dalton Avenue & Linn Street	B	12.5	1,160	B	15.7	1,620	B	12.3	1,210	B	16.2	1,890	B	12.5	1,180	B	15.6	1,710
6 th Street & Linn Street	A	8.6	670	B	14.8	1,530	A	9.1	790	D	34.7	1,840	A	8.5	690	C	15.4	1,570
Court Street & Central Avenue	B	16.5	1,100	B	12.1	860	B	16.7	1,240	B	12.3	850	B	13.1	900	B	12.0	820
9 th Street & Central Avenue	B	18.9	1,020	D	35.1	2,830	B	11.2	660	B	19.8	1,320	B	18.6	760	C	23.8	1,870
7 th Street & Central Avenue	B	17.8	2,750	B	12.4	1,150	C	24.7	2,830	B	12.9	1,200	B	17.6	2,610	B	12.2	1,070
6 th Street & Central Avenue	B	15.1	970	C	23.8	2,110	D	38.9	1,850	D	50.1	2,110	B	11.9	750	B	13.2	1,510
5 th Street & Central Avenue	C	26.6	2,500	B	17.5	1,570	D	41.7	3,010	C	20.5	1,840	C	22.2	2,100	B	16.9	1,360
4 th Street & Central Avenue	B	15.3	910	D	38.8	2,600	B	15.7	1,090	E	55.4	3,250	B	14.1	750	C	27.0	2,310
3 rd Street & Central Avenue	D	39.2	1,730	D	44.0	2,620	D	37.6	1,450	C	31.5	1,870	D	41.1	1,570	D	43.8	2,060
4 th Street & Plum Street	B	11.3	580	B	13.0	1,400	B	11.5	710	B	14.6	1,780	B	11.3	590	B	13.2	1,430

Table 5. CO Site Selection Screening Analysis (continued).

Intersection	No Build (2035)						Alternative E						Alternative I					
	AM			PM			AM			PM			AM			PM		
	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume
Ohio																		
3 rd Street & Plum Street	B	12.5	990	B	12.6	1,020	B	12.3	910	B	12.1	780	B	12.2	900	B	12.4	940
4 th Street & Elm Street	B	12.6	1,390	B	14.3	2,200	B	13.0	1,490	B	15.4	2,410	B	12.7	1,320	B	14.2	2,140
3 rd Street & Elm Street	B	14.1	2,050	B	14.6	2,500	B	13.5	1,900	B	14.4	2,440	B	13.5	1,890	B	14.9	2,610
2 nd Street & Elm Street	B	16.2	3,480	B	15.3	2,350	B	16.1	3,560	B	14.1	2,320	B	15.2	3,270	B	14.0	2,300
3rd Street & Clay Wade Bailey Bridge	C	23.0	1,280	C	32.9	2,420	B	15.5	1,030	C	30.7	1,980	C	24.1	1,460	D	37.5	2,110
Central Parkway & McMillan Street	C	20.0	2,860	D	41.9	3,690	A	8.4	3,040	B	19.1	3,310	C	20.0	2,860	D	41.9	3,690
Central Parkway & McMillan Street	-	-	-	-	-	-	B	17.0	2,630	A	9.7	3,620	-	-	-	-	-	-
Western Hills Viaduct & I-75 Southbound Ramp	-	-	-	-	-	-	D	40.1	6,030	C	33.0	4,900	A	3.7	2,140	A	9.4	1,800
Western Hills Viaduct & I-75 Northbound Ramp	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
C-D Road & 4 th Street	-	-	-	-	-	-	B	17.9	2,900	D	49.1	4,550	-	-	-	-	-	-
C-D Road & 5 th Street	-	-	-	-	-	-	B	18.7	3,980	A	6.4	4,600	-	-	-	-	-	-
I-71 Southbound/I-75 Northbound & 6 th Street	-	-	-	-	-	-	C	28.6	4,740	C	33.7	4,900	-	-	-	-	-	-
C-D Road & 7 th Street	-	-	-	-	-	-	D	41.5	4,130	B	14.7	2,230	-	-	-	-	-	-

Table 5. CO Site Selection Screening Analysis (continued).

Intersection	No Build (2035)						Alternative E						Alternative I						
	AM			PM			AM			PM			AM			PM			
	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	
Kentucky																			
4th Street & Crescent Avenue	C	21.9	800	F	121.1	940	B	17.9	1,700	B	18.8	1,750	C	18.2	700	C	18.0	740	
4th Street & Philadelphia Street	D	54.5	2,370	F	83.5	2,930	F	100.8	2,610	B	14.4	2,090	C	32.2	2,020	B	14.0	2,020	
4th Street & Bakewell Street	B	12.1	1,300	B	14.0	1,880	B	13.0	1,650	B	12.7	1,460	B	11.9	1,200	B	12.3	1,310	
4th Street & Main Street / Clay Wade Bailey Bridge	B	16.1	2,040	C	28.6	2,890	B	15.8	2,120	D	36.3	2,630	B	13.1	1,670	D	45.9	2,660	
5th Street & Crescent Avenue	B	11.4	600	C	15.3	780	-	-	-	-	-	-	B	11.0	590	C	15.9	780	
5th Street & Philadelphia Street	B	17.3	1,820	B	15.3	1,540	B	17.7	1,750	B	16.0	1,500	B	15.9	1,630	B	13.8	1,310	
5th Street & Bakewell Street	E	42.6	1,310	C	21.1	1,000	F	53.9	1,400	D	32.9	1,210	F	106.7	1,250	D	25.3	930	
5th Street & Main Street	B	17.6	1,940	B	16.3	2,050	B	15.9	1,870	D	35.7	2,500	B	16.0	1,930	C	31.9	2,570	
Pike Street & Bullock Street	C	22.5	2,380	C	34.1	2,160	B	13.4	2,010	B	19.6	2,890	C	24.1	2,450	C	22.7	2,910	
Pike Street & Jillians Way	D	49.4	2,630	B	16.2	1,850	B	13.9	1,690	B	13.1	1,550	B	19.8	3,080	B	19.3	2,560	
12th Street & Bullock Street	C	15.6	1,090	C	15.4	1,130	B	13.1	1,500	B	14.3	2,100	B	13.4	1,410	B	16.9	1,850	
12th Street & Jillians Way	F	565.3	1,480	F	302.7	1,560	B	12.5	1,530	B	13.1	1,670	C	24.1	2,370	B	14.6	2,120	
Kyles Lane & Dixie Highway	F	214.6	3,430	F	171.3	3,560	F	222.8	3,480	F	165.9	3,650	F	222.8	3,480	F	166.1	3,650	
Kyles Lane & I-75 SB Ramp	C	26.8	2,350	D	47.9	3,230	B	19.7	2,350	C	24.0	3,260	B	19.7	2,350	C	24.0	3,260	
Kyles Lane & I-75 NB Ramp	F	108.7	3,160	C	32.3	3,490	C	20.2	3,220	C	24.6	3,500	C	20.2	3,220	C	24.6	3,500	
Kyles Lane & Highland Avenue	F	105.7	2,960	F	137.7	3,410	F	90.0	3,060	F	102.8	3,470	F	90.0	3,060	F	102.8	3,470	
Dixie Highway & I-75 NB	C	22.0	1,970	B	18.1	2,050	C	22.2	2,060	B	16.2	2,080	C	22.2	2,060	B	16.2	2,080	
Dixie Highway & I-75 SB	B	18.6	2,250	C	20.2	2,510	B	17.6	2,360	C	20.5	2,590	B	17.6	2,360	C	20.5	2,590	

Table 5. CO Site Selection Screening Analysis (continued).

Intersection	No Build (2035)						Alternative E						Alternative I						
	AM			PM			AM			PM			AM			PM			
	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	LOS	Delay	Volume	
Kentucky																			
9th & Jillians Way	-	-	-	-	-	-	C	22.4	1,440	C	26.9	1,770	B	12.7	870	B	12.0	740	
9th & Bullock Street	-	-	-	-	-	-	B	13.0	1,930	C	21.9	3,180	B	13.4	1,160	B	16.0	1,690	
5th & Exit Ramp	-	-	-	-	-	-	B	16.6	1,670	B	14.5	1,510	B	14.1	1,340	B	12.6	960	
4th & Exit Ramp	-	-	-	-	-	-	C	19.3	1,210	E	37.6	1,310	-	-	-	-	-	-	

Table 6. CO Microscale Analysis Sites.

Analysis Site #	Location
1	Kyles Lane and Dixie Highway
2	KY 5 th Street and Bakewell Street
3	OH 4 th Street and Central Avenue
4	Western Hills Viaduct and I-75 southbound ramp

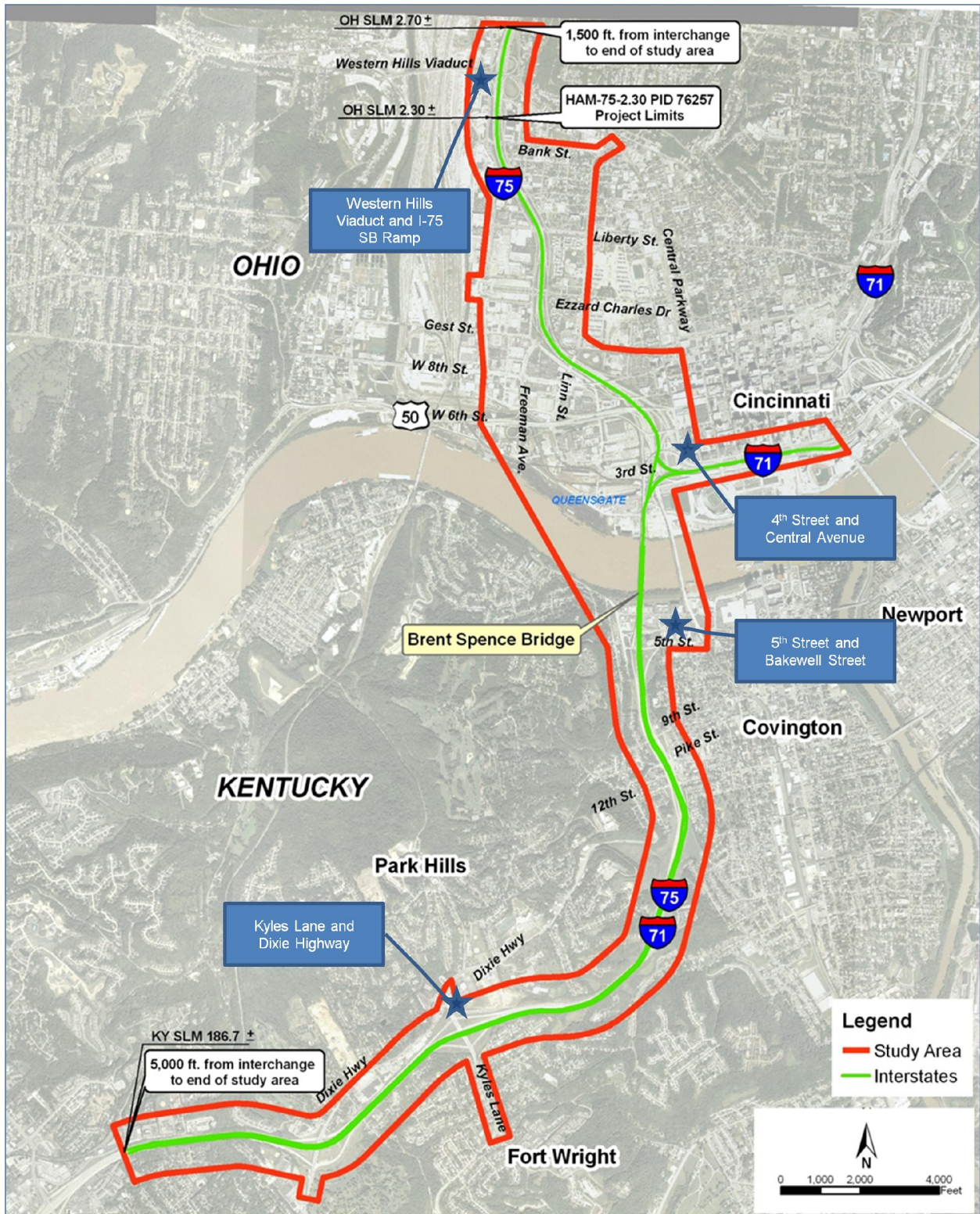


Exhibit 5. Microscale Analysis Locations

MOBILE6.2 is a mobile source emission estimate program that provides current and future estimates of emissions from highway motor vehicles. The latest in the MOBILE series, dating back to 1978, MOBILE6.2 was designed by the USEPA to address a wide variety of air pollution modeling needs. This latest version of MOBILE differs significantly in both structure and data requirements from previous versions. MOBILE6.2 incorporates updated information on basic emission rates, more realistic driving patterns, separate start and running emissions, improved correction factors, and changing fleet composition. Input and output files for the MOBILE6.2 program can be found in Appendix B.

3.1.2.2 Dispersion Model

Mobile source models are the basic analytical tools used to estimate CO concentrations expected under given traffic, roadway geometry, and meteorological conditions. The mathematical expressions and formulations that comprise the various models attempt to describe an extremely complex physical phenomenon as closely as possible. The dispersion modeling program used in this study for estimating pollutant concentrations near roadway intersections is the CAL3QHC (Version 2.0) dispersion model developed by the USEPA and released in 1992.

CAL3QHC is a Gaussian model recommended in the USEPA *Guidelines for Modeling Carbon Monoxide from Roadway Intersections* (EPA-454/R-92-005). Gaussian models assume that the dispersion of pollutants downwind of a pollution source follow a normal distribution from the center of the pollution source.

Different emission rates occur when vehicles are stopped (idling), accelerating, decelerating, and moving at different average speeds. CAL3QHC simplifies these different emission rates into two components:

- Emissions when vehicles are stopped (idling) during the red phase of a signalized intersection
- Emissions when vehicles are in motion during the green phase of a signalized intersection

The CAL3QHC (Version 2.0) air quality dispersion model has undergone extensive testing by USEPA and has been found to provide reliable estimates of inert (nonreactive) pollutant concentrations resulting from motor vehicle emissions. A complete description of the model is in the *User's Guide to CAL3QHC version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations near Roadway Intersections* (EPA-454/R-92-006). The CAL3QHC input and output files used for the microscale modeling are presented in Appendix C.

3.1.2.3 Meteorological Conditions

The transport and concentration of pollutants emitted from motor vehicles are influenced by three principal meteorological factors: wind direction, wind speed, and the temperature profile of the atmosphere. The values for these parameters were chosen to maximize pollutant concentrations at each prediction site (i.e., to establish a conservative worst case situation).

The selection of these meteorological parameters was based on recommendations from the OKI and USEPA's Guidelines:

- **Wind Direction.** Maximum CO concentrations are normally found when the wind is assumed to blow approximately parallel to a single roadway adjacent to the receptor location. At complex intersections, however, it is difficult to predict which wind angle will result in maximum concentrations. At each receptor location, therefore, the approximate wind angle that would result in maximum pollutant concentrations was used in the analysis. All wind angles from 0° to 360° (in 5° increments) were considered.
- **Wind Speed.** CO concentrations are greatest at low wind speeds. A conservative wind speed of 1.0 meter per second (2.2 miles per hour) was used to predict CO concentrations during peak traffic periods.
- **Temperature and Profile of the Atmosphere.** Minimum and maximum winter temperatures of 19°C and 37°C, respectively, a “mixing” height (the height in the atmosphere to which pollutants rise) of 1000 meters, and neutral atmospheric stability (stability class D) conditions will be used in estimating microscale CO concentrations.

The CO levels estimated by the model are the maximum concentrations which could be expected to occur at each air quality receptor site analyzed, given the assumed simultaneous occurrence of a number of worst case conditions: peak hour traffic conditions, conservative vehicular operating conditions, low wind speed, low atmospheric temperature, neutral atmospheric conditions, and maximizing wind direction.

3.1.2.4 Persistence Factor

Peak eight-hour concentrations of CO were obtained by multiplying the highest peak hour CO estimates by a persistence factor. The persistence factor accounts for the fact that:

- Over eight-hours (as distinct from a single hour) vehicle volumes will fluctuate downward from the peak hour.
- Vehicle speeds may vary.
- Meteorological conditions including wind speed and wind direction will vary compared to the conservative assumptions used for the single hour.

A persistence factor of 0.7 was used in this analysis. This factor is recommended for use by the USEPA.

3.1.2.5 Background Concentrations

Microscale modeling is used to predict CO concentrations resulting from emissions from motor vehicles using roadways immediately adjacent to the locations at which predictions are being made. A CO background level must be added to this value to account for CO entering the area from other sources upwind of the receptors. The CO background level should be located away from the influence of local traffic congestion. For the study area, the data collected at the 100 E. 5th Street monitoring station located in Cincinnati, Ohio was used for a background concentration. The use of this monitor is conservative because, though it is the closest monitor to the general study area, it is a microscale monitor, therefore it already accounts for local traffic. The second highest maximum monitored value was used as a background concentration. The second highest monitored one-hour CO concentration during the period of 2006 – 2008 (2009 data is not currently validated) was 9.9 ppm; the second highest eight-hour average was 3.0 ppm. These values were conservatively used as the background for all CO modeling

analyses. Future CO background levels are anticipated to be lower than existing levels due to mandated emission source reductions.

3.1.2.6 Traffic Information

Traffic data for the air quality analysis were derived from traffic counts and other information developed as part of an overall traffic analysis for the project. Output from the Highway Capacity model was used to obtain signal timing parameters. The microscale CO analysis was performed based on data from this analysis for the AM and PM peak traffic periods. These are the periods when maximum traffic volumes occur on local streets and when the greatest traffic and air quality effects of the proposed project are expected.

3.1.2.7 Analysis Years

CO concentrations were predicted for the design year (2035) of the project.

3.1.3 Analysis Results

Maximum one-hour and eight-hour CO levels were predicted at receptor sites within the study area. Maximum one-hour CO concentrations are shown in Table 7. Maximum eight-hour CO concentrations are shown in Table 8.

No violations of the NAAQS are predicted under any alternative.

Table 7. Predicted Worst-Case One-hour CO Concentrations (ppm).

No	Site Description	No Build		Alternative E		Alternative I	
		AM	PM	AM	PM	AM	PM
1	Kyles Lane and Dixie Highway	12.5	12.5	12.6	12.7	12.6	12.5
2	5 th Street and Bakewell Street	11.5	12.4	12.9	12.0	12.5	12.6
3	4 th Street and Central Avenue	11.9	13.0	10.8	12.3	11.9	14.6
4	Western Hills & I-75 SB ramp	11.8	13.2	12.1	13.2	12.3	13.5

Note: Concentrations include one-hour CO background = 9.9 ppm; One-hour NAAQS = 35 ppm

Table 8. Predicted Worst-Case Eight-hour CO Concentrations (ppm).

No	Site Description	No Build	Alternative E	Alternative I
1	Kyles Lane and Dixie Highway	4.8	5.0	4.9
2	5 th Street and Bakewell Street	4.8	5.1	4.9
3	4 th Street and Central Avenue	5.2	4.7	6.3
4	Western Hills & I-75 SB ramp	5.3	5.3	5.5

Note: Concentrations include one-hour CO background = 3.0 ppm; Eight-hour NAAQS = 9 ppm,

3.2 Construction Assessment

Construction-related effects of the project would be limited to short-term increased fugitive dust and mobile-source emissions during construction. State and local regulations regarding dust control and other air quality emission reduction controls will be followed.

Once a detailed construction schedule is developed, a more refined construction analysis will be conducted to determine the air quality impacts of construction.

3.3 Fugitive Dust Emissions

Fugitive dust is airborne particulate matter, generally of a relatively large particulate size. Construction-related fugitive dust would be generated by haul trucks, concrete trucks, delivery trucks, and earth-moving vehicles operating around the construction sites. This fugitive dust would be due primarily to particulate matter re-suspended (“kicked up”) by vehicle movement over paved and unpaved roads, dirt tracked onto paved surfaces from unpaved areas at access points, and material blown from uncovered haul trucks.

Generally, the distance that particles drift from their source depends on their size, the emission height, and the wind speed. Small particles (30 – 100 micron range) can travel several hundred feet before settling to the ground. Most fugitive dust, however, is comprised of relatively large particles (that is, particles greater than 100 microns in diameter). These particles are responsible for the reduced visibility often associated with this type of construction. Given their relatively large size, these particles tend to settle within 20 to 30 feet of their source.

In order to minimize the amount of construction dust generated, the guidelines below should be followed. The following preventive and mitigative measures should be taken to minimize the potential particulate pollution problem:

- **Site Preparation**
 - ▶ Minimize land disturbance.
 - ▶ Use watering trucks to minimize dust.
 - ▶ Cover trucks when hauling dirt.
 - ▶ Stabilize the surface of dirt piles if they are not removed immediately.
 - ▶ Use windbreaks to prevent accidental dust pollution.
 - ▶ Limit vehicular paths and stabilize these temporary roads.
 - ▶ Pave all unpaved construction roads and parking areas to road grade for a length no less than 50 feet from where such roads and parking areas exit the construction site. This prevents dirt from washing onto paved roadways.

- **Construction**
 - ▶ Cover trucks when transferring materials.
 - ▶ Use dust suppressants on unpaved traveled paths.
 - ▶ Minimize unnecessary vehicular and machinery activities.
 - ▶ Minimize dirt track-out by washing or cleaning trucks before leaving the construction site. An alternative to this strategy is to pave a few hundred feet of the exit road just before entering the public road.

- **Post-Construction**
 - ▶ Re-vegetate any disturbed land not used.
 - ▶ Remove unused material.
 - ▶ Remove dirt piles.
 - ▶ Re-vegetate all vehicular paths created during construction to avoid future off-road vehicular activities.

3.4 CO Emissions

Since CO emissions from motor vehicles generally increase with decreasing vehicle speed, disruption of traffic during construction (such as the temporary reduction of roadway capacity and the increased queue lengths) could result in short-term, elevated concentrations of CO. In order to minimize the amount of emissions generated, every effort should be made during the construction phase to limit disruption to traffic, especially during peak travel hours.

4.0 CONCLUSION

The Brent Spence Bridge Replacement/Rehabilitation project, identified as Kentucky Transportation Cabinet Project ID 6-17.03, 6-17.04, and Ohio Department of Transportation PID 75119, was included in the regional emissions analysis conducted by the Ohio Kentucky Regional Council of Governments for the 2030 Regional Transportation Plan and the Fiscal Year 2008-2011 Transportation Improvement Plan, dated June 2008. This analysis found that the plan and, therefore, the individual projects contained in the plan, are conforming projects, and will have air quality impacts consistent with those identified in the State Implementation Plans for achieving the National Ambient Air Quality Standards (NAAQS). In addition, the result of the air quality analyses conducted for the proposed project is that it would not cause an exceedance of the carbon monoxide NAAQS.

5.0 REFERENCES

Federal Highway Administration. *Transportation Conformity Reference Guide*. 2008.
<http://www.fhwa.dot.gov/environment/conform.htm>

Kentucky Transportation Cabinet, August, 2010. <http://transportation.ky.gov/>

Ohio, Kentucky, Indiana Regional Council of Governments. Air Quality Conformity Determination of the OKI 2030 Regional Transportation Plan", 2010.
<http://www.oki.org/environment/aqtransportation.html>

US Environmental Protection Agency, Air Quality Analysis Branch, User's Guide to Mobile6.2, USEPA-TEB-92-01 <http://www.epa.gov/oms/m6.htm>

US Environmental Protection Agency, Airsdata, 2010.
<http://www.epa.gov/air/data/geosel.html>

US Environmental Protection Agency, Office of Air Quality Planning and Standards, User's Guide to CAL3QHC Version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations near Roadway Intersections, USEPA -454/R-92-006 <http://nepis.epa.gov>

Appendix A Monitored Data
Appendix B MOBILE6.2 Input and Output Files
Appendix C CAL3QHC Input and Output Files

Appendix A
Monitored Data



AirData

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AirData - Monitor Values Report - Criteria Air Pollutants
Generated on Thursday, April 1, 2010

EPA is assessing its data systems, including AirData reports and maps. Data updates are suspended while the assessment is underway. The last update included data through January 10, 2009; see [database status](#) for details. For more recent air quality data, visit the [AirExplorer](#) and [Air Emission Sources](#) sites.

Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Carbon Monoxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Carbon Monoxide: 35 ppm (1-hour average), 9 ppm (8-hour average)

ppm = parts per million

46 Rows

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Row #	# Obs	1-Hour Values			8-Hour Values			Monitor Number	Year	Site ID	Site Address	City	County	State	EPA Region
		1st Max	2nd Max	# Exceed	1st Max	2nd Max	# Exceed								
		Sort	1st Max	2nd Max	# Exceed	1st Max	2nd Max								
1	7,928	2.6	2.6	0	1.8	1.8	0	1	391530022	177 S. Broadway	Akron	Summit Co	OH	05	
2	8,389	2.2	2.0	0	1.7	1.4	0	1	391530020	800 Patterson Ave.	Akron	Summit Co	OH	05	
3	8,363	2.7	2.5	0	1.2	1.1	0	1	391530022	177 S. Broadway	Akron	Summit Co	OH	05	
4	8,382	2.3	1.7	0	1.6	1.4	0	1	391530020	800 Patterson Ave.	Akron	Summit Co	OH	05	
5	7,003	1.7	1.6	0	1.3	1.1	0	1	391530020	800 Patterson Ave.	Akron	Summit Co	OH	05	
6	6,948	2.0	1.5	0	0.9	0.8	0	1	391530022	177 S. Broadway	Akron	Summit Co	OH	05	
7	7,750	3.5	3.3	0	2.7	2.2	0	1	391510020	420 Market	Canton	Stark Co	OH	05	
8	8,311	2.1	2.1	0	1.8	1.7	0	1	391510020	420 Market	Canton	Stark Co	OH	05	
9	6,158	2.9	2.9	0	2.6	2.5	0	1	391510020	420 Market	Canton	Stark Co	OH	05	
10	8,636	10.6	9.9	0	4.3	3.0	0	1	390610021	100 E. 5th St.	Cincinnati	Hamilton Co	OH	05	

11	8,706	4.9	4.1	0	3.1	2.8	0	1	2007	390610021	100 E. 5th St.	Cincinnati	Hamilton Co	OH	05
12	6,358	5.9	5.1	0	3.6	2.7	0	1	2008	390610021	100 E. 5th St.	Cincinnati	Hamilton Co	OH	05
13	8,592	7.8	7.3	0	5.8	3.9	0	1	2006	390350051	1301 E. 9th St.	Cleveland	Cuyahoga Co	OH	05
14	8,441	5.0	2.8	0	1.8	1.6	0	1	2006	390350048	2026 East 9th St.	Cleveland	Cuyahoga Co	OH	05
15	8,533	5.0	4.0	0	2.2	2.0	0	1	2006	390350053	4169 Pearl Rd.	Cleveland	Cuyahoga Co	OH	05
16	8,590	2.5	2.3	0	1.6	1.5	0	1	2006	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
17	8,576	3.8	3.0	0	2.0	1.5	0	1	2007	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
18	8,282	7.0	6.7	0	3.1	2.9	0	1	2007	390350051	1301 E. 9th St.	Cleveland	Cuyahoga Co	OH	05
19	8,581	6.0	5.0	0	3.4	2.6	0	1	2007	390350048	2026 East 9th St.	Cleveland	Cuyahoga Co	OH	05
20	8,642	2.5	2.5	0	2.5	2.3	0	1	2007	390350053	4169 Pearl Rd.	Cleveland	Cuyahoga Co	OH	05
21	6,967	4.8	4.8	0	2.1	1.5	0	1	2008	390350048	2026 East 9th St.	Cleveland	Cuyahoga Co	OH	05
22	7,252	2.0	2.0	0	1.2	1.2	0	1	2008	390350053	4169 Pearl Rd.	Cleveland	Cuyahoga Co	OH	05
23	7,023	7.8	6.3	0	3.3	2.4	0	1	2008	390350051	1301 E. 9th St.	Cleveland	Cuyahoga Co	OH	05
24	7,232	2.0	1.8	0	1.5	1.3	0	1	2008	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
25	8,582	3.6	2.9	0	2.4	2.1	0	1	2006	390490005	1585 Morse Rd.	Columbus	Franklin Co	OH	05
26	8,607	2.9	2.4	0	2.0	1.6	0	1	2006	390490036	122 S. Front St.	Columbus	Franklin Co	OH	05
27	6,722	1.7	1.6	0	1.1	1.1	0	1	2007	390490036	122 S. Front St.	Columbus	Franklin Co	OH	05
28	8,590	2.4	2.3	0	1.6	1.6	0	1	2007	390490005	1585 Morse Rd.	Columbus	Franklin Co	OH	05
29	7,183	2.7	2.3	0	1.6	1.4	0	1	2008	390490005	1585 Morse Rd.	Columbus	Franklin Co	OH	05
30	8,724	2.8	2.6	0	2.0	1.9	0	1	2006	391130034	117 South Main St.	Dayton	Montgomery Co	OH	05
31	8,711	4.5	4.2	0	2.6	1.5	0	1	2006	391130028	901 West Fairview Ave.	Dayton	Montgomery Co	OH	05
32	8,680	4.7	4.2	0	2.5	1.6	0	1	2007	391130028	901 West Fairview Ave.	Dayton	Montgomery Co	OH	05
33	8,719	4.4	3.0	0	1.5	1.5	0	1	2007	391130034	117 South Main St.	Dayton	Montgomery Co	OH	05
34	8,739	2.3	2.3	0	1.6	1.5	0	1	2008	391130034	117 South Main St.	Dayton	Montgomery Co	OH	05
35	8,720	1.5	1.4	0	1.1	1.0	0	1	2008	391130028	901 West Fairview Ave.	Dayton	Montgomery Co	OH	05
36	8,398	4.3	3.2	0	3.1	2.7	0	1	2006	211110046	3510 Goldsmith Lane, Seneca High School	Louisville	Jefferson Co	KY	04
37	8,598	11.4	4.9	0	3.1	2.8	0	1	2006	211111019	1735 Bardstown Rd, Fire Station #20	Louisville	Jefferson Co	KY	04
38	8,538	4.1	3.7	0	2.2	2.1	0	1	2007	211111019	1735 Bardstown Rd, Fire Station #20	Louisville	Jefferson Co	KY	04



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AirData - Monitor Values Report - Criteria Air Pollutants
Generated on Thursday, April 1, 2010

EPA is assessing its data systems, including AirData reports and maps. Data updates are suspended while the assessment is underway. The last update included data through January 10, 2009; see [database status](#) for details. For more recent air quality data, visit the [AirExplorer](#) and [Air Emission Sources](#) sites.

Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Nitrogen Dioxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Nitrogen Dioxide: 0.053 ppm (annual mean)

ppm = parts per million

36 Rows

See Disclaimer

Row #	NO2 (ppm)												
	1-Hour Values					Annual							
	# Obs	1st Max	2nd Max	Mean	# Exceed	Monitor Number	Year	Site ID	Site Address	City	County	State	EPA Region
SORT													
1	7,183	0.049	0.043	0.010	0	1	2006	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co	KY	04
2	8,158	0.059	0.055	0.011	0	1	2007	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co	KY	04
3	6,207	0.056	0.050	0.010	0	1	2008	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co	KY	04
4	7,891	0.046	0.045	0.008	0	1	2006	210290006	2nd & Carpenter Sts	Shepherdsville	Bullitt Co	KY	04
5	1,662	0.052	0.047	0.011	0	1	2007	210290006	2nd & Carpenter Sts	Shepherdsville	Bullitt Co	KY	04
6	1,597	0.052	0.048	0.011	0	1	2006	210370003	700 Alexandria Pk, Water Plt, Ft Thomas	Fort Thomas	Campbell Co	KY	04
7	3,926	0.044	0.041	0.006	0	1	2007	210373002	524a John Hill Road	Highland Heights	Campbell Co	KY	04

8	6,219	0.044	0.044	0.006	0	1	2008	210373002	524a John Hill Road	Highland Heights	Campbell Co	KY	04
9	7,928	0.041	0.041	0.006	0	1	2006	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviess Co	KY	04
10	8,310	0.051	0.049	0.005	0	1	2007	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviess Co	KY	04
11	5,265	0.042	0.038	0.007	0	1	2008	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviess Co	KY	04
12	8,220	0.061	0.061	0.012	0	1	2006	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate N	Fayette Co	KY	04
13	8,126	0.066	0.062	0.011	0	1	2007	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate N	Fayette Co	KY	04
14	6,120	0.051	0.050	0.008	0	1	2008	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate N	Fayette Co	KY	04
15	7,914	0.050	0.050	0.015	0	2	2006	211111021	1918 Mellwood Avenue, Wilky-Tv	Louisville	Jefferson Co	KY	04
16	8,323	0.058	0.055	0.016	0	2	2007	211111021	1918 Mellwood Avenue, Wilky-Tv	Louisville	Jefferson Co	KY	04
17	6,821	0.077	0.064	0.015	0	2	2008	211111021	1918 Mellwood Avenue, Wilky-Tv	Louisville	Jefferson Co	KY	04
18	6,471	0.060	0.060	0.014	0	1	2006	211170007	1401 Dixie Hwy, University College	Covington	Kenton Co	KY	04
19	4,300	0.063	0.062	0.015	0	1	2007	211170007	1401 Dixie Hwy, University College	Covington	Kenton Co	KY	04
20	7,829	0.051	0.051	0.009	0	1	2006	211451024	2901 Powell St, Jackson Purchase Recc	Paducah	McCracken Co	KY	04
21	8,178	0.049	0.047	0.009	0	1	2007	211451024	2901 Powell St, Jackson Purchase Recc	Paducah	McCracken Co	KY	04
22	6,092	0.061	0.053	0.008	0	1	2008	211451024	2901 Powell St, Jackson Purchase Recc	Paducah	McCracken Co	KY	04
23	6,911	0.021	0.020	0.002	0	2	2007	212218001	Old Dover Highway Cadiz, Ky		Trigg Co	KY	04
24	1,329	0.033	0.032	0.004	0	2	2008	212218001	Old Dover Highway Cadiz, Ky		Trigg Co	KY	04
25	7,946	0.049	0.048	0.008	0	1	2006	212270008	Oakland Elementary Sch, Ky 179, Oakland	Oakland	Warren Co	KY	04
26	8,252	0.040	0.037	0.005	0	1	2007	390090004	7760 Blackburn Road	Athens	Athens Co	OH	05
27	7,639	0.064	0.053	0.005	0	1	2008	390090004	7760 Blackburn Road	Athens	Athens Co	OH	05
28	8,396	0.068	0.065	0.018	0	1	2006	390350060	E. 14th & Orange	Cleveland	Cuyahoga Co	OH	05
29	8,390	0.073	0.070	0.020	0	1	2007	390350060	E. 14th & Orange	Cleveland	Cuyahoga Co	OH	05

30	7,103	0.075	0.073	0.017	0	1	2008	390350060	E. 14th & Orange	Cleveland	Cuyahoga Co	OH	05
31	8,457	0.175	0.075	0.014	0	1	2006	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
32	8,508	0.098	0.075	0.016	0	1	2007	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
33	7,052	0.074	0.069	0.014	0	1	2008	390350070	13013 Corlett Ave.	Cleveland	Cuyahoga Co	OH	05
34	8,596	0.061	0.061	0.018	0	1	2006	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
35	8,726	0.081	0.072	0.017	0	1	2007	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
36	7,264	0.079	0.073	0.016	0	1	2008	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
Grand Total					0		2007						
					0		2006						
					0		2008						

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Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Ozone
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Ozone: 0.12 ppm (1-hour average), 0.075 ppm (8-hour average)

ppm = parts per million

238 Rows

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Row #	O3 (ppm)													EPA Region								
	1-Hour Values						8-Hour Values						Year		Site ID	Site Address	City	County	State			
	1st Max	2nd Max	3rd Max	4th Max	Required Days	# Exceed Actual	# Exceed Estimated	Missing Days	% Days	# Days	Days > Std	Required Days								# Days	% Days	Monitor Number
SORT	1st Max	2nd Max	3rd Max	4th Max	Required Days	# Exceed Actual	# Exceed Estimated	Missing Days	% Days	# Days	Days > Std	Required Days	# Days	% Days	Monitor Number	Site ID	Site Address	City	County	State	EPA Region	
1	0.078	0.075	0.073	0.073	245	0	0.0	0	100	245	0	245	245	100	1	2006	211950002	101 North Mayo Trail, Dot District Offic	Pikeville	Pike Co	KY	04
2	0.094	0.094	0.089	0.089	245	0	0.0	1	100	244	9	245	244	100	1	2007	211950002	101 North Mayo Trail, Dot District Offic	Pikeville	Pike Co	KY	04
3	0.083	0.082	0.081	0.080	245	0	0.0	0	100	245	0	245	245	100	1	2008	211950002	101 North Mayo Trail, Dot District Offic	Pikeville	Pike Co	KY	04
4	0.091	0.086	0.085	0.085	245	0	0.0	2	99	243	5	245	241	98	1	2006	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
5	0.105	0.097	0.097	0.092	245	0	0.0	1	99	242	24	245	243	99	1	2007	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
6	0.071	0.070	0.064	0.062	245	0	0.0	0	13	31	0	245	31	13	1	2008	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
7	0.085	0.076	0.076	0.075	242	0	0.0	0	100	242	0	242	242	100	2	2008	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
8	0.095	0.092	0.092	0.092	214	0	0.0	1	100	213	9	214	213	100	1	2006	390610006	11590 Grooms Rd	Cincinnati	Hamilton Co	OH	05
																	11590 Grooms					



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Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Particles < 2.5 micrometers diameter
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Particles < 2.5 micrometers diameter: 35 µg/m3 (24-Hour Average), 15.0 µg/m3 (annual mean)

µg/m3 = micrograms per cubic meter

237 Rows

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Row #	# Obs	PM2.5 (µg/m3)								Year	Site ID	Site Address	City	County	State	EPA Region
		24-Hour Values				Annual										
		1st Max	2nd Max	3rd Max	4th Max	98th Pct	# Exceed	Mean	# Exceed							
SORT																
1	61	30.2	25.7	24.5	24.1	25.7	0	13.75	0	210130002	Middlesboro Airport, 34th & Dorchester	Middlesborough (Corporate Name)	Bell Co	KY	04	
2	59	40.7	29.5	28.2	27.5	29.5	0	15.24	1	210130002	Middlesboro Airport, 34th & Dorchester	Middlesborough (Corporate Name)	Bell Co	KY	04	
3	55	30.3	24.4	23.1	23.1	24.4	0	12.78	0	210130002	Middlesboro Airport, 34th & Dorchester	Middlesborough (Corporate Name)	Bell Co	KY	04	
4	115	48.6	28.9	28.6	28.0	28.6	0	13.76	0	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co	KY	04	

5	117	40.4	39.0	38.5	35.2	38.5	1	14.34	0	1	2007	210190017	St, Fivco Health Dept	Ashland	Boyd Co	KY	04
6	110	27.8	25.8	24.3	23.8	24.3	0	12.17	0	1	2008	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co	KY	04
7	117	39.0	34.3	33.5	30.9	33.5	0	14.14	0	1	2006	210290006	2nd & Carpenter Sts	Shepherdsville	Bullitt Co	KY	04
8	118	46.8	37.7	35.1	34.0	35.1	1	15.14	1	1	2007	210290006	2nd & Carpenter Sts	Shepherdsville	Bullitt Co	KY	04
9	111	29.3	25.9	25.4	24.8	25.4	0	13.13	0	1	2008	210290006	2nd & Carpenter Sts	Shepherdsville	Bullitt Co	KY	04
10	18	25.2	19.8	17.0	16.8	25.2	0	11.54	0	1	2006	210370003	700 Alexandria Pk, Water Plt, Ft Thomas	Fort Thomas	Campbell Co	KY	04
11	50	34.0	33.5	26.3	26.0	34.0	0	14.36	0	1	2007	210373002	524a John Hill Road	Highland Heights	Campbell Co	KY	04
12	109	30.5	27.3	26.1	24.4	26.1	0	11.98	0	1	2008	210373002	524a John Hill Road	Highland Heights	Campbell Co	KY	04
13	112	43.2	26.3	25.5	24.9	25.5	0	11.49	0	1	2006	210430500	Camp Webb Grayson Lake		Carter Co	KY	04
14	116	36.7	31.8	30.9	30.8	30.9	0	12.81	0	1	2007	210430500	Camp Webb Grayson Lake		Carter Co	KY	04
15	111	25.2	24.5	22.6	21.2	22.6	0	10.33	0	1	2008	210430500	Camp Webb Grayson Lake		Carter Co	KY	04
16	115	36.8	30.9	30.3	27.1	30.3	0	12.63	0	1	2006	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
17	116	43.6	39.5	35.5	35.5	35.5	1	13.99	0	1	2007	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
18	107	28.4	27.9	27.2	26.7	27.2	0	12.08	0	1	2008	210470006	10800 Pilot Rock Road, Williamson Res.		Christian Co	KY	04
19	114	42.7	38.2	30.0	28.8	30.0	0	13.05	0	1	2006	210590005	Wyndall Shpg Ctr Us	Owensboro	Davless Co	KY	04

127	113	39.0	38.3	34.0	32.8	34.0	0	13.42	0	1	2006	390490025	1700 Ann St.	Columbus	Franklin Co	OH	05
128	109	40.0	35.6	35.5	31.6	35.5	0	14.67	0	1	2007	390490025	1700 Ann St.	Columbus	Franklin Co	OH	05
129	93	32.6	27.1	26.8	26.4	27.1	0	11.81	0	1	2008	390490025	1700 Ann St.	Columbus	Franklin Co	OH	05
130	87	32.0	31.2	29.9	28.8	31.2	0	12.89	0	1	2006	390490081	5750 Maple Canyon	Columbus	Franklin Co	OH	05
131	106	45.1	38.5	33.5	30.9	33.5	0	13.11	0	1	2007	390490081	5750 Maple Canyon	Columbus	Franklin Co	OH	05
132	95	43.8	30.3	25.3	24.6	30.3	0	10.43	0	1	2008	390490081	5750 Maple Canyon	Columbus	Franklin Co	OH	05
133	119	31.5	28.8	26.5	26.5	26.5	0	11.94	0	1	2006	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
134	116	38.7	34.6	32.6	32.2	32.6	0	13.28	0	1	2007	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
135	109	33.3	26.9	26.8	25.3	26.8	0	11.64	0	1	2008	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
136	118	35.0	34.6	33.3	31.8	33.3	0	13.29	0	1	2006	390610006	11590 Grooms Rd	Cincinnati	Hamilton Co	OH	05
137	296	40.8	39.2	38.1	37.2	34.7	0	14.63	0	1	2007	390610006	11590 Grooms Rd	Cincinnati	Hamilton Co	OH	05
138	154	33.9	28.1	28.1	27.0	27.0	0	12.03	0	1	2008	390610006	11590 Grooms Rd	Cincinnati	Hamilton Co	OH	05
139	58	36.3	35.2	31.5	27.1	35.2	1	15.51	0	1	2006	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
140	109	41.5	38.1	36.5	36.2	36.5	1	16.59	1	1	2007	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
141	99	37.7	33.0	31.7	29.7	33.0	0	14.52	0	1	2008	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
142	48	40.1	33.0	32.1	28.3	40.1	1	14.51	0	2	2008	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
143	121	34.5	33.7	32.8	32.3	32.8	0	13.57	0	1	2006	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
144	107	41.9	35.3	34.7	33.1	34.7	1	15.09	1	1	2007	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
145	90	31.5	26.6	25.5	25.0	26.6	0	12.13	0	1	2008	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
146	122	39.4	37.0	34.5	33.5	34.5	0	14.94	0	1	2006	390610042	2101 W. 8th St.	Cincinnati	Hamilton Co	OH	05
147	110	39.2	36.3	35.9	33.6	35.9	1	15.90	1	1	2007	390610042	2101 W. 8th St.	Cincinnati	Hamilton Co	OH	05
148	91	32.2	27.5	27.5	27.2	27.5	0	14.04	0	1	2008	390610042	2101 W. 8th St.	Cincinnati	Hamilton Co	OH	05
149	118	39.0	35.8	34.9	32.2	34.9	0	14.47	0	1	2006	390610043	3254 E.	Sharonville	Hamilton Co	OH	05



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AirData - Monitor Values Report - Criteria Air Pollutants
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Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Particles < 10 micrometers diameter
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Particles < 10 micrometers diameter: 150 µg/m3 (24-hour average), 50 µg/m3 (annual mean)

µg/m3 = micrograms per cubic meter

177 Rows

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Row #	SORT	PM10 (µg/m3)										EPA Region					
		24-Hour Values					Annual										
		# Obs	1st Max	2nd Max	3rd Max	4th Max	# Exceed Actual	# Exceed Estimated	Mean	# Exceed	Monitor Number						
1	8	28	24	24	23	0	0.0	18	0	1	2006	210130002	Middlesboro Airport, 34th & Dorchester	Middlesborough (Corporate Name)	Bell Co	KY	04
2	59	108	72	68	68	0	0.0	34	0	1	2006	210190002	122 22nd St, Ashland Oil Pad	Ashland	Boyd Co	KY	04
3	57	106	72	72	68	0	0.0	33	0	2	2006	210190002	122 22nd St, Ashland Oil Pad	Ashland	Boyd Co	KY	04
4	58	98	94	92	77	0	0.0	39	0	1	2007	210190002	122 22nd St, Ashland	Ashland	Boyd Co	KY	04

87	47	58	43	43	38	0	0.0	18	0	1	2008	390351002	16900 Holland Rd.	Brook Park	Cuyahoga Co	OH	05
88	61	56	55	54	50	0	0.0	27	0	1	2006	390490024	State Fairgrounds	Columbus	Franklin Co	OH	05
89	59	123	76	72	70	0	0.0	36	0	1	2007	390490024	State Fairgrounds	Columbus	Franklin Co	OH	05
90	51	82	79	61	58	0	0.0	36	0	1	2008	390490024	State Fairgrounds	Columbus	Franklin Co	OH	05
91	363	80	64	60	59	0	0.0	23	0	1	2006	390490034	Korbel Ave.	Columbus	Franklin Co	OH	05
92	161	59	56	56	56	0	0.0	21	0	1	2007	390490034	Korbel Ave.	Columbus	Franklin Co	OH	05
93	58	33	33	30	29	0	0.0	16	0	1	2006	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
94	56	48	38	30	30	0	0.0	18	0	1	2007	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
95	58	32	32	30	29	0	0.0	15	0	1	2008	390570005	100 Dayton St.	Yellow Springs	Greene Co	OH	05
96	60	53	48	46	44	0	0.0	23	0	1	2006	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
97	59	51	49	49	46	0	0.0	26	0	1	2007	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
98	48	48	45	45	42	0	0.0	26	0	1	2008	390610014	Seymour & Vine St.	Cincinnati	Hamilton Co	OH	05
99	59	43	40	38	38	0	0.0	19	0	1	2006	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
100	242	58	56	55	50	0	0.0	22	0	9	2006	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
101	56	46	45	43	42	0	0.0	25	0	1	2007	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
102	49	39	37	35	35	0	0.0	19	0	1	2008	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
103	44	46	42	41	41	0	0.0	25	0	9	2008	390610040	250 Wm. Howard Taft	Cincinnati	Hamilton Co	OH	05
104	58	47	44	42	39	0	0.0	21	0	1	2006	390615001	101 Cooper Ave.	Lockland	Hamilton Co	OH	05
105	52	47	46	45	41	0	0.0	25	0	1	2007	390615001	101 Cooper Ave.	Lockland	Hamilton Co	OH	05
106	50	41	38	35	35	0	0.0	20	0	1	2008	390615001	101 Cooper Ave.	Lockland	Hamilton Co	OH	05



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Monitor Values Report - Criteria Air Pollutants

Geographic Area: Kentucky, Ohio
Pollutant: Sulfur Dioxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:

Sulfur Dioxide: 0.5 ppm (3-hour average), 0.14 ppm (24-hour average), 0.030 ppm (annual mean)

ppm = parts per million

125 Rows

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Row #	SO2 (ppm)														County	City	Site Address	Site ID	Year	Monitor Number
	1-Hour Values			3-Hour Values			24-Hour Values			Annual										
	# Obs	1st Max	2nd Max	1st Max	2nd Max	# Exceed	1st Max	2nd Max	# Exceed	Mean	# Exceed									
1	8,713	0.132	0.067	0.059	0.047	0	0.018	0.016	0	0.004	0	0.004	0	0.004	1	2006	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co
2	8,684	0.118	0.084	0.078	0.046	0	0.023	0.016	0	0.004	0	0.004	0	0.003	1	2007	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co
3	6,513	0.046	0.045	0.031	0.030	0	0.012	0.011	0	0.003	0	0.003	0	0.003	1	2008	210190017	2924 Holt St, Fivco Health Dept	Ashland	Boyd Co
4	1,588	0.064	0.061	0.053	0.046	0	0.015	0.014	0	0.005	0	0.005	0	0.005	1	2006	210370003	700 Alexandria Pk, Water Pit, Ft	Fort Thomas	Campbell Co

5	4,136	0.129	0.078	0.080	0.056	0	0.020	0.015	0	0.004	0	1	2007	210373002	Thomas	Highland Heights	Campbell Co	K\			
6	6,326	0.076	0.072	0.048	0.046	0	0.017	0.015	0	0.003	0	1	2008	210373002	Thomas	Highland Heights	Campbell Co	K\			
7	8,448	0.081	0.064	0.061	0.042	0	0.014	0.013	0	0.004	0	1	2006	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviss Co	K\			
8	8,206	0.088	0.067	0.054	0.048	0	0.016	0.015	0	0.005	0	1	2007	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviss Co	K\			
9	5,181	0.107	0.062	0.048	0.044	0	0.013	0.011	0	0.003	0	1	2008	210590005	Wyndall Shpg Ctr Us 60 & Plsnt Valley Rd	Owensboro	Daviss Co	K\			
10	7,735	0.055	0.048	0.042	0.031	0	0.013	0.013	0	0.004	0	1	2006	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate)	Fayette Co	K\			
11	8,685	0.069	0.057	0.044	0.034	0	0.017	0.010	0	0.004	0	1	2007	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate)	Fayette Co	K\			
12	6,365	0.044	0.041	0.027	0.022	0	0.009	0.008	0	0.003	0	1	2008	210670012	650 Newtown Pike, Fayette Co Health Dept	Lexington-Fayette (Corporate)	Fayette Co	K\			
13	8,221	0.050	0.049	0.042	0.033	0	0.017	0.016	0	0.004	0	1	2006	210890007	Scott & Center Streets, Worthington	Worthington	Greenup Co	K\			
14	8,625	0.067	0.049	0.042	0.035	0	0.023	0.014	0	0.004	0	1	2007	210890007	Scott & Center Streets, Worthington	Worthington	Greenup Co	K\			
15	6,533	0.041	0.035	0.028	0.025	0	0.014	0.012	0	0.003	0	1	2008	210890007	Scott & Center Streets, Worthington	Worthington	Greenup Co	K\			
16	8,704	0.107	0.102	0.085	0.081	0	0.028	0.022	0	0.003	0	1	2006	211010014	Baskett Fire Department		Henderson Co	K\			
															Baskett Fire			Henderson			

Appendix B

MOBILE 6.2

Input and Output Files

REGIONAL MOBILE6.2 INPUT AND OUTPUT FILES

* Mobile6 input file for Kentucky

*
***** Header Section *****
MOBILE6 INPUT FILE :
POLLUTANTS : NOx HC
PARTICULATES :
* PARTICULATES REPORTED IN *.PM FILE

RUN DATA
***** Run Section *****

REG DIST : KYREG.d
FUEL PROGRAM : 1
OXYGENATED FUELS : .000 .420 .000 .036 2
STAGE II REFUELING : 93 3 86. 86.

EXPAND BUS EFS :
REBUILD EFFECTS : 0.10

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 57.6 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 45.6 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 12.9 freeway
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 58.1 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 46.3 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 12.6 freeway
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 58.1 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 7
FUEL RVP : 7.8
MIN/MAX TEMP : 62.0 91.3
AVERAGE SPEED : 46.2 Non-Ramp
PARTICLE SIZE : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Summer Scenario Section *****

```

SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 12.5 freeway
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 18.6 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 18.7 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 18.8 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Summer Scenario Section *****
SCENARIO RECORD : Brent Spence NOx HC PM2.5 emissions 2035
CALENDAR YEAR  : 2035
EVALUATION MONTH : 7
FUEL RVP       : 7.8
MIN/MAX TEMP   : 62.0 91.3
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE  : 10.
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** End of Run *****

```

```

END OF RUN

```

* MOBILE6.2.03 (24-Sep-2003) *
* Input File: K35REGS.INP (file 1, run 1). *

* Reading Registration Distributions from the following external
* data file: KYREG.D
M616 Comment: User has supplied post-1999 sulfur levels.
M601 Comment: User has enabled STAGE II REFUELING.

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 1.
* #####

M581 Warning:
The user supplied freeway average speed of 57.6
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b
M 48 Warning:
there are no sales for vehicle class LDDT12
HDDV DEFEAT DEVICE EFFECTS ARE PRESENT. THE REBUILD FRACTION IS 0.10.

* Reading Ammonia (NH3) Basic Emission Rates
* from the external data file PMNH3BER.D

* Reading Ammonia (NH3) Sulfur Deterioration Rates
* from the external data file PMNH3SDR.D

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm
Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx, and Veh. Type breakdown (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 2.
* #####

M581 Warning:
The user supplied freeway average speed of 45.6
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels

* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:	<6000	>6000	(All)							
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.240	0.291	0.462	0.333	0.225	0.036	0.086	0.171	2.12	0.298
Composite NOX :	0.191	0.290	0.461	0.332	0.182	0.025	0.112	0.439	1.21	0.300
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite VOC :	0.433	0.171	0.204							
Composite NOX :	0.319	0.702	0.521							

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 3.
* #####
M582 Warning:

The user supplied freeway average speed of 12.9 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No

ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.435	0.472	0.722	0.533	0.559	0.070	0.171	0.432	3.34	0.511
Composite NOX :	0.220	0.309	0.495	0.354	0.141	0.030	0.136	0.535	0.94	0.327
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite VOC :	0.933	0.432	0.517							
Composite NOX :	0.247	0.855	0.634							

* #####
* Brent Spence NOx HC PM2.5 emissions 2035

* File 1, Run 1, Scenario 4.
* #####
* M581 Warning:
The user supplied freeway average speed of 58.1
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV
M 48 Warning:
there are no sales for vehicle class HDGV8b
M 48 Warning:
there are no sales for vehicle class LDDT12
M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.224	0.278	0.437	0.317	0.201	0.033	0.080	0.152	2.30	0.282
Composite NOX :	0.197	0.304	0.481	0.348	0.198	0.034	0.154	0.609	1.50	0.328
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite VOC :	0.392	0.152	0.182							
Composite NOX :	0.347	0.974	0.722							

* #####
* Brent Spence NOx HC PM2.5 emissions 2035

* File 1, Run 1, Scenario 5.
* #####
* M581 Warning:
The user supplied freeway average speed of 46.3
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.239	0.290	0.460	0.332	0.223	0.036	0.086	0.169	2.12	0.297
Composite NOX :	0.191	0.291	0.462	0.333	0.183	0.025	0.114	0.445	1.22	0.301

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.430	0.169	0.202							
Composite NOX :	0.320	0.712	0.528							

* #####
 Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 6.
 * #####
 M582 Warning:
 The user supplied freeway average speed of 12.6
 will be used for all hours of the day. 100% of VMT
 has been assigned to a fixed combination of freeways
 and freeway ramps for all hours of the day and all
 vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi

Weathered RVP: 8.0 psi
Fuel Sul fur Content: 30.0 ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT, HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors, and Veh. Type breakdown.

* #####
* Brent Spence Nox HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 7.
* #####

M581 Warning:
The user supplied freeway average speed of 58.1
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehi cle class HDGV8b

M 48 Warning: there are no sales for vehi cle class LDDT12

M111 Warning: The input diesel sul fur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sul fur li mit of 15 ppm.

Calendar Year: 2035
Month: July
Al ti tude: Low
Mi ni mum Temperature: 62.0 (F)
Maxi mum Temperature: 91.3 (F)
Absolute Humi di ty: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sul fur Content: 30.0 ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT, HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors, and Veh. Type breakdown.

* #####
* Brent Spence Nox HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 8.
* #####

M581 Warning:

The user supplied freeway average speed of 46.2 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWR:		<6000	>6000	(All)						
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC:	0.239	0.290	0.460	0.332	0.223	0.036	0.086	0.169	2.12	0.297
Composite NOX:	0.191	0.291	0.462	0.333	0.182	0.025	0.114	0.444	1.22	0.301

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC:	0.430	0.169	0.203							
Composite NOX:	0.320	0.711	0.527							

 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 9.
 * #####

M582 Warning:

The user supplied freeway average speed of 12.5 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July

Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.445	0.482	0.737	0.545	0.572	0.071	0.174	0.440	3.39	0.522
Composite NOX :	0.224	0.314	0.503	0.360	0.141	0.030	0.137	0.541	0.94	0.332

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.953	0.439	0.526							
Composite NOX :	0.247	0.865	0.642							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 10.
 * #####

M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.291	0.332	0.526	0.380	0.313	0.048	0.116	0.261	2.47	0.352
Composite NOX :	0.199	0.292	0.466	0.335	0.158	0.023	0.105	0.410	1.07	0.300

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.566	0.261	0.312							
Composite NOX :	0.277	0.656	0.486							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 11.
 * #####

M583 Warning:
 The user supplied arterial average speed of 18.6
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.351	0.393	0.613	0.447	0.413	0.059	0.145	0.350	2.83	0.422
Composite NOX :	0.226	0.322	0.511	0.369	0.147	0.026	0.119	0.466	0.97	0.331

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.717	0.349	0.419							
Composite NOX :	0.257	0.745	0.553							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 12.
 * #####

M583 Warning:
 The user supplied arterial average speed of 21.4
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds

the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.323	0.363	0.573	0.415	0.368	0.055	0.134	0.316	2.68	0.390
Composite NOX :	0.215	0.309	0.492	0.355	0.150	0.025	0.113	0.442	1.00	0.318

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.651	0.315	0.378							
Composite NOX :	0.264	0.707	0.524							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 13.
 * #####
 * M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.291	0.332	0.526	0.380	0.313	0.048	0.116	0.261	2.47	0.352
Composite NOX :	0.199	0.292	0.466	0.335	0.158	0.023	0.105	0.410	1.07	0.300

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composi te Emi ssi on Factors (g/mi):
 Composi te VOC : 0.566 0.261 0.312
 Composi te NOX : 0.277 0.656 0.486

* #####
 * Brent Spence NOx HC PM2.5 emi ssi ons 2035
 * File 1, Run 1, Scenari o 14.
 * #####

M583 Warning:
 The user suppl ied arteri al average speed of 18.7
 wi ll be used for all hours of the day. 100% of VMT
 has been assi gned to the arteri al/col l ector roadway
 type for all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deteri orati on Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deteri orati on Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehi cle class HDGV8b

M 48 Warning:
 there are no sales for vehi cle class LDDT12

M111 Warning:
 The input diesel sul fur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sul fur l i mi t of 15 ppm.

Calendar Year: 2035
 Month: Jul y
 Al ti tude: Low
 Mini mum Temperature: 62.0 (F)
 Maxi mum Temperature: 91.3 (F)
 Absolut e Humi di ty: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformul ated Gas: No

Ether Blend Market Share: 0.000 Al coh ol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Al coh ol Blend Oxygen Content: 0.036
 Al coh ol Blend RVP Wai ver: Yes

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
VMT Di stri buti on:	0.2805	0.4458	0.1461	-----	0.0354	0.0003	0.0021	0.0849	0.0050	1.0000
Composi te Emi ssi on Factors (g/mi):										
Composi te VOC :	0.350	0.391	0.611	0.445	0.411	0.059	0.144	0.349	2.82	0.420
Composi te NOX :	0.226	0.321	0.510	0.368	0.147	0.026	0.119	0.465	0.97	0.331

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):
 Composi te VOC : 0.715 0.348 0.417
 Composi te NOX : 0.258 0.744 0.552

* #####
 * Brent Spence NOx HC PM2.5 emi ssi ons 2035
 * File 1, Run 1, Scenari o 15.
 * #####

M583 Warning:
 The user suppl ied arteri al average speed of 21.4
 wi ll be used for all hours of the day. 100% of VMT
 has been assi gned to the arteri al/col l ector roadway
 type for all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deteri orati on Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deteri orati on Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehi cle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx, and Veh. Type (GasBUS, URBAN, SCHOOL) with VMT Mix.

* #####
Brent Spence NOx HC PM2.5 emissions 2035
File 1, Run 1, Scenario 16
#####

M583 Warning:
The user supplied arterial average speed of 27.1
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx.

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

 Composite Emission Factors (g/mi):
 Composite VOC : 0.566 0.261 0.312
 Composite NOX : 0.277 0.656 0.486

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####
 * M583 Warning:
 The user supplied arterial average speed of 18.8
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.348	0.390	0.610	0.444	0.409	0.059	0.144	0.347	2.82	0.419
Composite NOX :	0.225	0.321	0.509	0.367	0.147	0.026	0.118	0.464	0.97	0.330

 Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composite Emission Factors (g/mi):
 Composite VOC : 0.712 0.347 0.416
 Composite NOX : 0.258 0.742 0.551

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 18.
 * #####
 * M583 Warning:
 The user supplied arterial average speed of 21.4
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning: there are no sales for vehicle class HDGV8b
 M 48 Warning: there are no sales for vehicle class LDDT12
 M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type: GWR:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2805	0.4458	0.1461		0.0354	0.0003	0.0021	0.0849	0.0050	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.323	0.363	0.573	0.415	0.368	0.055	0.134	0.316	2.68	0.390
Composite NOX :	0.215	0.309	0.492	0.355	0.150	0.025	0.113	0.442	1.00	0.318

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.651	0.315	0.378							
Composite NOX :	0.264	0.707	0.524							

* Mobile6 input file for Kentucky

*
***** Header Section *****
MOBILE6 INPUT FILE :
POLLUTANTS : CO
PARTICULATES :
* PARTICULATES REPORTED IN *.PM FILE

RUN DATA
***** Run Section *****

REG DIST : KYREG.d
FUEL PROGRAM : 1
OXYGENATED FUELS : .000 .420 .000 .036 2
STAGE II REFUELING : 93 3 86. 86.

EXPAND BUS EFS :
REBUILD EFFECTS : 0.10

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 57.6 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 45.6 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 12.9 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 58.1 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 46.3 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 12.6 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 58.1 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 46.2 Non-Ramp
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

```

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 12.5 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 27.1 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 18.6 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 21.4 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 27.1 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 18.7 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 21.4 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 27.1 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 18.8 37.0
AVERAGE SPEED  : 50.0 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 21.4 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43

```

```

***** End of Run *****

```

```

END OF RUN

```

* MOBILE6.2.03 (24-Sep-2003)
* Input file: K2035REG.INP (file 1, run 1).

* # # # # # Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 1.

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT34 (>6000), LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for Lead, GASPm, ECARBON, OCARBON, S04, Total Exhaust PM, Brake, Tire, Total PM, S02, NH3.

Table with columns: Veh. Type, GasBUS, URBAN, SCH00L. Rows include VMT Mix and Composite Emission Factors (g/mi) for Lead, GASPm, ECARBON, OCARBON, S04, Total Exhaust PM, Brake, Tire, Total PM, S02, NH3.

* # # # # # Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 2.

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT34 (>6000), LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for Lead, GASPm, ECARBON, OCARBON, S04, Total Exhaust PM, Brake, Tire, Total PM, S02, NH3.

Table with columns: Veh. Type, GasBUS, URBAN, SCH00L. Rows include VMT Mix and Composite Emission Factors (g/mi) for Lead, GASPm, ECARBON, OCARBON, S04, Total Exhaust PM, Brake, Tire, Total PM, S02, NH3.

* # # # # # Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 3.

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composition Factors (g/mi), and various pollutant emissions (Lead, GASPM, ECARBON, OCARBON, SO4, etc.).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 4.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composition Factors (g/mi), and various pollutant emissions (Lead, GASPM, ECARBON, OCARBON, SO4, etc.).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 5.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

VMT Distribution:	0.2803	0.4463	0.1459		K2035REG. PM 0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0095	0.0164	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927

Veh. Type: GasBUS URBAN SCH00L

VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0127	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0021	0.0044	0.0031							
Total Exhaust PM:	0.0148	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Ti re:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0251	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 6.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Parti cle Size Cutoff: 2.50 Mi crons
Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0113	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0113
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927

Veh. Type: GasBUS URBAN SCH00L

VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0133	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0014	0.0044	0.0031							
Total Exhaust PM:	0.0147	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Ti re:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0253	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 7.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Parti cle Size Cutoff: 2.50 Mi crons
Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053

K2035REG. PM

Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0095	0.0164	0.0084	0.0161	0.0377	0.0033	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0113	0.0927

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	-----	-----
GASPM:	0.0127	-----	-----
ECARBON:	-----	0.0116	0.0118
OCARBON:	-----	0.0091	0.0092
S04:	0.0021	0.0044	0.0031
Total Exhaust PM:	0.0148	0.0251	0.0241
Brake:	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030
Total PM:	0.0231	0.0335	0.0324
S02:	0.0251	0.0623	0.0440
NH3:	0.0451	0.0270	0.0270

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 8.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWR:		<6000	>6000	(All)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0095	0.0164	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	-----	-----
GASPM:	0.0127	-----	-----
ECARBON:	-----	0.0116	0.0118
OCARBON:	-----	0.0091	0.0092
S04:	0.0021	0.0044	0.0031
Total Exhaust PM:	0.0148	0.0251	0.0241
Brake:	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030
Total PM:	0.0231	0.0335	0.0324
S02:	0.0251	0.0623	0.0440
NH3:	0.0451	0.0270	0.0270

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 9.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWR:		<6000	>6000	(All)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0113	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0113
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

NH3: 0.0451 0.0270 0.0270

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Veh. Type: GasBUS URBAN SCH00L
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 13
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Veh. Type: GasBUS URBAN SCH00L
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 14
* #####

Calendar Year: 2035
Month: Jan.

K2035REG. PM

Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Table with columns: Veh. Type, GasBUS, URBAN, SCH00L, VMT Mix. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 15
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Table with columns: Veh. Type, GasBUS, URBAN, SCH00L, VMT Mix. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 16
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composition Emission Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

K2035REG. PM

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0035	0.0034	0.0034	0.0034	0.0034	0.0076	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0006	
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003	
S04:	0.0004	0.0005	0.0005	0.0005	0.0017	0.0004	0.0008	0.0026	0.0001	0.0007	
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050	
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024	
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0168	0.0162	0.0165	0.0258	0.0206	0.0127	
S02:	0.0068	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0113	
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927	

Veh. Type:	GasBUS	URBAN	SCHOOL								
VMT Mi x:	0.0001	0.0009	0.0019								

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----								
GASPM:	0.0130	-----	-----								
ECARBON:	-----	0.0116	0.0118								
OCARBON:	-----	0.0091	0.0092								
S04:	0.0017	0.0044	0.0031								
Total Exhaust PM:	0.0148	0.0251	0.0241								
Brake:	0.0053	0.0053	0.0053								
Ti re:	0.0030	0.0030	0.0030								
Total PM:	0.0231	0.0335	0.0324								
S02:	0.0252	0.0623	0.0440								
NH3:	0.0451	0.0270	0.0270								

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:		<6000	>6000	(AI I)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----								
GASPM:	0.0127	-----	-----								
ECARBON:	-----	0.0116	0.0118								
OCARBON:	-----	0.0091	0.0092								
S04:	0.0021	0.0044	0.0031								
Total Exhaust PM:	0.0148	0.0251	0.0241								
Brake:	0.0053	0.0053	0.0053								
Ti re:	0.0030	0.0030	0.0030								
Total PM:	0.0231	0.0335	0.0324								
S02:	0.0251	0.0623	0.0440								
NH3:	0.0451	0.0270	0.0270								

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 18.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:		<6000	>6000	(AI I)						
VMT Di stri buti on:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

K2035REG. PM										
S02:	0.0067	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0113
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0927

Veh. Type:	GasBUS	URBAN	SCHOOL							

VMT Mi x:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0133	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0014	0.0044	0.0031							
Total Exhaust PM:	0.0147	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Tire:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0253	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

 * MOBILE6.2.03 (24-Sep-2003) *
 * Input file: K2035REG10.INP (file 1, run 1). *

* Reading Registration Distributions from the following external
 * data file: KYREG.D
 M616 Comment: User has supplied post-1999 sulfur levels.
 M601 Comment: User has enabled STAGE II REFUELING.

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 1.
 * #####

M581 Warning:
 The user supplied freeway average speed of 57.6
 will be used for all hours of the day. 100% of VMT
 has been assigned to the freeway roadway type for
 all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 HDDV DEFEAT DEVICE EFFECTS ARE PRESENT. THE REBUILD FRACTION IS 0.10.

* Reading Ammonia (NH3) Basic Emission Rates
 * from the external data file PMNH3BER.D

* Reading Ammonia (NH3) Sulfur Deterioration Rates
 * from the external data file PMNH3SDR.D

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	14.14	13.60	16.84	14.40	7.05	0.470	0.283	0.153	13.05	12.818
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	13.42	0.232	0.157							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 2.
 * #####

M581 Warning:
 The user supplied freeway average speed of 45.6
 will be used for all hours of the day. 100% of VMT
 has been assigned to the freeway roadway type for
 all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 3.
* #####
M582 Warning:

The user supplied freeway average speed of 12.9
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Page 2

Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	13.83	13.11	16.31	13.90	17.03	0.943	0.581	0.432	24.70	12.871
Veh. Type: GasBUS URBAN SCHOOL										
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	32.44	0.654	0.441							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 4.
 * #####
 * M581 Warning:
 The user supplied freeway average speed of 58.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the freeway roadway type for
 all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
 * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
 * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV
 * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	14.17	13.64	16.89	14.44	7.14	0.472	0.285	0.155	13.66	12.858
Veh. Type: GasBUS URBAN SCHOOL										
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	13.61	0.234	0.158							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 5.
 * #####
 * M581 Warning:
 The user supplied freeway average speed of 46.3
 will be used for all hours of the day. 100% of VMT
 has been assigned to the freeway roadway type for
 all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
 * Reading PM Gas Carbon DR2 Levels

* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VTM Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.36	12.72	15.74	13.47	5.82	0.450	0.271	0.142	9.88	11.986

Veh. Type:	GasBUS	URBAN	SCHOOL							
VTM Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	11.10	0.215	0.145							

* #####
* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 6.
* #####

M582 Warning: The user supplied freeway average speed of 12.6 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036

Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	13.92	13.20	16.43	13.99	17.38	0.957	0.590	0.440	25.21	12.964
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	33.11	0.667	0.450							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 7.
 * #####
 * M581 Warning:

The user supplied freeway average speed of 58.1 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	14.17	13.64	16.89	14.44	7.14	0.472	0.285	0.155	13.66	12.858
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	13.61	0.234	0.158							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 8.
 * #####
 * M581 Warning:

The user supplied freeway average speed of 46.2 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:		<6000	>6000	(All)						
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	13.35	12.71	15.73	13.46	5.82	0.450	0.271	0.142	9.88	11.978
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	11.09	0.215	0.145							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 9.
* #####

M582 Warning:
The user supplied freeway average speed of 12.5
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.95	13.23	16.47	14.02	17.50	0.962	0.593	0.443	25.39	12.997

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	33.35	0.671	0.453							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 10.
 * #####

M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	12.63	11.87	14.70	12.57	8.08	0.570	0.347	0.213	13.94	11.356

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	15.40	0.322	0.217							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 11.
 * #####

M583 Warning:
 The user supplied arterial average speed of 18.6
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.24	12.50	15.53	13.25	12.07	0.742	0.455	0.314	18.38	12.101

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	22.99	0.475	0.321							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12.
* #####

M583 Warning: The user supplied arterial average speed of 21.4 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh

GWWR:		<6000	>6000	(All)						
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	12.96	12.21	15.15	12.93	10.40	0.672	0.411	0.272	16.57	11.766

Veh. Type: GasBUS URBAN SCHOOL										

VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.82	0.413	0.279							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 13.
 * #####

M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:		LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000	

Composite Emission Factors (g/mi):											
Composite CO :	12.63	11.87	14.70	12.57	8.08	0.570	0.347	0.213	13.94	11.356	

Veh. Type: GasBUS URBAN SCHOOL											

VMT Mix:	0.0001	0.0009	0.0019								

Composite Emission Factors (g/mi):											
Composite CO :	15.40	0.322	0.217								

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 14.
 * #####

M583 Warning:
 The user supplied arterial average speed of 18.7
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 15
* #####

M583 Warning:
The user supplied arterial average speed of 21.4
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

				K2035REG. TXT						
				0.0353	0.0003	0.0021	0.0848	0.0049	1.0000	
VMT Distribution:	0.2803	0.4463	0.1459							

Composite Emission Factors (g/mi):										
Composite CO :	12.96	12.21	15.15	12.93	10.40	0.672	0.411	0.272	16.57	11.766

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.82	0.413	0.279							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 16.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 27.1 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
- M 48 Warning:
 there are no sales for vehicle class HDGV8b
- M 48 Warning:
 there are no sales for vehicle class LDDT12
- M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	12.63	11.87	14.70	12.57	8.08	0.570	0.347	0.213	13.94	11.356

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	15.40	0.322	0.217							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 50.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates

* from the external data file PMDDR1.CSV
 * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning: there are no sales for vehicle class HDGV8b
 M 48 Warning: there are no sales for vehicle class LDDT12
 M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 18.8 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	13.62	13.02	16.11	13.78	5.96	0.449	0.270	0.141	9.71	12.250
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	11.36	0.214	0.144							

 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 18.
 #####
 M583 Warning: The user supplied arterial average speed of 21.4 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
 * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
 * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV
 * Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV
 * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning: there are no sales for vehicle class HDGV8b
 M 48 Warning: there are no sales for vehicle class LDDT12
 M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459	-----	0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	12.96	12.21	15.15	12.93	10.40	0.672	0.411	0.272	16.57	11.766

Veh. Type:	GasBUS	URBAN	SCHOOL							

VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.82	0.413	0.279							

02035reg.inp
 * Mobile6 input file for Butler, Clermont, Hamilton and Warren counties,
 * low RVP beginning summer 2008
 * created 4/9/07 by ajr, includes annual scenario, low RVP, post 2007
 ***** Header Section *****

MOBILE6 INPUT FILE :
 POLLUTANTS : CO
 PARTICULATES :
 * PARTICULATES REPORTED IN *.PM FILE

RUN DATA
 ***** Run Section *****
 VMT BY HOUR : OHVMT30.Def
 VMT BY FACILITY : OFVMT30.Def
 REG DIST : OHREG_30.D
 FUEL PROGRAM : 1
 OXYGENATED FUELS : .000 .420 .000 .036 2
 STAGE II REFUELING : 93 3 86. 86.
 EXPAND BUS EFS :
 REBUILD EFFECTS : 0.10

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 57.6 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 45.6 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 12.9 freeway
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 58.1 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 46.3 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 12.6 freeway
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 58.1 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 46.2 Non-Ramp

```

PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 12.5 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 18.6 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 18.7 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 18.8 37.0
AVERAGE SPEED : 50.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

***** End of Run *****
END OF RUN

* MOBILE6.2.03 (24-Sep-2003) *
* Input file: O35REGS.INP (file 1, run 1). *

* Reading Hourly VMT distribution from the following external
* data file: OHVMT30.DEF
* Reading Hourly Roadway VMT distribution from the following external
* data file: OFVMT30.DEF

Reading User Supplied ROADWAY VMT Factors

* Reading Registration Distributions from the following external
* data file: OHREG_30.D
M616 Comment: User has supplied post-1999 sulfur levels.
M601 Comment: User has enabled STAGE II REFUELING.

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 1.
* #####
M581 Warning:
The user supplied freeway average speed of 57.6
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV
M 48 Warning:
there are no sales for vehicle class HDGV8b
M 48 Warning:
there are no sales for vehicle class LDDT12
HDDV DEFEAT DEVICE EFFECTS ARE PRESENT. THE REBUILD FRACTION IS 0.10.

* Reading Ammonia (NH3) Basic Emission Rates
* from the external data file PMNH3BER.D

* Reading Ammonia (NH3) Sulfur Deterioration Rates
* from the external data file PMNH3SDR.D
M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm
Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type VMT Mix.

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 2.
* #####
M581 Warning:
The user supplied freeway average speed of 45.6

will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning:
there are no sales for vehicle class HDGV8b
- M 48 Warning:
there are no sales for vehicle class LDDT12
- M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:	<6000	>6000	(All)							
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.284	0.319	0.364	0.331	0.223	0.040	0.083	0.171	2.12	0.309
Composite NOX :	0.232	0.333	0.425	0.358	0.181	0.026	0.113	0.439	1.22	0.329
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							
Composite Emission Factors (g/mi):										
Composite VOC :	0.429	0.171	0.204							
Composite NOX :	0.318	0.702	0.521							

- * #####
- * Brent Spence NOx HC PM2.5 emissions 2035
- * File 1, Run 1, Scenario 3.
- * #####
- M582 Warning:
The user supplied freeway average speed of 12.9 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning:
there are no sales for vehicle class HDGV8b
- M 48 Warning:
there are no sales for vehicle class LDDT12
- M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)

Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulphur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.494	0.511	0.579	0.530	0.550	0.077	0.170	0.432	3.33	0.525
Composite NOX :	0.264	0.354	0.455	0.381	0.141	0.031	0.137	0.535	0.95	0.356

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.919	0.432	0.517							
Composite NOX :	0.247	0.855	0.634							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 4.
 * #####

M581 Warning:
 The user supplied freeway average speed of 58.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the freeway roadway type for
 all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulphur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulphur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulphur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.266	0.305	0.347	0.316	0.200	0.037	0.077	0.152	2.29	0.294
Composite NOX :	0.240	0.350	0.444	0.376	0.198	0.035	0.156	0.609	1.51	0.358

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.389	0.152	0.182							
Composite NOX :	0.347	0.973	0.722							

* #####

* Brent Spence NOx HC PM2.5 emissions 2035

* File 1, Run 1, Scenario 5.

* #####

M581 Warning:

The user supplied freeway average speed of 46.3 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx, and Veh. Type breakdown (GasBUS, URBAN, SCHOOL).

* #####

* Brent Spence NOx HC PM2.5 emissions 2035

* File 1, Run 1, Scenario 6.

* #####

M582 Warning:

The user supplied freeway average speed of 12.6 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC:	0.501	0.520	0.588	0.538	0.559	0.078	0.172	0.438	3.37	0.534
Composite NOX:	0.268	0.358	0.461	0.386	0.140	0.031	0.138	0.539	0.95	0.361

Veh. Type:	GasBUS	URBAN	SCHOOL							
GWWR:	-----	-----	-----							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC:	0.934	0.437	0.524							
Composite NOX:	0.246	0.862	0.640							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 7.
 * #####
 M581 Warning:

The user supplied freeway average speed of 58.1 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC:	0.266	0.305	0.347	0.316	0.200	0.037	0.077	0.152	2.29	0.294
Composite NOX:	0.240	0.350	0.444	0.376	0.198	0.035	0.156	0.609	1.51	0.358

Veh. Type:	GasBUS	URBAN	SCHOOL							
GWWR:	-----	-----	-----							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx, and Veh. Type (GasBUS, URBAN, SCHOOL) with VMT Mix.

* #####
Brent Spence NOx HC PM2.5 emissions 2035
File 1, Run 1, Scenario 10.
#####

M583 Warning:
The user supplied arterial average speed of 27.1
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOx, and Veh. Type (GasBUS, URBAN, SCHOOL) with VMT Mix.

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mi x:	0.0001	0.0010	0.0019

Composite Emission Factors (g/mi):
Composite VOC : 0.559 0.260 0.312
Composite NOX : 0.276 0.655 0.486

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 11.
* #####

M583 Warning:
The user supplied arterial average speed of 18.6
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000
Composite Emission Factors (g/mi):										
Composite VOC :	0.406	0.429	0.489	0.446	0.408	0.065	0.143	0.350	2.82	0.436
Composite NOX :	0.272	0.369	0.472	0.397	0.147	0.027	0.120	0.466	0.98	0.362

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mi x:	0.0001	0.0010	0.0019

Composite Emission Factors (g/mi):
Composite VOC : 0.709 0.349 0.419
Composite NOX : 0.257 0.745 0.553

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 12.
* #####

M583 Warning:
The user supplied arterial average speed of 21.4
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.375	0.398	0.454	0.413	0.364	0.060	0.132	0.316	2.68	0.403
Composite NOX :	0.259	0.355	0.454	0.382	0.150	0.026	0.114	0.442	1.01	0.348

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.644	0.315	0.378							
Composite NOX :	0.263	0.707	0.524							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 13.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
 * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
 * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV
 * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):
 Composite VOC : 0.339 0.363 0.415 0.377 0.310 0.053 0.113 0.261 2.46 0.364
 Composite NOX : 0.240 0.335 0.428 0.360 0.158 0.024 0.106 0.410 1.08 0.328

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mix: 0.0001 0.0010 0.0019

Composite Emission Factors (g/mi):
 Composite VOC : 0.559 0.260 0.312
 Composite NOX : 0.276 0.655 0.486

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 14.
 * #####

M583 Warning:
 The user supplied arterial average speed of 18.7
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):
 Composite VOC : 0.404 0.428 0.488 0.444 0.406 0.065 0.142 0.349 2.82 0.435
 Composite NOX : 0.271 0.369 0.471 0.396 0.147 0.027 0.120 0.465 0.98 0.362

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mix: 0.0001 0.0010 0.0019

Composite Emission Factors (g/mi):
 Composite VOC : 0.706 0.348 0.417
 Composite NOX : 0.257 0.744 0.552

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 15.
 * #####

M583 Warning:
 The user supplied arterial average speed of 21.4
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi) for VOC and NOX, and Veh. Type breakdown (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence NOx HC PM2.5 emissions 2035
* File 1, Run 1, Scenario 16
* #####

M583 Warning: The user supplied arterial average speed of 27.1
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: July
Altitude: Low
Minimum Temperature: 62.0 (F)
Maximum Temperature: 91.3 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 7.8 psi
Weathered RVP: 8.0 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT, HDGV, LDDV, LDDT, HDDV, MC, All Veh. Page 11

GWWR:	<6000	>6000	(All)							
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.339	0.363	0.415	0.377	0.310	0.053	0.113	0.261	2.46	0.364
Composite NOX :	0.240	0.335	0.428	0.360	0.158	0.024	0.106	0.410	1.08	0.328

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.559	0.260	0.312							
Composite NOX :	0.276	0.655	0.486							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####

M583 Warning:
 The user supplied arterial average speed of 18.8
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632		0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.403	0.426	0.486	0.443	0.404	0.065	0.142	0.347	2.81	0.433
Composite NOX :	0.271	0.368	0.470	0.396	0.147	0.027	0.119	0.464	0.98	0.361

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.703	0.347	0.416							
Composite NOX :	0.258	0.742	0.551							

* #####
 * Brent Spence NOx HC PM2.5 emissions 2035
 * File 1, Run 1, Scenario 18.
 * #####

M583 Warning:
 The user supplied arterial average speed of 21.4
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels

* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: July
 Altitude: Low
 Minimum Temperature: 62.0 (F)
 Maximum Temperature: 91.3 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 7.8 psi
 Weathered RVP: 8.0 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type: GWR:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2697	0.4367	0.1632	-----	0.0361	0.0002	0.0024	0.0866	0.0051	1.0000

Composite Emission Factors (g/mi):										
Composite VOC :	0.375	0.398	0.454	0.413	0.364	0.060	0.132	0.316	2.68	0.403
Composite NOX :	0.259	0.355	0.454	0.382	0.150	0.026	0.114	0.442	1.01	0.348

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0010	0.0019							

Composite Emission Factors (g/mi):										
Composite VOC :	0.644	0.315	0.378							
Composite NOX :	0.263	0.707	0.524							

02035reg.inp
 * Mobile6 input file for Butler, Clermont, Hamilton and Warren counties,
 * low RVP beginning summer 2008
 * created 4/9/07 by ajr, includes annual scenario, low RVP, post 2007
 ***** Header Section *****

MOBILE6 INPUT FILE :
 POLLUTANTS : CO
 PARTICULATES :
 * PARTICULATES REPORTED IN *.PM FILE

RUN DATA
 ***** Run Section *****
 VMT BY HOUR : OHVMT30.Def
 VMT BY FACILITY : OFVMT30.Def
 REG DIST : OHREG_30.D
 FUEL PROGRAM : 1
 OXYGENATED FUELS : .000 .420 .000 .036 2
 STAGE II REFUELING : 93 3 86. 86.
 EXPAND BUS EFS :
 REBUILD EFFECTS : 0.10

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 57.6 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 45.6 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 12.9 freeway
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 58.1 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 46.3 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 12.6 freeway
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 58.1 Non-Ramp
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
 DIESEL SULFUR : 43

***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 46.2 Non-Ramp

```

PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 12.5 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 18.6 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 18.7 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 27.1 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 18.8 37.0
AVERAGE SPEED : 50.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

```

***** Winter CO Scenario Section *****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 21.4 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

```

***** End of Run *****
END OF RUN

* MOBILE6.2.03 (24-Sep-2003) *
* Input file: 02035REG.INP (file 1, run 1). *

* Reading Hourly VMT distribution from the following external
* data file: 0HVTM30.DEF

* Reading Hourly Roadway VMT distribution from the following external
* data file: 0FVMT30.DEF

Reading User Supplied ROADWAY VMT Factors

* Reading Registration Distributions from the following external
* data file: 0HREG_30.D

M616 Comment: User has supplied post-1999 sulfur levels.
M601 Comment: User has enabled STAGE II REFUELING.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 1.

* #####
M581 Warning:
The user supplied freeway average speed of 57.6
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV
M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12
HDDV DEFEAT DEVICE EFFECTS ARE PRESENT. THE REBUILD FRACTION IS 0.10.

* Reading Ammonia (NH3) Basic Emission Rates
* from the external data file PMNH3BER.D

* Reading Ammonia (NH3) Sulfur Deterioration Rates
* from the external data file PMNH3SDR.D
M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm
Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 2.
* #####
M581 Warning:
The user supplied freeway average speed of 45.6
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for

all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning: there are no sales for vehicle class HDGV8b
- M 48 Warning: there are no sales for vehicle class LDDT12
- M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:	<6000	>6000	(All)							
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	14.75	13.71	14.70	13.98	5.83	0.475	0.254	0.142	9.93	12.656
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	11.11	0.215	0.145							

- * #####
- * Brent Spence CO emissions 2035
- * File 1, Run 1, Scenario 3.
- * #####
- M582 Warning: The user supplied freeway average speed of 12.9 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning: there are no sales for vehicle class HDGV8b
- M 48 Warning: there are no sales for vehicle class LDDT12
- M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi

Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 4.
* #####

M581 Warning:
The user supplied freeway average speed of 58.1
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV
* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV
M 48 Warning:
there are no sales for vehi cle class HDGV8b
M 48 Warning:
there are no sales for vehi cle class LDDT12
M111 Warning:
The input diesel sul fur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sul fur li mi t of 15 ppm.

Calendar Year: 2035
Month: Jan.
Al ti tude: Low
Mini mum Temperature: 19.0 (F)
Maxi mum Temperature: 37.0 (F)
Absolute Humi di ty: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 5.
* #####

M581 Warning:
The user supplied freeway average speed of 46.3
will be used for all hours of the day. 100% of VMT
has been assigned to the freeway roadway type for
all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VTM Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.81	13.77	14.78	14.05	5.86	0.474	0.254	0.142	9.89	12.715

Veh. Type:	GasBUS	URBAN	SCHOOL							
VTM Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):		
Composite CO :	11.17	0.145

* #####
* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 6.
* #####

M582 Warning:
The user supplied freeway average speed of 12.6
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GVWR, VMT Distribution, Composite Emission Factors (g/mi), Veh. Type, VMT Mix, Composite Emission Factors (g/mi). Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####

* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 7.

* #####

M581 Warning:

The user supplied freeway average speed of 58.1 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GVWR, VMT Distribution, Composite Emission Factors (g/mi), Veh. Type, VMT Mix, Composite Emission Factors (g/mi). Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####

* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 8.

* #####

M581 Warning:

The user supplied freeway average speed of 46.2 will be used for all hours of the day. 100% of VMT has been assigned to the freeway roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:	<6000	>6000	(All)							
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.80	13.76	14.77	14.04	5.86	0.474	0.254	0.142	9.90	12.706

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	11.16	0.215	0.145							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 9.
* #####

M582 Warning: The user supplied freeway average speed of 12.5 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 10
* #####

M583 Warning:
The user supplied arterial average speed of 27.1
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 11
* #####

M583 Warning:
The user supplied arterial average speed of 18.6
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels

* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type: GWR:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.68	13.53	14.53	13.80	12.15	0.777	0.438	0.314	18.42	12.816

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	23.14	0.475	0.321							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12.
* #####

M583 Warning: The user supplied arterial average speed of 21.4 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No

ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.35	13.20	14.14	13.45	10.47	0.704	0.394	0.272	16.60	12.444

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.95	0.413	0.278							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 13.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.96	12.81	13.70	13.05	8.14	0.599	0.330	0.213	13.96	11.992

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	15.50	0.322	0.217							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 14.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 18.7
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.67	13.52	14.51	13.79	12.08	0.774	0.437	0.312	18.35	12.800

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	23.01	0.473	0.319							

* #####
* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 15.
* #####

M583 Warning: The user supplied arterial average speed of 21.4 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.35	13.20	14.14	13.45	10.47	0.704	0.394	0.272	16.60	12.444

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.95	0.413	0.278							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 16.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 27.1
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV
 * Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV
 * Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV
 * Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV
 * Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV
 M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm
 Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.96	12.81	13.70	13.05	8.14	0.599	0.330	0.213	13.96	11.992

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	15.50	0.322	0.217							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####
 M583 Warning:
 The user supplied arterial average speed of 50.0
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV
 * Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2. CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML. CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1. CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2. CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 18.8 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	15.12	14.11	15.16	14.40	6.00	0.473	0.253	0.141	9.72	13.013

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	11.44	0.214	0.144							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 18.
* #####

M583 Warning: The user supplied arterial average speed of 21.4 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML. CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1. CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2. CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML. CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1. CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2. CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Page 12

Ether Blend Oxygen Content: 0.000

Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.35	13.20	14.14	13.45	10.47	0.704	0.394	0.272	16.60	12.444

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	19.95	0.413	0.278							

 * MOBILE6.2.03 (24-Sep-2003) *
 * Input file: 02035REG.INP (file 1, run 1). *

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 1.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L

 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0127	-----	-----	-----	-----	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	0.0116	0.0118	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	0.0091	0.0092	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0021	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0148	0.0251	0.0241	-----	-----	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	-----	-----	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0030	0.0030	0.0030	-----	-----	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0231	0.0335	0.0324	-----	-----	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0251	0.0623	0.0440	-----	-----	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.0451	0.0270	0.0270	-----	-----	0.0068	0.0068	0.0270	0.0113	0.0926

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 2.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L

 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0127	-----	-----	-----	-----	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	0.0116	0.0118	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	0.0091	0.0092	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0021	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0148	0.0251	0.0241	-----	-----	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	-----	-----	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0030	0.0030	0.0030	-----	-----	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0231	0.0335	0.0324	-----	-----	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0251	0.0623	0.0440	-----	-----	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.0451	0.0270	0.0270	-----	-----	0.0068	0.0068	0.0270	0.0113	0.0926

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 3.
 * #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCH00L).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 4.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCH00L).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 5.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

				O2035REG. PM						
				0.0355	0.0002	0.0024	0.0854	0.0049	1.0000	
VMT Distribution:	0.2691	0.4384	0.1639							

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0127	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0021	0.0044	0.0031							
Total Exhaust PM:	0.0148	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Ti re:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0251	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

* #####
 * Brent Spence CO emi ssi ons 2035
 * File 1, Run 1, Scenario 6.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasol i ne Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cl e Si ze Cutoff: 2.50 Mi crons
 Reformulated Gas: No

Vehi cl e Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0133	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0014	0.0044	0.0031							
Total Exhaust PM:	0.0147	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Ti re:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0253	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

* #####
 * Brent Spence CO emi ssi ons 2035
 * File 1, Run 1, Scenario 7.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasol i ne Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cl e Si ze Cutoff: 2.50 Mi crons
 Reformulated Gas: No

Vehi cl e Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053

O2035REG. PM

Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	-----	-----
GASPM:	0.0127	-----	-----
ECARBON:	-----	0.0116	0.0118
OCARBON:	-----	0.0091	0.0092
S04:	0.0021	0.0044	0.0031
Total Exhaust PM:	0.0148	0.0251	0.0241
Brake:	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030
Total PM:	0.0231	0.0335	0.0324
S02:	0.0251	0.0623	0.0440
NH3:	0.0451	0.0270	0.0270

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 8.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:		<6000	>6000	(All)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	-----	-----
GASPM:	0.0127	-----	-----
ECARBON:	-----	0.0116	0.0118
OCARBON:	-----	0.0091	0.0092
S04:	0.0021	0.0044	0.0031
Total Exhaust PM:	0.0148	0.0251	0.0241
Brake:	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030
Total PM:	0.0231	0.0335	0.0324
S02:	0.0251	0.0623	0.0440
NH3:	0.0451	0.0270	0.0270

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 9.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:		<6000	>6000	(All)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):

Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL
VMT Mix:	0.0001	0.0009	0.0019

Composi te Emi ssi on Factors (g/mi):

Lead: 0.0000 -----
 GASPM: 0.0133 -----
 ECARBON: ----- 0.0116 0.0118
 OCARBON: ----- 0.0091 0.0092
 S04: 0.0014 0.0044 0.0031
 Total Exhaust PM: 0.0147 0.0251 0.0241
 Brake: 0.0053 0.0053 0.0053
 Tire: 0.0030 0.0030 0.0030
 Total PM: 0.0231 0.0335 0.0324
 S02: 0.0253 0.0623 0.0440
 NH3: 0.0451 0.0270 0.0270

 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 10.

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0035	0.0034	0.0034	0.0034	0.0076	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0004	0.0005	0.0005	0.0005	0.0017	0.0004	0.0008	0.0026	0.0001	0.0007
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0168	0.0162	0.0165	0.0258	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0130	-----	-----	-----	-----	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	0.0116	0.0118	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	0.0091	0.0092	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0017	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0148	0.0251	0.0241	-----	-----	0.0093	0.0088	0.0092	0.0140	0.0144
Brake:	0.0053	0.0053	0.0053	-----	-----	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030	-----	-----	0.0022	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0231	0.0335	0.0324	-----	-----	0.0168	0.0162	0.0165	0.0207	0.0127
S02:	0.0253	0.0623	0.0440	-----	-----	0.0166	0.0084	0.0161	0.0377	0.0033
NH3:	0.0451	0.0270	0.0270	-----	-----	0.0451	0.0068	0.0068	0.0270	0.0926

 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 11.

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0080	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0013	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0113	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0134	-----	-----	-----	-----	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	0.0116	0.0118	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	0.0091	0.0092	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0013	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0147	0.0251	0.0241	-----	-----	0.0093	0.0088	0.0092	0.0140	0.0144
Brake:	0.0053	0.0053	0.0053	-----	-----	0.0053	0.0053	0.0053	0.0053	0.0053
Tire:	0.0030	0.0030	0.0030	-----	-----	0.0022	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0230	0.0335	0.0324	-----	-----	0.0168	0.0162	0.0165	0.0207	0.0127
S02:	0.0253	0.0623	0.0440	-----	-----	0.0166	0.0084	0.0161	0.0377	0.0033

NH3: 0.0451 0.0270 0.0270

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi):

Veh. Type: GasBUS URBAN SCH00L
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi):

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 13.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 2.50 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi):

Veh. Type: GasBUS URBAN SCH00L
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi):

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 14.
* #####

Calendar Year: 2035
Month: Jan.

O2035REG. PM

Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
VTM Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0080	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0013	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0144	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0113	0.0113	0.0113	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----
GASPM:	0.0134	-----	-----	-----	-----	-----	-----	-----	-----	-----
ECARBON:	-----	0.0116	0.0118	-----	-----	-----	-----	-----	-----	-----
OCARBON:	-----	0.0091	0.0092	-----	-----	-----	-----	-----	-----	-----
S04:	0.0013	0.0044	0.0031	-----	-----	-----	-----	-----	-----	-----
Total Exhaust PM:	0.0147	0.0251	0.0241	-----	-----	-----	-----	-----	-----	-----
Brake:	0.0053	0.0053	0.0053	-----	-----	-----	-----	-----	-----	-----
Ti re:	0.0030	0.0030	0.0030	-----	-----	-----	-----	-----	-----	-----
Total PM:	0.0230	0.0335	0.0324	-----	-----	-----	-----	-----	-----	-----
S02:	0.0253	0.0623	0.0440	-----	-----	-----	-----	-----	-----	-----
NH3:	0.0451	0.0270	0.0270	-----	-----	-----	-----	-----	-----	-----

* #####
 * Brent Spence CO emi ssi ons 2035
 * File 1, Run 1, Scenari o 15
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
VTM Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0007
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0113	0.0112	0.0168	0.0162	0.0165	0.0258	0.0207	0.0127
S02:	0.0067	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCH00L
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----
GASPM:	0.0133	-----	-----	-----	-----	-----	-----	-----	-----	-----
ECARBON:	-----	0.0116	0.0118	-----	-----	-----	-----	-----	-----	-----
OCARBON:	-----	0.0091	0.0092	-----	-----	-----	-----	-----	-----	-----
S04:	0.0014	0.0044	0.0031	-----	-----	-----	-----	-----	-----	-----
Total Exhaust PM:	0.0147	0.0251	0.0241	-----	-----	-----	-----	-----	-----	-----
Brake:	0.0053	0.0053	0.0053	-----	-----	-----	-----	-----	-----	-----
Ti re:	0.0030	0.0030	0.0030	-----	-----	-----	-----	-----	-----	-----
Total PM:	0.0231	0.0335	0.0324	-----	-----	-----	-----	-----	-----	-----
S02:	0.0253	0.0623	0.0440	-----	-----	-----	-----	-----	-----	-----
NH3:	0.0451	0.0270	0.0270	-----	-----	-----	-----	-----	-----	-----

* #####
 * Brent Spence CO emi ssi ons 2035
 * File 1, Run 1, Scenari o 16
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (Al l)	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
VTM Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

O2035REG. PM

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0035	0.0034	0.0034	0.0034	0.0034	0.0076	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003	0.0003
S04:	0.0004	0.0005	0.0005	0.0005	0.0017	0.0004	0.0008	0.0026	0.0001	0.0001	0.0007
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0168	0.0162	0.0165	0.0258	0.0206	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0113	0.0926

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
GASPM:	0.0130	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
ECARBON:	-----	0.0116	0.0118	-----	-----	-----	-----	-----	-----	-----	-----
OCARBON:	-----	0.0091	0.0092	-----	-----	-----	-----	-----	-----	-----	-----
S04:	0.0017	0.0044	0.0031	-----	-----	-----	-----	-----	-----	-----	-----
Total Exhaust PM:	0.0148	0.0251	0.0241	-----	-----	-----	-----	-----	-----	-----	-----
Brake:	0.0053	0.0053	0.0053	-----	-----	-----	-----	-----	-----	-----	-----
Ti re:	0.0030	0.0030	0.0030	-----	-----	-----	-----	-----	-----	-----	-----
Total PM:	0.0231	0.0335	0.0324	-----	-----	-----	-----	-----	-----	-----	-----
S02:	0.0252	0.0623	0.0440	-----	-----	-----	-----	-----	-----	-----	-----
NH3:	0.0451	0.0270	0.0270	-----	-----	-----	-----	-----	-----	-----	-----

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:	<6000	>6000	(AI I)							
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0035	0.0035	0.0035	0.0073	0.0073	-----	-----	-----	0.0142	0.0034
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003	0.0003
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0001	0.0006
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0094	0.0088	0.0092	0.0140	0.0143	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0112	0.0112	0.0169	0.0162	0.0165	0.0258	0.0206	0.0206	0.0127
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0113	0.0926

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
GASPM:	0.0127	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
ECARBON:	-----	0.0116	0.0118	-----	-----	-----	-----	-----	-----	-----	-----
OCARBON:	-----	0.0091	0.0092	-----	-----	-----	-----	-----	-----	-----	-----
S04:	0.0021	0.0044	0.0031	-----	-----	-----	-----	-----	-----	-----	-----
Total Exhaust PM:	0.0148	0.0251	0.0241	-----	-----	-----	-----	-----	-----	-----	-----
Brake:	0.0053	0.0053	0.0053	-----	-----	-----	-----	-----	-----	-----	-----
Ti re:	0.0030	0.0030	0.0030	-----	-----	-----	-----	-----	-----	-----	-----
Total PM:	0.0231	0.0335	0.0324	-----	-----	-----	-----	-----	-----	-----	-----
S02:	0.0251	0.0623	0.0440	-----	-----	-----	-----	-----	-----	-----	-----
NH3:	0.0451	0.0270	0.0270	-----	-----	-----	-----	-----	-----	-----	-----

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 18.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Parti cle Size Cutoff: 2.50 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:	<6000	>6000	(AI I)							
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0034	0.0033	0.0033	0.0033	0.0079	0.0079	-----	-----	-----	0.0142	0.0033
ECARBON:	-----	-----	-----	-----	-----	0.0065	0.0034	0.0075	-----	0.0007	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0018	0.0049	0.0038	-----	0.0003	0.0003
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0002	0.0007
Total Exhaust PM:	0.0039	0.0039	0.0039	0.0039	0.0093	0.0088	0.0092	0.0140	0.0143	0.0143	0.0050
Brake:	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053	0.0053
Ti re:	0.0020	0.0020	0.0020	0.0020	0.0022	0.0020	0.0020	0.0020	0.0065	0.0010	0.0024
Total PM:	0.0112	0.0112	0.0113	0.0112	0.0168	0.0162	0.0165	0.0258	0.0207	0.0207	0.0127

O2035REG. PM										
S02:	0.0067	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL							

VMT Mi x:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0133	-----	-----							
ECARBON:	-----	0.0116	0.0118							
OCARBON:	-----	0.0091	0.0092							
S04:	0.0014	0.0044	0.0031							
Total Exhaust PM:	0.0147	0.0251	0.0241							
Brake:	0.0053	0.0053	0.0053							
Tire:	0.0030	0.0030	0.0030							
Total PM:	0.0231	0.0335	0.0324							
S02:	0.0253	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, AI I Veh. Rows include VMT Di stri buti on, Compo si te Emi ssi on Factors (g/mi), and various pollutant breakdowns like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emi ssi on s 2035
* File 1, Run 1, Scenario 4.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, AI I Veh. Rows include VMT Di stri buti on, Compo si te Emi ssi on Factors (g/mi), and various pollutant breakdowns like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emi ssi on s 2035
* File 1, Run 1, Scenario 5.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, AI I Veh.

				035REG10. PM						
				0.0355	0.0002	0.0024	0.0854	0.0049	1.0000	
VMT Distribution:	0.2691	0.4384	0.1639							

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0040	0.0038	0.0038	0.0038	0.0080	-----	-----	-----	0.0205	0.0037
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
Ti re:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0371	0.0275
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mi x:	0.0001	0.0009	0.0019							

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0140	-----	-----							
ECARBON:	-----	0.0126	0.0128							
OCARBON:	-----	0.0099	0.0100							
S04:	0.0021	0.0044	0.0031							
Total Exhaust PM:	0.0160	0.0269	0.0259							
Brake:	0.0125	0.0125	0.0125							
Ti re:	0.0120	0.0120	0.0120							
Total PM:	0.0406	0.0515	0.0504							
S02:	0.0251	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 6.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Partic le Size Cutoff: 10.00 Mi crons
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Distribution:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0036	0.0036	0.0036	0.0087	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0207	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
Ti re:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mi x:	0.0001	0.0009	0.0019							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 7.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Partic le Size Cutoff: 10.00 Mi crons
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	Al l Veh
GWR:		<6000	>6000	(Al l)						
VMT Distribution:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0040	0.0038	0.0038	0.0038	0.0080	-----	-----	-----	0.0205	0.0037
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125

035REG10. PM

Table with 10 columns: Tire, Total PM, SO2, NH3, and 7 other unlabeled columns. Values range from 0.0080 to 0.0926.

Table with 4 columns: Veh. Type (GasBUS, URBAN, SCHOOL), VMT Mix (0.0001, 0.0009, 0.0019).

Table with 4 columns: Composite Emission Factors (g/mi) for Lead, GASPM, ECARBON, OCARBON, SO4, Total Exhaust PM, Brake, Tire, Total PM, SO2, NH3.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 8.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with 11 columns: Vehicle Type (LDGV, LDGT12, LDGT34, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh), GWR, VMT Distribution (0.2691, 0.4384, 0.1639, 0.0355, 0.0002, 0.0024, 0.0854, 0.0049, 1.0000).

Table with 11 columns: Composite Emission Factors (g/mi) for Lead, GASPM, ECARBON, OCARBON, SO4, Total Exhaust PM, Brake, Tire, Total PM, SO2, NH3.

Table with 4 columns: Veh. Type (GasBUS, URBAN, SCHOOL), VMT Mix (0.0001, 0.0009, 0.0019).

Table with 4 columns: Composite Emission Factors (g/mi) for Lead, GASPM, ECARBON, OCARBON, SO4, Total Exhaust PM, Brake, Tire, Total PM, SO2, NH3.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 9.
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with 11 columns: Vehicle Type (LDGV, LDGT12, LDGT34, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh), GWR, VMT Distribution (0.2691, 0.4384, 0.1639, 0.0355, 0.0002, 0.0024, 0.0854, 0.0049, 1.0000).

Table with 11 columns: Composite Emission Factors (g/mi) for Lead, GASPM, ECARBON, OCARBON, SO4, Total Exhaust PM, Brake, Tire, Total PM, SO2, NH3.

Table with 4 columns: Veh. Type (GasBUS, URBAN, SCHOOL), VMT Mix (0.0001, 0.0009, 0.0019).

Composite Emission Factors (g/mi):

Lead: 0.0000 -----
 GASPM: 0.0146 -----
 ECARBON: ----- 0.0126 0.0128
 OCARBON: ----- 0.0099 0.0100
 S04: 0.0014 0.0044 0.0031
 Total Exhaust PM: 0.0160 0.0269 0.0259
 Brake: 0.0125 0.0125 0.0125
 Tire: 0.0120 0.0120 0.0120
 Total PM: 0.0406 0.0515 0.0504
 S02: 0.0253 0.0623 0.0440
 NH3: 0.0451 0.0270 0.0270

 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 10.

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 10.00 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0038	0.0037	0.0037	0.0037	0.0084	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0004	0.0005	0.0005	0.0005	0.0017	0.0004	0.0008	0.0026	0.0001	0.0007
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
Tire:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275
S02:	0.0068	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0143	-----	-----	-----	-----	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	0.0126	0.0128	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	0.0099	0.0100	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0017	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0207	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
Tire:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 11.

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Particle Size Cutoff: 10.00 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0037	0.0036	0.0036	0.0036	0.0087	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0005	0.0006	0.0006	0.0006	0.0013	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0207	0.0054
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
Tire:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275
S02:	0.0067	0.0088	0.0115	0.0095	0.0166	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Vehi cle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Lead:	0.0000	-----	-----	-----	-----	-----	-----	-----	0.0000	0.0000
GASPM:	0.0147	-----	-----	-----	-----	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	0.0126	0.0128	-----	-----	0.0071	0.0037	0.0082	-----	0.0007
OCARBON:	-----	0.0099	0.0100	-----	-----	0.0020	0.0053	0.0042	-----	0.0004
S04:	0.0013	0.0044	0.0031	-----	-----	0.0004	0.0008	0.0026	0.0002	0.0008
Total Exhaust PM:	0.0160	0.0269	0.0259	-----	-----	0.0096	0.0099	0.0150	0.0207	0.0054
Brake:	0.0125	0.0125	0.0125	-----	-----	0.0125	0.0125	0.0125	0.0125	0.0125
Tire:	0.0120	0.0120	0.0120	-----	-----	0.0080	0.0080	0.0258	0.0040	0.0095
Total PM:	0.0406	0.0515	0.0504	-----	-----	0.0301	0.0304	0.0534	0.0372	0.0275
S02:	0.0253	0.0623	0.0440	-----	-----	0.0084	0.0161	0.0377	0.0033	0.0114

035REG10. PM

Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Veh. Type: GasBUS URBAN SCHOOL
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emi ssi ons 2035
* File 1, Run 1, Scenario 15
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

Veh. Type: GasBUS URBAN SCHOOL
VMT Mix: 0.0001 0.0009 0.0019

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

* #####
* Brent Spence CO emi ssi ons 2035
* File 1, Run 1, Scenario 16
* #####

Calendar Year: 2035
Month: Jan.
Gasoline Fuel Sul fur Content: 30. ppm
Diesel Fuel Sul fur Content: 43. ppm
Particle Size Cutoff: 10.00 Microns
Reformulated Gas: No

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composit e Emi ssi on Factors (g/mi) for various pollutants like Lead, GASPM, ECARBON, etc.

O35REG10. PM

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000
GASPM:	0.0038	0.0037	0.0037	0.0037	0.0037	0.0084	-----	-----	-----	0.0205	0.0036
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007	
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004	
S04:	0.0004	0.0005	0.0005	0.0005	0.0017	0.0004	0.0008	0.0026	0.0001	0.0007	
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054	
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	
Ti re:	0.0080	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0258	0.0040	0.0095	
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275	
S02:	0.0068	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114	
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926	

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----								
GASPM:	0.0143	-----	-----								
ECARBON:	-----	0.0126	0.0128								
OCARBON:	-----	0.0099	0.0100								
S04:	0.0017	0.0044	0.0031								
Total Exhaust PM:	0.0160	0.0269	0.0259								
Brake:	0.0125	0.0125	0.0125								
Ti re:	0.0120	0.0120	0.0120								
Total PM:	0.0406	0.0515	0.0504								
S02:	0.0252	0.0623	0.0440								
NH3:	0.0451	0.0270	0.0270								

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 17.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Partic le Size Cutoff: 10.00 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:		<6000	>6000	(AI I)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000	
GASPM:	0.0040	0.0038	0.0038	0.0038	0.0080	-----	-----	-----	0.0205	0.0037	
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007	
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004	
S04:	0.0002	0.0004	0.0004	0.0004	0.0021	0.0004	0.0008	0.0026	0.0001	0.0006	
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054	
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	
Ti re:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095	
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0371	0.0275	
S02:	0.0068	0.0088	0.0115	0.0096	0.0164	0.0084	0.0161	0.0377	0.0033	0.0115	
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926	

Veh. Type: GasBUS URBAN SCHOOL
 VMT Mi x: 0.0001 0.0009 0.0019

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	-----	-----								
GASPM:	0.0140	-----	-----								
ECARBON:	-----	0.0126	0.0128								
OCARBON:	-----	0.0099	0.0100								
S04:	0.0021	0.0044	0.0031								
Total Exhaust PM:	0.0160	0.0269	0.0259								
Brake:	0.0125	0.0125	0.0125								
Ti re:	0.0120	0.0120	0.0120								
Total PM:	0.0406	0.0515	0.0504								
S02:	0.0251	0.0623	0.0440								
NH3:	0.0451	0.0270	0.0270								

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 18.
 * #####

Calendar Year: 2035
 Month: Jan.
 Gasoline Fuel Sul fur Content: 30. ppm
 Diesel Fuel Sul fur Content: 43. ppm
 Partic le Size Cutoff: 10.00 Microns
 Reformulated Gas: No

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	AI I Veh
GWR:		<6000	>6000	(AI I)						
VMT Di stri buti on:	0.2691	0.4384	0.1639	-----	0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composi te Emi ssi on Factors (g/mi):											
Lead:	0.0000	0.0000	0.0000	0.0000	0.0000	-----	-----	-----	0.0000	0.0000	
GASPM:	0.0037	0.0036	0.0036	0.0036	0.0086	-----	-----	-----	0.0205	0.0036	
ECARBON:	-----	-----	-----	-----	-----	0.0071	0.0037	0.0082	-----	0.0007	
OCARBON:	-----	-----	-----	-----	-----	0.0020	0.0053	0.0042	-----	0.0004	
S04:	0.0005	0.0006	0.0006	0.0006	0.0014	0.0004	0.0008	0.0026	0.0002	0.0007	
Total Exhaust PM:	0.0042	0.0042	0.0042	0.0042	0.0101	0.0096	0.0099	0.0150	0.0206	0.0054	
Brake:	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	
Ti re:	0.0080	0.0080	0.0080	0.0080	0.0086	0.0080	0.0080	0.0258	0.0040	0.0095	
Total PM:	0.0247	0.0247	0.0247	0.0247	0.0313	0.0301	0.0304	0.0534	0.0372	0.0275	

035REG10. PM										
S02:	0.0067	0.0088	0.0115	0.0095	0.0165	0.0084	0.0161	0.0377	0.0033	0.0114
NH3:	0.1017	0.1017	0.1017	0.1017	0.0451	0.0068	0.0068	0.0270	0.0113	0.0926

Veh. Type:	GasBUS	URBAN	SCHOOL							

VMT Mi x:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Lead:	0.0000	-----	-----							
GASPM:	0.0146	-----	-----							
ECARBON:	-----	0.0126	0.0128							
OCARBON:	-----	0.0099	0.0100							
S04:	0.0014	0.0044	0.0031							
Total Exhaust PM:	0.0160	0.0269	0.0259							
Brake:	0.0125	0.0125	0.0125							
Tire:	0.0120	0.0120	0.0120							
Total PM:	0.0406	0.0515	0.0504							
S02:	0.0253	0.0623	0.0440							
NH3:	0.0451	0.0270	0.0270							

MICROSCALE MOBILE6.2 INPUT AND OUTPUT FILES

* Mobile6 input file for Kentucky

*
***** Header Section *****
MOBILE6 INPUT FILE :
POLLUTANTS : CO
PARTICULATES :
* PARTICULATES REPORTED IN *.PM FILE

RUN DATA
***** Run Section *****

REG DIST : KYREG.d
FUEL PROGRAM : 1
OXYGENATED FUELS : .000 .420 .000 .036 2
STAGE II REFUELING : 93 3 86. 86.

EXPAND BUS EFS :
REBUILD EFFECTS : 0.10

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 2.5 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 5.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 10.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 15.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 20.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 25.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 30.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 35.0 freeway
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

```
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 40.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 45.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 50.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 55.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 60.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 65.0 freeway
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 2.5 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 5.0 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 10.0 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR   : 2035
EVALUATION MONTH : 1
FUEL RVP        : 9.0
MIN/MAX TEMP    : 19.0 37.0
AVERAGE SPEED  : 15.0 arterial
PARTICLE SIZE   : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR  : 43
*****
```

***** Winter CO Scenario Section *****

```

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 20.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 25.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 30.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 35.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 40.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 45.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 50.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 55.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 60.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 65.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
DI ESEL SULFUR : 43
*****
***** End of Run *****

```

END OF RUN

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	<6000	>6000	(All)							
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	19.91	19.25	24.46	20.53	30.70	1.469	0.912	0.741	58.32	19.178
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	58.49	1.123	0.758							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 3.
* #####

M582 Warning: The user supplied freeway average speed of 10.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 4.
* #####

M582 Warning:
The user supplied freeway average speed of 15.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 5.
* #####

M582 Warning:
The user supplied freeway average speed of 20.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type: GWR:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	13.03	12.27	15.18	12.99	11.20	0.705	0.432	0.292	17.38	11.850

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	21.35	0.442	0.299							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 6.
 * #####

M582 Warning:
 The user supplied freeway average speed of 25.0
 will be used for all hours of the day. 100% of VMT
 has been assigned to a fixed combination of freeways
 and freeway ramps for all hours of the day and all
 vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b
 M 48 Warning:
 there are no sales for vehicle class LDDT12
 M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####

* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 7.

* #####

M582 Warning:

The user supplied freeway average speed of 30.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####

* Brent Spence CO emissions 2035

* File 1, Run 1, Scenario 8.

* #####

M582 Warning:

The user supplied freeway average speed of 35.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning: there are no sales for vehicle class HDGV8b
- M 48 Warning: there are no sales for vehicle class LDDT12
- M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	<6000	>6000	(All)							
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	12.82	12.08	14.90	12.77	6.38	0.490	0.296	0.166	11.52	11.457
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	12.15	0.251	0.169							

- * #####
- * Brent Spence CO emissions 2035
- * File 1, Run 1, Scenario 9.
- * #####
- M582 Warning: The user supplied freeway average speed of 40.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
- * from the external data file PMGZML.CSV
- * Reading PM Gas Carbon DR1 Levels
- * from the external data file PMGDR1.CSV
- * Reading PM Gas Carbon DR2 Levels
- * from the external data file PMGDR2.CSV
- * Reading PM Diesel Zero Mile Levels
- * from the external data file PMDZML.CSV
- * Reading the First PM Deterioration Rates
- * from the external data file PMDDR1.CSV
- * Reading the Second PM Deterioration Rates
- * from the external data file PMDDR2.CSV
- M 48 Warning: there are no sales for vehicle class HDGV8b
- M 48 Warning: there are no sales for vehicle class LDDT12
- M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi

Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 10
* #####

M582 Warning:
The user supplied freeway average speed of 45.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehi cle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 11
* #####

M582 Warning:
The user supplied freeway average speed of 50.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways

and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12 <6000, LDGT34 >6000, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution and Composite Emission Factors (g/mi) for CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12.
* #####

M582 Warning: The user supplied freeway average speed of 55.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi

Weathered RVP: 9.5 psi
Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 13.
* #####
M582 Warning:

The user supplied freeway average speed of 60.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sul fur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 14.
* #####
M515 Warning:

The combined freeway and ramp average speed entered cannot be greater than 60.7 miles per hour.

M582 Warning: The average speed will be reset to this value. The user supplied freeway average speed of 60.7 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 15.
* #####

M583 Warning: The user supplied arterial average speed of 2.5 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low

type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and VMT Mix.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 24.
* #####
M583 Warning:

The user supplied arterial average speed of 45.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	<6000	>6000	(All)							
VMT Di stri bution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Composi te CO :	13.26	12.61	15.60	13.35	5.77	0.451	0.271	0.142	9.95	11.888
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mi x:	0.0001	0.0009	0.0019							
Composi te Emi ssi on Factors (g/mi):										
Composi te CO :	10.99	0.215	0.145							

* #####

* Brent Spence CO emi ssi ons 2035

* File 1, Run 1, Scenario 25.

* #####

M583 Warning:

The user supplied arterial average speed of 50.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehi cle class HDGV8b

M 48 Warning:

there are no sales for vehi cle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehi cle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	<6000	>6000	(All)							
VMT Di stri bution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composi te Emi ssi on Factors (g/mi):										
Composi te CO :	13.60	13.00	16.09	13.76	5.96	0.449	0.270	0.141	9.70	12.235
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mi x:	0.0001	0.0009	0.0019							
Composi te Emi ssi on Factors (g/mi):										
Composi te CO :	11.36	0.214	0.144							

* #####

* Brent Spence CO emi ssi ons 2035

* File 1, Run 1, Scenario 26.

* #####

M583 Warning:

The user supplied arterial average speed of 55.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehi cle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:	<6000	>6000	(All)							
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	13.95	13.39	16.58	14.18	6.51	0.458	0.276	0.147	9.70	12.597
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	12.39	0.222	0.150							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 27.
* #####

M583 Warning: The user supplied arterial average speed of 60.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No

Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.30	13.78	17.06	14.59	7.50	0.479	0.290	0.159	15.88	13.005

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	14.29	0.241	0.163							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 28.
 * #####

M583 Warning:
 The user supplied arterial average speed of 65.0
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWWR:	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
VMT Distribution:	0.2803	0.4463	0.1459		0.0353	0.0003	0.0021	0.0848	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.64	14.17	17.55	15.00	9.14	0.517	0.313	0.181	22.07	13.437

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	17.41	0.274	0.185							

* Mobile6 input file for Butler, Clermont, Hamilton and Warren counties,

* low RVP beginning summer 2008

* created 4/9/07 by ajr, includes annual scenario, low RVP, post 2007

***** Header Section *****

MOBILE6 INPUT FILE :

POLLUTANTS : CO

PARTICULATES :

* PARTICULATES REPORTED IN *.PM FILE

RUN DATA

***** Run Section *****

VMT BY HOUR : OHVMT30.Def

VMT BY FACILITY : OFVMT30.Def

REG DIST : OHREG_30.D

FUEL PROGRAM : 1

OXYGENATED FUELS : .000 .420 .000 .036 2

STAGE II REFUELING : 93 3 86. 86.

EXPAND BUS EFS :

REBUILD EFFECTS : 0.10

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035

EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0

AVERAGE SPEED : 2.5 freeway

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV
PMDDR2.CSV

DISEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035

EVALUATI ON MONTH : 1
FUEL RVP : 9.0
MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 5.0 freeway
PARTI CLE SI ZE : 2.5
PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035
CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1
FUEL RVP : 9.0
MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 10.0 freeway
PARTI CLE SI ZE : 2.5
PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035
CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1
FUEL RVP : 9.0
MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 15.0 freeway
PARTI CLE SI ZE : 2.5
PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035
CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1
FUEL RVP : 9.0
MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 20.0 freeway
PARTI CLE SI ZE : 2.5

OHI 02035. i np

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 25.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 30.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 35.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARI O RECORD : Brent Spence CO emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 40.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter C0 Scenario Secti on *****

SCENARI O RECORD : Brent Spence C0 emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 45.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter C0 Scenario Secti on *****

SCENARI O RECORD : Brent Spence C0 emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 50.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter C0 Scenario Secti on *****

SCENARI O RECORD : Brent Spence C0 emi ssi ons 2035

CALENDAR YEAR : 2035
EVALUATI ON MONTH : 1

FUEL RVP : 9.0

MI N/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 55.0 freeway

PARTI CLE SI ZE : 2.5

PARTI CULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter C0 Scenario Secti on *****

SCENARI O RECORD : Brent Spence C0 emi ssi ons 2035

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CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 60.0 freeway

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 65.0 freeway

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 2.5 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 5.0 arterial

PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DIESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 10.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DIESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 15.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DIESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035
CALENDAR YEAR : 2035
EVALUATION MONTH : 1
FUEL RVP : 9.0
MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 20.0 arterial
PARTICLE SIZE : 2.5
PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DIESEL SULFUR : 43

***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

OHI 02035. i np

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 25.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 30.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 35.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 40.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV

OHI 02035. i np

PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 45.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 50.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0
AVERAGE SPEED : 55.0 arterial

PARTICLE SIZE : 2.5

PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
PMDDR2. CSV
DI ESEL SULFUR : 43
***** Winter CO Scenario Section *****

SCENARIO RECORD : Brent Spence CO emissions 2035

CALENDAR YEAR : 2035
EVALUATION MONTH : 1

FUEL RVP : 9.0

MIN/MAX TEMP : 19.0 37.0

OHI 02035. inp

AVERAGE SPEED : 60.0 arterial
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
 PMDDR2. CSV
 DIESEL SULFUR : 43
 ***** Winter CO Scenario Section *****
 SCENARIO RECORD : Brent Spence CO emissions 2035
 CALENDAR YEAR : 2035
 EVALUATION MONTH : 1
 FUEL RVP : 9.0
 MIN/MAX TEMP : 19.0 37.0
 AVERAGE SPEED : 65.0 arterial
 PARTICLE SIZE : 2.5
 PARTICULATE EF : PMGZML. CSV PMGDR1. CSV PMGDR2. CSV PMDZML. CSV PMDDR1. CSV
 PMDDR2. CSV
 DIESEL SULFUR : 43
 ***** End of Run *****
 END OF RUN

* #####

M582 Warning:
The user supplied freeway average speed of 5.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Composite CO.

* #####

* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 3.
M582 Warning:
The user supplied freeway average speed of 10.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.

* File 1, Run 1, Scenario 5.
* #####

M582 Warning:
The user supplied freeway average speed of 20.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.39	13.24	14.17	13.49	11.28	0.738	0.415	0.292	17.42	12.513

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	21.48	0.442	0.299							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 6.
* #####

M582 Warning:
The user supplied freeway average speed of 25.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035

* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 8.
* #####

M582 Warning:
The user supplied freeway average speed of 35.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 9.

M582 Warning:
The user supplied freeway average speed of 40.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 11.
* #####

M582 Warning:
The user supplied freeway average speed of 50.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type: GWR:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	15.43	14.41	15.48	14.70	6.25	0.480	0.258	0.145	9.86	13.291

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	11.91	0.220	0.149							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 12.
* #####

M582 Warning:
The user supplied freeway average speed of 55.0
will be used for all hours of the day. 100% of VMT
has been assigned to a fixed combination of freeways
and freeway ramps for all hours of the day and all
vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GWR, VMT Distribution, Composite Emission Factors (g/mi), Composite CO, Veh. Type, VMT Mix. Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 13.
* #####
M582 Warning:

The user supplied freeway average speed of 60.0 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV
* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

- * Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV
M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12
M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GWR, VMT Distribution, Composite Emission Factors (g/mi), Composite CO, Veh. Type, VMT Mix. Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 14.
* #####

M515 Warning:
The combined freeway and ramp average speed entered cannot be greater than 60.7 miles per hour. The average speed will be reset to this value.

M582 Warning:
The user supplied freeway average speed of 60.7 will be used for all hours of the day. 100% of VMT has been assigned to a fixed combination of freeways and freeway ramps for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWR:	<6000	>6000	(All)							
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	16.38	15.47	16.66	15.79	8.98	0.541	0.295	0.180	21.27	14.361
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							
Composite Emission Factors (g/mi):										
Composite CO :	17.11	0.273	0.184							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 15.
* #####

M583 Warning:
The user supplied arterial average speed of 2.5 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors, and Veh. Type breakdown.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 16
* #####

M583 Warning:

The user supplied arterial average speed of 5.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV
* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV
* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors, and Veh. Type breakdown.

Composite Emission Factors (g/mi):
Composite CO : 61.79 1.179 0.796

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 17.
* #####

M583 Warning:
The user supplied arterial average speed of 10.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GWR:		<6000	>6000	(All)						
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000
Composite Emission Factors (g/mi):										
Composite CO :	16.95	15.81	17.15	16.17	21.58	1.168	0.677	0.537	30.98	15.270
Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):
Composite CO : 41.11 0.813 0.549

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 18.
* #####

M583 Warning:
The user supplied arterial average speed of 15.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:

The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GVWR, VMT Distribution, Composite Emission Factors (g/mi), Composite CO, Veh. Type, VMT Mix. Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 19
* #####
M583 Warning:

The user supplied arterial average speed of 20.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

- * Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV
* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b

M 48 Warning: there are no sales for vehicle class LDDT12

M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, GVWR, VMT Distribution, Composite Emission Factors (g/mi), Composite CO, Veh. Type, VMT Mix. Rows include LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 20
* #####

M583 Warning:
The user supplied arterial average speed of 25.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Veh. Type (GasBUS, URBAN, SCHOOL).

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 21
* #####

M583 Warning:
The user supplied arterial average speed of 30.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b

M 48 Warning:
there are no sales for vehicle class LDDT12

M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Composite CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 22.
* #####

M583 Warning:
The user supplied arterial average speed of 35.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

- * Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV
* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV
* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV
* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

- * Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV
* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12
M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Composite CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 23
* #####

M583 Warning:
The user supplied arterial average speed of 40.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b
M 48 Warning:
there are no sales for vehicle class LDDT12
M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12 <6000	LDGT34 >6000	LDGT (All)	HDGV	LDDV	LDDT	HDDV	MC	All Veh
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	14.29	13.20	14.14	13.46	5.94	0.489	0.263	0.150	10.58	12.227

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	11.32	0.227	0.153							

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 24
* #####

M583 Warning:
The user supplied arterial average speed of 45.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning:
there are no sales for vehicle class HDGV8b
M 48 Warning:
there are no sales for vehicle class LDDT12
M111 Warning:
The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035

* File 1, Run 1, Scenario 26.
* #####
M583 Warning:

The user supplied arterial average speed of 55.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12
M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low
Minimum Temperature: 19.0 (F)
Maximum Temperature: 37.0 (F)
Absolute Humidity: 75. grains/lb
Nominal Fuel RVP: 9.0 psi
Weathered RVP: 9.5 psi
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
Evap I/M Program: No
ATP Program: No
Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
Alcohol Blend RVP Waiver: Yes

Table with 11 columns: Vehicle Type, LDGV, LDGT12, LDGT34, LDGT (All), HDGV, LDDV, LDDT, HDDV, MC, All Veh. Rows include VMT Distribution, Composite Emission Factors (g/mi), and Composite CO.

* #####
* Brent Spence CO emissions 2035
* File 1, Run 1, Scenario 27.
* #####
M583 Warning:

The user supplied arterial average speed of 60.0
will be used for all hours of the day. 100% of VMT
has been assigned to the arterial/collector roadway
type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
* from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
* from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
* from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
* from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
* from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
* from the external data file PMDDR2.CSV

M 48 Warning: there are no sales for vehicle class HDGV8b
M 48 Warning: there are no sales for vehicle class LDDT12
M111 Warning: The input diesel sulfur level of 43.0 ppm exceeds
the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
Month: Jan.
Altitude: Low

Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:		<6000	>6000	(All)						
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	15.91	14.98	16.14	15.30	7.55	0.505	0.272	0.159	15.92	13.857

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	14.38	0.241	0.163							

* #####
 * Brent Spence CO emissions 2035
 * File 1, Run 1, Scenario 28.
 * #####

M583 Warning:
 The user supplied arterial average speed of 65.0
 will be used for all hours of the day. 100% of VMT
 has been assigned to the arterial/collector roadway
 type for all hours of the day and all vehicle types.

* Reading PM Gas Carbon ZML Levels
 * from the external data file PMGZML.CSV

* Reading PM Gas Carbon DR1 Levels
 * from the external data file PMGDR1.CSV

* Reading PM Gas Carbon DR2 Levels
 * from the external data file PMGDR2.CSV

* Reading PM Diesel Zero Mile Levels
 * from the external data file PMDZML.CSV

* Reading the First PM Deterioration Rates
 * from the external data file PMDDR1.CSV

* Reading the Second PM Deterioration Rates
 * from the external data file PMDDR2.CSV

M 48 Warning:
 there are no sales for vehicle class HDGV8b

M 48 Warning:
 there are no sales for vehicle class LDDT12

M111 Warning:
 The input diesel sulfur level of 43.0 ppm exceeds
 the 2007 HDD Rule diesel sulfur limit of 15 ppm.

Calendar Year: 2035
 Month: Jan.
 Altitude: Low
 Minimum Temperature: 19.0 (F)
 Maximum Temperature: 37.0 (F)
 Absolute Humidity: 75. grains/lb
 Nominal Fuel RVP: 9.0 psi
 Weathered RVP: 9.5 psi
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: No
 Evap I/M Program: No
 ATP Program: No
 Reformulated Gas: No

Ether Blend Market Share: 0.000 Alcohol Blend Market Share: 0.420
 Ether Blend Oxygen Content: 0.000 Alcohol Blend Oxygen Content: 0.036
 Alcohol Blend RVP Waiver: Yes

Vehicle Type:	LDGV	LDGT12	LDGT34	LDGT	HDGV	LDDV	LDDT	HDDV	MC	All Veh
GVWR:		<6000	>6000	(All)						
VMT Distribution:	0.2691	0.4384	0.1639		0.0355	0.0002	0.0024	0.0854	0.0049	1.0000

Composite Emission Factors (g/mi):										
Composite CO :	16.32	15.43	16.64	15.76	9.20	0.543	0.296	0.181	22.13	14.334

Veh. Type:	GasBUS	URBAN	SCHOOL							
VMT Mix:	0.0001	0.0009	0.0019							

Composite Emission Factors (g/mi):										
Composite CO :	17.53	0.274	0.185							

Appendix C

CAL3QHC

Input and Output Files

2
 33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
 90 59 2.0 160 73.3 1343 1 3
 1
 31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 140.11.5 0. 32. 30.
 1.0 04 1000. 0Y 5 0 72

 Brent Spence Bridge S1altEpm.dat 60.0175.0.0000.000240.30480000 1 1
 R1 SB Mid 264384. 276323. 5.
 R2 SB 164 264321. 276211. 5.
 R3 SB 82 264290. 276136. 5.
 R4 SB Corner 264262. 276069. 5.
 R5 SB Corner 264230. 275990. 5.
 R6 SB 82 264193. 275900. 5.
 R7 SB 164 264151. 275798. 5.
 R8 SB Mid 264103. 275678. 5.
 R9 NB Mid 264155. 275655. 5.
 R10 NB 164 264184. 275729. 5.
 R11 NB 82 264215. 275805. 5.
 R12 NB Corner 264242. 275872. 5.
 R13 EB Corner 264272. 275903. 5.
 R14 EB 82 264340. 275765. 5.
 R15 EB 164 264378. 275678. 5.
 R16 EB Mid 264408. 275600. 5.
 R17 WB Mid 264455. 275722. 5.
 R18 WB 164 264399. 275833. 5.
 R19 WB 82 264362. 275906. 5.
 R20 WB Corner 264330. 275971. 5.
 R21 NB Corner 264319. 276046. 5.
 R22 NB 82 264343. 276114. 5.
 R23 NB 164 264376. 276189. 5.
 R24 NB Mid 264447. 276280. 5.
 Kyles Lane & Dixie Hwy 36 1 1
 1
 01 Dixie NB Appr AG264099.275553.264162.275726. 760.11.5 0. 44. 30.
 1
 02 Dixie NB Appr AG264162.275726.264197.275813. 760.11.5 0. 44. 30.
 1
 03 Dixie NB Appr AG264197.275813.264240.275916. 760.11.5 0. 44. 30.
 2
 03 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
 100 75 2.0 760 73.3 1511 1 3
 1
 04 Dixie NB @ KylesAG264240.275916.264280.276013. 450.11.5 0. 44. 30.
 1
 05 Dixie NB Depart AG264280.276013.264303.276071. 465.11.5 0. 44. 30.
 1
 06 Dixie NB Depart AG264303.276071.264360.276209. 1295.11.5 0. 44. 30.
 1
 07 Dixie NB Depart AG264360.276209.264406.276278. 1295.11.5 0. 44. 30.
 1
 08 Dixie NB Depart AG264406.276278.264446.276325. 1295.11.5 0. 44. 30.
 1
 09 Dixie NB Depart AG264446.276325.264529.276400. 1295.11.5 0. 44. 30.
 1
 10 Dixie SB Appr AG264499.276415.264439.276361. 1600.11.5 0. 44. 30.
 1
 11 Dixie SB Appr AG264439.276361.264381.276288. 1600.11.5 0. 44. 30.
 1
 12 Dixie SB Appr AG264381.276288.264351.276234. 1600.11.5 0. 44. 30.
 1
 13 Dixie SB Appr AG264351.276234.264252.275994. 1600.11.5 0. 44. 30.
 2
 14 Dixie SB Queue AG264276.276054.264321.276161. 0. 24. 2
 100 40 2.0 1600 73.3 1831 1 3
 1
 14 Dixie SB @ KylesAG264252.275994.264236.275956. 505.11.5 0. 40. 30.
 1
 15 Dixie SB Depart AG264236.275956.264179.275824. 665.11.5 0. 44. 30.
 1
 16 Dixie SB Depart AG264179.275824.264143.275732. 1340.11.5 0. 44. 30.
 1
 17 Dixie SB Depart AG264143.275732.264083.275564. 1340.11.5 0. 44. 30.
 1
 18 Dixie NB Rt. AG264240.275916.264284.275929. 310.11.5 0. 32. 30.
 1
 19 Kyles EB @ DixieAG264252.275994.264284.275929. 650.11.5 0. 32. 30.
 1
 20 Kyles EB Depart AG264284.275929.264483.275522. 960.11.5 0. 44. 30.
 1
 21 Kyles WB Appr AG264516.275540.264468.275639. 1240.11.5 0. 56. 30.
 1
 22 Kyles WB Appr AG264468.275639.264359.275852. 1240.11.5 0. 56. 30.
 1
 23 Kyles WB Rt. AG264359.275852.264347.275900. 830.11.5 0. 32. 30.
 1
 24 Kyles WB Rt. AG264347.275900.264300.276003. 830.11.5 0. 32. 30.
 2
 25 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
 100 58 2.0 830 73.3 1599 1 3
 1
 25 Kyles WB Rt. @ DAG264300.276003.264303.276071. 830.11.5 0. 32. 30.
 1
 26 Kyles WB Appr AG264359.275852.264296.275980. 30.11.5 0. 32. 30.
 2
 28 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
 100 58 2.0 30 73.3 1881 1 3

1
27 Kyles WB @ DixieAG264296.275980.264280.276013. 15.11.5 0. 32. 30.
1
28 Kyles WB Lt. AG264296.275980.264252.275994. 15.11.5 0. 32. 30.
1
29 Kyles WB Lt. AG264359.275852.264325.275892. 380.11.5 0. 32. 30.
1
30 Kyles WB Lt. AG264325.275892.264287.275965. 380.11.5 0. 32. 30.
2
33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
100 58 2.0 380 73.3 1357 1 3
1
31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 140.11.5 0. 32. 30.
1.0 04 1000. 0Y 5 0 72

Brent Spence Bridge S1alltam.dat 60.0175.0.0000.000240.30480000 1 1
R1 SB Mid 264384. 276323. 5.
R2 SB 164 264321. 276211. 5.
R3 SB 82 264290. 276136. 5.
R4 SB Corner 264262. 276069. 5.
R5 SB Corner 264230. 275990. 5.
R6 SB 82 264193. 275900. 5.
R7 SB 164 264151. 275798. 5.
R8 SB Mid 264103. 275678. 5.
R9 NB Mid 264155. 275655. 5.
R10 NB 164 264184. 275729. 5.
R11 NB 82 264215. 275805. 5.
R12 NB Corner 264242. 275872. 5.
R13 EB Corner 264272. 275903. 5.
R14 EB 82 264340. 275765. 5.
R15 EB 164 264378. 275678. 5.
R16 EB Mid 264408. 275600. 5.
R17 WB Mid 264455. 275722. 5.
R18 WB 164 264399. 275833. 5.
R19 WB 82 264362. 275906. 5.
R20 WB Corner 264330. 275971. 5.
R21 NB Corner 264319. 276046. 5.
R22 NB 82 264343. 276114. 5.
R23 NB 164 264376. 276189. 5.
R24 NB Mid 264447. 276280. 5.
Kyles Lane & Dixie Hwy 36 1 1
1
01 Dixie NB Appr AG264099.275553.264162.275726. 1520.11.5 0. 44. 30.
1
02 Dixie NB Appr AG264162.275726.264197.275813. 1520.11.5 0. 44. 30.
1
03 Dixie NB Appr AG264197.275813.264240.275916. 1520.11.5 0. 44. 30.
2
03 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
90 55 2.0 1520 73.3 1641 1 3
1
04 Dixie NB @ KylesAG264240.275916.264280.276013. 1240.11.5 0. 44. 30.
1
05 Dixie NB Depart AG264280.276013.264303.276071. 1245.11.5 0. 44. 30.
1
06 Dixie NB Depart AG264303.276071.264360.276209. 1955.11.5 0. 44. 30.
1
07 Dixie NB Depart AG264360.276209.264406.276278. 1955.11.5 0. 44. 30.
1
08 Dixie NB Depart AG264406.276278.264446.276325. 1955.11.5 0. 44. 30.
1
09 Dixie NB Depart AG264446.276325.264529.276400. 1955.11.5 0. 44. 30.
1
10 Dixie SB Appr AG264499.276415.264439.276361. 1020.11.5 0. 44. 30.
1
11 Dixie SB Appr AG264439.276361.264381.276288. 1020.11.5 0. 44. 30.
1
12 Dixie SB Appr AG264381.276288.264351.276234. 1020.11.5 0. 44. 30.
1
13 Dixie SB Appr AG264351.276234.264252.275994. 1020.11.5 0. 44. 30.
2
14 Dixie SB Queue AG264276.276054.264321.276161. 0. 24. 2
90 40 2.0 1020 73.3 1829 1 3
1
14 Dixie SB @ KylesAG264252.275994.264236.275956. 505.11.5 0. 40. 30.
1
15 Dixie SB Depart AG264236.275956.264179.275824. 665.11.5 0. 44. 30.
1
16 Dixie SB Depart AG264179.275824.264143.275732. 665.11.5 0. 44. 30.
1
17 Dixie SB Depart AG264143.275732.264083.275564. 665.11.5 0. 44. 30.
1
18 Dixie NB Rt. AG264240.275916.264284.275929. 280.11.5 0. 32. 30.
1
19 Kyles EB @ DixieAG264252.275994.264284.275929. 520.11.5 0. 32. 30.
1
20 Kyles EB Depart AG264284.275929.264483.275522. 800.11.5 0. 44. 30.
1
21 Kyles WB Appr AG264516.275540.264468.275639. 880.11.5 0. 56. 30.
1
22 Kyles WB Appr AG264468.275639.264359.275852. 880.11.5 0. 56. 30.
1
23 Kyles WB Rt. AG264359.275852.264347.275900. 710.11.5 0. 32. 30.
1
24 Kyles WB Rt. AG264347.275900.264300.276003. 710.11.5 0. 32. 30.
2
25 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
90 59 2.0 710 73.3 1599 1 3

1
 25 Kyles WB Rt. @ DAG264300.276003.264303.276071. 710.11.5 0. 32. 30.
 1
 26 Kyles WB Appr AG264359.275852.264296.275980. 10.11.5 0. 32. 30.
 2
 28 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
 90 59 2.0 10 73.3 1881 1 3
 1
 27 Kyles WB @ DixieAG264296.275980.264280.276013. 5.11.5 0. 32. 30.
 1
 28 Kyles WB Lt. AG264296.275980.264252.275994. 5.11.5 0. 32. 30.
 1
 29 Kyles WB Lt. AG264359.275852.264325.275892. 160.11.5 0. 32. 30.
 1
 30 Kyles WB Lt. AG264325.275892.264287.275965. 160.11.5 0. 32. 30.
 2
 33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
 90 59 2.0 160 73.3 1343 1 3
 1
 31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 160.11.5 0. 32. 30.
 1.0 04 1000. 0Y 5 0 72

Brent Spence Bridge S1altlpm.dat 60.0175.0.0000.000240.30480000 1 1
 R1 SB Mid 264384. 276323. 5.
 R2 SB 164 264321. 276211. 5.
 R3 SB 82 264290. 276136. 5.
 R4 SB Corner 264262. 276069. 5.
 R5 SB Corner 264230. 275990. 5.
 R6 SB 82 264193. 275900. 5.
 R7 SB 164 264151. 275798. 5.
 R8 SB Mid 264103. 275678. 5.
 R9 NB Mid 264155. 275655. 5.
 R10 NB 164 264184. 275729. 5.
 R11 NB 82 264215. 275805. 5.
 R12 NB Corner 264242. 275872. 5.
 R13 EB Corner 264272. 275903. 5.
 R14 EB 82 264340. 275765. 5.
 R15 EB 164 264378. 275678. 5.
 R16 EB Mid 264408. 275600. 5.
 R17 WB Mid 264455. 275722. 5.
 R18 WB 164 264399. 275833. 5.
 R19 WB 82 264362. 275906. 5.
 R20 WB Corner 264330. 275971. 5.
 R21 NB Corner 264319. 276046. 5.
 R22 NB 82 264343. 276114. 5.
 R23 NB 164 264376. 276189. 5.
 R24 NB Mid 264447. 276280. 5.
 Kyles Lane & Dixie Hwy 36 1 1

1
 01 Dixie NB Appr AG264099.275553.264162.275726. 760.11.5 0. 44. 30.
 1
 02 Dixie NB Appr AG264162.275726.264197.275813. 760.11.5 0. 44. 30.
 1
 03 Dixie NB Appr AG264197.275813.264240.275916. 760.11.5 0. 44. 30.
 2
 03 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
 100 75 2.0 760 73.3 1511 1 3
 1
 04 Dixie NB @ KylesAG264240.275916.264280.276013. 540.11.5 0. 44. 30.
 1
 05 Dixie NB Depart AG264280.276013.264303.276071. 465.11.5 0. 44. 30.
 1
 06 Dixie NB Depart AG264303.276071.264360.276209. 1295.11.5 0. 44. 30.
 1
 07 Dixie NB Depart AG264360.276209.264406.276278. 1295.11.5 0. 44. 30.
 1
 08 Dixie NB Depart AG264406.276278.264446.276325. 1295.11.5 0. 44. 30.
 1
 09 Dixie NB Depart AG264446.276325.264529.276400. 1295.11.5 0. 44. 30.
 1
 10 Dixie SB Appr AG264499.276415.264439.276361. 1600.11.5 0. 44. 30.
 1
 11 Dixie SB Appr AG264439.276361.264381.276288. 1600.11.5 0. 44. 30.
 1
 12 Dixie SB Appr AG264381.276288.264351.276234. 1600.11.5 0. 44. 30.
 1
 13 Dixie SB Appr AG264351.276234.264252.275994. 1600.11.5 0. 44. 30.
 2
 14 Dixie SB Queue AG264276.276054.264321.276161. 0. 24. 2
 100 50 2.0 1600 73.3 1831 1 3
 1
 14 Dixie SB @ KylesAG264252.275994.264236.275956. 965.11.5 0. 40. 30.
 1
 15 Dixie SB Depart AG264236.275956.264179.275824. 1345.11.5 0. 44. 30.
 1
 16 Dixie SB Depart AG264179.275824.264143.275732. 1345.11.5 0. 44. 30.
 1
 17 Dixie SB Depart AG264143.275732.264083.275564. 1345.11.5 0. 44. 30.
 1
 18 Dixie NB Rt. AG264240.275916.264284.275929. 310.11.5 0. 32. 30.
 1
 19 Kyles EB @ DixieAG264252.275994.264284.275929. 650.11.5 0. 32. 30.
 1
 20 Kyles EB Depart AG264284.275929.264483.275522. 960.11.5 0. 44. 30.
 1
 21 Kyles WB Appr AG264516.275540.264468.275639. 1240.11.5 0. 56. 30.
 1
 22 Kyles WB Appr AG264468.275639.264359.275852. 1240.11.5 0. 56. 30.

1
23 Kyles WB Rt. AG264359.275852.264347.275900. 830.11.5 0. 32. 30.
1
24 Kyles WB Rt. AG264347.275900.264300.276003. 830.11.5 0. 32. 30.
2
25 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
100 59 2.0 830 73.3 1599 1 3
1
25 Kyles WB Rt. @ DAG264300.276003.264303.276071. 830.11.5 0. 32. 30.
1
26 Kyles WB Appr AG264359.275852.264296.275980. 30.11.5 0. 32. 30.
2
28 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
100 59 2.0 30 73.3 1881 1 3
1
27 Kyles WB @ DixieAG264296.275980.264280.276013. 15.11.5 0. 32. 30.
1
28 Kyles WB Lt. AG264296.275980.264252.275994. 15.11.5 0. 32. 30.
1
29 Kyles WB Lt. AG264359.275852.264325.275892. 380.11.5 0. 32. 30.
1
30 Kyles WB Lt. AG264325.275892.264287.275965. 380.11.5 0. 32. 30.
2
33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
100 59 2.0 380 73.3 1357 1 3
1
31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 380.11.5 0. 32. 30.
1.0 04 1000. 0Y 5 0 72
Brent Spence Bridge NB-AM S1nbam.dat 60.0175.0.0000.000240.30480000 1 1
R1 SB Mid 264384. 276323. 5.
R2 SB 164 264321. 276211. 5.
R3 SB 82 264290. 276136. 5.
R4 SB Corner 264262. 276069. 5.
R5 SB Corner 264230. 275990. 5.
R6 SB 82 264193. 275900. 5.
R7 SB 164 264151. 275798. 5.
R8 SB Mid 264103. 275678. 5.
R9 NB Mid 264155. 275655. 5.
R10 NB 164 264184. 275729. 5.
R11 NB 82 264215. 275805. 5.
R12 NB Corner 264242. 275872. 5.
R13 EB Corner 264272. 275903. 5.
R14 EB 82 264340. 275765. 5.
R15 EB 164 264378. 275678. 5.
R16 EB Mid 264408. 275600. 5.
R17 WB Mid 264455. 275722. 5.
R18 WB 164 264399. 275833. 5.
R19 WB 82 264362. 275906. 5.
R20 WB Corner 264330. 275971. 5.
R21 NB Corner 264319. 276046. 5.
R22 NB 82 264343. 276114. 5.
R23 NB 164 264376. 276189. 5.
R24 NB Mid 264447. 276280. 5.
Kyles Lane & Dixie Hwy 36 1 1
1
01 Dixie NB Appr AG264099.275553.264162.275726. 1460.11.5 0. 44. 30.
1
02 Dixie NB Appr AG264162.275726.264197.275813. 1460.11.5 0. 44. 30.
1
03 Dixie NB Appr AG264197.275813.264240.275916. 1460.11.5 0. 44. 30.
2
03 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
120 74 2.0 1460 73.3 1642 1 3
1
04 Dixie NB @ KylesAG264240.275916.264280.276013. 1210.11.5 0. 44. 30.
1
05 Dixie NB Depart AG264280.276013.264303.276071. 1215.11.5 0. 44. 30.
1
06 Dixie NB Depart AG264303.276071.264360.276209. 1955.11.5 0. 44. 30.
1
07 Dixie NB Depart AG264360.276209.264406.276278. 1955.11.5 0. 44. 30.
1
08 Dixie NB Depart AG264406.276278.264446.276325. 1955.11.5 0. 44. 30.
1
09 Dixie NB Depart AG264446.276325.264529.276400. 1955.11.5 0. 44. 30.
1
10 Dixie SB Appr AG264499.276415.264439.276361. 1020.11.5 0. 44. 30.
1
11 Dixie SB Appr AG264439.276361.264381.276288. 1020.11.5 0. 44. 30.
1
12 Dixie SB Appr AG264381.276288.264351.276234. 1020.11.5 0. 44. 30.
1
13 Dixie SB Appr AG264351.276234.264252.275994. 1020.11.5 0. 44. 30.
2
14 Dixie SB Queue AG264276.276054.264321.276161. 0. 24. 2
120 55 2.0 1020 73.3 1829 1 3
1
14 Dixie SB @ KylesAG264252.275994.264236.275956. 485.11.5 0. 40. 30.
1
15 Dixie SB Depart AG264236.275956.264179.275824. 625.11.5 0. 44. 30.
1
16 Dixie SB Depart AG264179.275824.264143.275732. 625.11.5 0. 44. 30.
1
17 Dixie SB Depart AG264143.275732.264083.275564. 625.11.5 0. 44. 30.
1
18 Dixie NB Rt. AG264240.275916.264284.275929. 250.11.5 0. 32. 30.
1
19 Kyles EB @ DixieAG264252.275994.264284.275929. 540.11.5 0. 32. 30.

1
20 Kyles EB Depart AG264284.275929.264483.275522. 790.11.5 0. 44. 30.
1
21 Kyles WB Appr AG264516.275540.264468.275639. 890.11.5 0. 56. 30.
1
22 Kyles WB Appr AG264468.275639.264359.275852. 890.11.5 0. 56. 30.
1
23 Kyles WB Rt. AG264359.275852.264347.275900. 740.11.5 0. 32. 30.
1
24 Kyles WB Rt. AG264347.275900.264300.276003. 740.11.5 0. 32. 30.
2
25 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
120 78 2.0 740 73.3 1599 1 3
1
25 Kyles WB Rt. @ DAG264300.276003.264303.276071. 740.11.5 0. 32. 30.
1
26 Kyles WB Appr AG264359.275852.264296.275980. 10.11.5 0. 32. 30.
2
28 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
120 78 2.0 10 73.3 1881 1 3
1
27 Kyles WB @ DixieAG264296.275980.264280.276013. 5.11.5 0. 32. 30.
1
28 Kyles WB Lt. AG264296.275980.264252.275994. 5.11.5 0. 32. 30.
1
29 Kyles WB Lt. AG264359.275852.264325.275892. 140.11.5 0. 32. 30.
1
30 Kyles WB Lt. AG264325.275892.264287.275965. 140.11.5 0. 32. 30.
2
33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
120 78 2.0 140 73.3 1350 1 3
1
31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 140.11.5 0. 32. 30.
1.0 04 1000. 0Y 5 0 72

Brent Spence Bridge NB-PM S1nbpm.dat 60.0175.0.0000.000240.30480000 1 1
R1 SB Mid 264384. 276323. 5.
R2 SB 164 264321. 276211. 5.
R3 SB 82 264290. 276136. 5.
R4 SB Corner 264262. 276069. 5.
R5 SB Corner 264230. 275990. 5.
R6 SB 82 264193. 275900. 5.
R7 SB 164 264151. 275798. 5.
R8 SB Mid 264103. 275678. 5.
R9 NB Mid 264155. 275655. 5.
R10 NB 164 264184. 275729. 5.
R11 NB 82 264215. 275805. 5.
R12 NB Corner 264242. 275872. 5.
R13 EB Corner 264272. 275903. 5.
R14 EB 82 264340. 275765. 5.
R15 EB 164 264378. 275678. 5.
R16 EB Mid 264408. 275600. 5.
R17 WB Mid 264455. 275722. 5.
R18 WB 164 264399. 275833. 5.
R19 WB 82 264362. 275906. 5.
R20 WB Corner 264330. 275971. 5.
R21 NB Corner 264319. 276046. 5.
R22 NB 82 264343. 276114. 5.
R23 NB 164 264376. 276189. 5.
R24 NB Mid 264447. 276280. 5.
Kyles Lane & Dixie Hwy 36 1 1
1
01 Dixie NB Appr AG264099.275553.264162.275726. 720.11.5 0. 44. 30.
1
02 Dixie NB Appr AG264162.275726.264197.275813. 720.11.5 0. 44. 30.
1
03 Dixie NB Appr AG264197.275813.264240.275916. 720.11.5 0. 44. 30.
2
03 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
110 84 2.0 720 73.3 1505 1 3
1
04 Dixie NB @ KylesAG264240.275916.264280.276013. 430.11.5 0. 44. 30.
1
05 Dixie NB Depart AG264280.276013.264303.276071. 445.11.5 0. 44. 30.
1
06 Dixie NB Depart AG264303.276071.264360.276209. 1295.11.5 0. 44. 30.
1
07 Dixie NB Depart AG264360.276209.264406.276278. 1295.11.5 0. 44. 30.
1
08 Dixie NB Depart AG264406.276278.264446.276325. 1295.11.5 0. 44. 30.
1
09 Dixie NB Depart AG264446.276325.264529.276400. 1295.11.5 0. 44. 30.
1
10 Dixie SB Appr AG264499.276415.264439.276361. 1020.11.5 0. 44. 30.
1
11 Dixie SB Appr AG264439.276361.264381.276288. 1570.11.5 0. 44. 30.
1
12 Dixie SB Appr AG264381.276288.264351.276234. 1570.11.5 0. 44. 30.
1
13 Dixie SB Appr AG264351.276234.264252.275994. 1570.11.5 0. 44. 30.
2
14 Dixie SB Queue AG264276.276054.264321.276161. 0. 24. 2
110 52 2.0 1570 73.3 1831 1 3
1
14 Dixie SB @ KylesAG264252.275994.264236.275956. 915.11.5 0. 40. 30.
1
15 Dixie SB Depart AG264236.275956.264179.275824. 1265.11.5 0. 44. 30.
1

16 Dixie SB Depart AG264179.275824.264143.275732. 1265.11.5 0. 44. 30.
 1
 17 Dixie SB Depart AG264143.275732.264083.275564. 1265.11.5 0. 44. 30.
 1
 18 Dixie NB Rt. AG264240.275916.264284.275929. 290.11.5 0. 32. 30.
 1
 19 Kyles EB @ DixieAG264252.275994.264284.275929. 670.11.5 0. 32. 30.
 1
 20 Kyles EB Depart AG264284.275929.264483.275522. 960.11.5 0. 44. 30.
 1
 21 Kyles WB Appr AG264516.275540.264468.275639. 1230.11.5 0. 56. 30.
 1
 22 Kyles WB Appr AG264468.275639.264359.275852. 1230.11.5 0. 56. 30.
 1
 23 Kyles WB Rt. AG264359.275852.264347.275900. 850.11.5 0. 32. 30.
 1
 24 Kyles WB Rt. AG264347.275900.264300.276003. 850.11.5 0. 32. 30.
 2
 25 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
 110 63 2.0 850 73.3 1599 1 3
 1
 25 Kyles WB Rt. @ DAG264300.276003.264303.276071. 850.11.5 0. 32. 30.
 1
 26 Kyles WB Appr AG264359.275852.264296.275980. 30.11.5 0. 32. 30.
 2
 28 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
 110 63 2.0 30 73.3 1881 1 3
 1
 27 Kyles WB @ DixieAG264296.275980.264280.276013. 15.11.5 0. 32. 30.
 1
 28 Kyles WB Lt. AG264296.275980.264252.275994. 15.11.5 0. 32. 30.
 1
 29 Kyles WB Lt. AG264359.275852.264325.275892. 350.11.5 0. 32. 30.
 1
 30 Kyles WB Lt. AG264325.275892.264287.275965. 350.11.5 0. 32. 30.
 2
 33 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
 110 63 2.0 350 73.3 1370 1 3
 1
 31 Kyles WB Lt. @ DAG264287.275965.264236.275956. 350.11.5 0. 32. 30.
 1.0 04 1000. 0Y 5 0 72

Brent Spence Bridge 60.0175.0.0000.000480.30480000 1 1

R1 EB 82 269739. 284764. 5.
 R2 SW Corner 269811. 284765. 5.
 R3 SB 82 269812. 284693. 5.
 R4 SB 164 269813. 284611. 5.
 R5 NB 164 269868. 284612. 5.
 R6 NB 82 269867. 284694. 5.
 R7 SE Corner 269866. 284766. 5.
 R8 EB 82 269938. 284768. 5.
 R9 EB 164 270018. 284770. 5.
 R10 EB 82 270099. 284760. 5.
 R10 SW Corner 270171. 284761. 5.
 R12 SE Corner 270217. 284772. 5.
 R13 EB 82r 270289. 284773. 5.
 R14 EB 164 270368. 284774. 5.
 R15 EB 82 270447. 284775. 5.
 R16 SW Corner 270519. 284776. 5.
 R17 SB 82 270520. 284704. 5.
 R18 SB 164 270521. 284622. 5.
 R19 NB 164 270583. 284618. 5.
 R20 NB 82 270581. 284700. 5.
 R21 SE Corner 270580. 284773. 5.
 R22 SB 82 270652. 284773. 5.
 R23 WB 82 270652. 284829. 5.
 R24 NE Corner 270580. 284829. 5.
 R25 NB 82 270579. 284901. 5.
 R26 NB 164 270577. 284983. 5.
 R27 SB 164 270525. 284975. 5.
 R28 SB 82 270527. 284893. 5.
 R29 NW Corner 270518. 284821. 5.
 R30 WB 82 270446. 284821. 5.
 R31 WB 164 270368. 284820. 5.
 R32 WB 82 270288. 284819. 5.
 R33 NE Corner 270216. 284818. 5.
 R34 NB 82 270215. 284890. 5.
 R35 NB 164 270214. 284972. 5.
 R36 SB 164 270168. 284972. 5.
 R37 SB 82 270169. 284890. 5.
 R38 NW Corner 270170. 284818. 5.
 R39 WB 82 270098. 284817. 5.
 R40 WB 164 270017. 284815. 5.
 R41 WB 82 269937. 284814. 5.
 R42 NE Corner 269865. 284813. 5.
 R43 NB 82 269864. 284885. 5.
 R44 NB 164 269863. 284967. 5.
 R45 SB 164 269809. 284966. 5.
 R46 SB 82 269810. 284884. 5.
 R47 NW Corner 269811. 284812. 5.
 R48 WB 82 269738. 284810. 5.
 W 5th Street & Bakewell 26 1 1

1
 1 EB 5th Phil Appr AG269695.284787.269838.284789. 1280.11.5 0. 44. 30.
 2
 2 EB 5th EB Queue AG269805.284789.269726.284788. 0. 24. 2
 60 31 2.0 1280 73.3 1758 1 3
 1

3 EB 5th Bake Appr AG269838.284789.270093.284793. 1270.11.5 0. 44. 30.
1
4 EB 5th Bake LT AG270093.284793.270194.284795. 1250.11.5 0. 44. 30.
1
5 EB 5th EB Rt AG270093.284776.270189.284778. 20.11.5 0. 44. 30.
1
6 EB 5th Main Appr AG270194.284795.270550.284799. 1340.11.5 0. 44. 30.
2
7 EB 5th EB Queue AG270491.284798.270385.284797. 0. 24. 2
60 28 2.0 1340 73.3 1715 1 3
1
8 EB 5th Main Dep AG270550.284799.270695.284801. 1270.11.5 0. 44. 30.
1
9 NB Phil 5th Appr AG269851.284462.269847.284786. 460.11.5 0. 44. 30.
2
10 NB PhilNB Queue AG269848.284750.269849.284672. 0. 24. 2
60 36 2.0 460 73.3 1731 1 3
1
11 NB Phil5th Dep AG269847.284786.269841.285143. 670.11.5 0. 44. 30.
1
12 SB Phil5th Appr AG269823.285126.269830.284793. 130.11.5 0. 44. 30.
2
13 SB PhilSB Queue AG269829.284819.269828.284898. 0. 24. 2
60 36 2.0 130 73.3 1196 1 3
1
14 SB PhilPhil Dep AG269830.284793.269835.284461. 110.11.5 0. 44. 30.
1
15 NB Park5th Appr AG270203.284576.270200.284791. 30.11.5 0. 32. 30.
2
16 NB ParkNB Queue AG270201.284761.270202.284696. 0. 12. 1
40 20 2.0 30 73.3 800 1 3
1
17 NB Bake5th Dep AG270200.284791.270194.285216. 50.11.5 0. 32. 30.
1
18 SB Bake5th Appr AG270180.285216.270189.284778. 100.11.5 0. 32. 30.
2
19 SB BakeSB Queue AG270188.284828.270186.284943. 0. 12. 1
40 20 2.0 100 73.3 800 1 3
1
20 SB BakeBake Dep AG270189.284778.270192.284577. 70.11.5 0. 32. 30.
1
21 NB MainMain Appr AG270564.284513.270559.284795. 160.11.5 0. 32. 30.
2
22 NB MainNB Queue AG270560.284768.270561.284691. 0. 12. 1
60 38 2.0 160 73.3 1834 1 3
1
23 NB MainMain Dep AG270559.284795.270556.285029. 330.11.5 0. 32. 30.
1
24 SB MainMain Appr AG270535.285030.270539.284802. 250.11.5. 0. 44. 30.
2
25 SB MainSB Queue AG270538.284828.270537.284906. 0. 24. 2
60 38 2.0 250 73.3 1477 1 3
1
26 SB MainMain Dep AG270539.284802.270543.284513. 150.11.5 0. 44. 30.
1.0 04 1000. 0Y 5 0 72
Brent Spence Bridge 60.0175.0.0000.000480.30480000 1 1
R1 EB 82 269739. 284764. 5.
R2 SW Corner 269811. 284765. 5.
R3 SB 82 269812. 284693. 5.
R4 SB 164 269813. 284611. 5.
R5 NB 164 269868. 284612. 5.
R6 NB 82 269867. 284694. 5.
R7 SE Corner 269866. 284766. 5.
R8 EB 82 269938. 284768. 5.
R9 EB 164 270018. 284770. 5.
R10 EB 82 270099. 284760. 5.
R10 SW Corner 270171. 284761. 5.
R12 SE Corner 270217. 284772. 5.
R13 EB 82r 270289. 284773. 5.
R14 EB 164 270368. 284774. 5.
R15 EB 82 270447. 284775. 5.
R16 SW Corner 270519. 284776. 5.
R17 SB 82 270520. 284704. 5.
R18 SB 164 270521. 284622. 5.
R19 NB 164 270583. 284618. 5.
R20 NB 82 270581. 284700. 5.
R21 SE Corner 270580. 284773. 5.
R22 SB 82 270652. 284773. 5.
R23 WB 82 270652. 284829. 5.
R24 NE Corner 270580. 284829. 5.
R25 NB 82 270579. 284901. 5.
R26 NB 164 270577. 284983. 5.
R27 SB 164 270525. 284975. 5.
R28 SB 82 270527. 284893. 5.
R29 NW Corner 270518. 284821. 5.
R30 WB 82 270446. 284821. 5.
R31 WB 164 270368. 284820. 5.
R32 WB 82 270288. 284819. 5.
R33 NE Corner 270216. 284818. 5.
R34 NB 82 270215. 284890. 5.
R35 NB 164 270214. 284972. 5.
R36 SB 164 270168. 284972. 5.
R37 SB 82 270169. 284890. 5.
R38 NW Corner 270170. 284818. 5.
R39 WB 82 270098. 284817. 5.
R40 WB 164 270017. 284815. 5.
R41 WB 82 269937. 284814. 5.
R42 NE Corner 269865. 284813. 5.

R17 SB 82	270520.	284704.	5.
R18 SB 164	270521.	284622.	5.
R19 NB 164	270583.	284618.	5.
R20 NB 82	270581.	284700.	5.
R21 SE Corner	270580.	284773.	5.
R22 SB 82	270652.	284773.	5.
R23 WB 82	270652.	284829.	5.
R24 NE Corner	270580.	284829.	5.
R25 NB 82	270579.	284901.	5.
R26 NB 164	270577.	284983.	5.
R27 SB 164	270525.	284975.	5.
R28 SB 82	270527.	284893.	5.
R29 NW Corner	270518.	284821.	5.
R30 WB 82	270446.	284821.	5.
R31 WB 164	270368.	284820.	5.
R32 WB 82	270288.	284819.	5.
R33 NE Corner	270216.	284818.	5.
R34 NB 82	270215.	284890.	5.
R35 NB 164	270214.	284972.	5.
R36 SB 164	270168.	284972.	5.
R37 SB 82	270169.	284890.	5.
R38 NW Corner	270170.	284818.	5.
R39 WB 82	270098.	284817.	5.
R40 WB 164	270017.	284815.	5.
R41 WB 82	269937.	284814.	5.
R42 NE Corner	269865.	284813.	5.
R43 NB 82	269864.	284885.	5.
R44 NB 164	269863.	284967.	5.
R45 SB 164	269809.	284966.	5.
R46 SB 82	269810.	284884.	5.
R47 NW Corner	269811.	284812.	5.
R48 WB 82	269738.	284810.	5.
W 5th Street & Bakewell	26	1	1
1			
1 EB 5th Phil Appr	AG269695.284787.269838.284789.	77011.5	0. 44. 30.
2			
2 EB 5th EB Queue	AG269805.284789.269726.284788.	0. 24.	2
60	44	2.0 770	73.3 1743 1 3
1			
3 EB 5th Bake Appr	AG269838.284789.270093.284793.	720.11.5	0. 44. 30.
1			
4 EB 5th Bake LT	AG270093.284793.270194.284795.	710.11.5	0. 44. 30.
1			
5 EB 5th EB Rt	AG270093.284776.270189.284778.	10.11.5	0. 44. 30.
1			
6 EB 5th Main Appr	AG270194.284795.270550.284799.	960.11.5	0. 44. 30.
2			
7 EB 5th EB Queue	AG270491.284798.270385.284797.	0. 24.	2
60	31	2.0 960	73.3 1743 1 3
1			
8 EB 5th Main Dep	AG270550.284799.270695.284801.	720.11.5	0. 44. 30.
1			
9 NB Phil 5th Appr	AG269851.284462.269847.284786.	410.11.5	0. 44. 30.
2			
10 NB PhilNB Queue	AG269848.284750.269849.284672.	0. 24.	2
60	23	2.0 410	73.3 1731 1 3
1			
11 NB Phil5th Dep	AG269847.284786.269841.285143.	320.11.5	0. 44. 30.
1			
12 SB Phil5th Appr	AG269823.285126.269830.284793.	1390.11.5	0. 44. 30.
2			
13 SB PhilSB Queue	AG269829.284819.269828.284898.	0. 24.	2
60	23	2.0 1390	73.3 1600 1 3
1			
14 SB PhilPhil Dep	AG269830.284793.269835.284461.	1120.11.5	0. 44. 30.
1			
15 NB Park5th Appr	AG270203.284576.270200.284791.	70.11.5	0. 32. 30.
2			
16 NB ParkNB Queue	AG270201.284761.270202.284696.	0. 12.	1
40	20	2.0 70	73.3 800 1 3
1			
17 NB Bake5th Dep	AG270200.284791.270194.285216.	140.11.5	0. 32. 30.
1			
18 SB Bake5th Appr	AG270180.285216.270189.284778.	140.11.5	0. 32. 30.
2			
19 SB BakeSB Queue	AG270188.284828.270186.284943.	0. 12.	1
40	20	2.0 140	73.3 800 1 3
1			
20 SB BakeBake Dep	AG270189.284778.270192.284577.	70.11.5	0. 32. 30.
1			
21 NB MainMain Appr	AG270564.284513.270559.284795.	170.11.5	0. 32. 30.
2			
22 NB MainNB Queue	AG270560.284768.270561.284691.	0. 12.	1
60	36	2.0 170	73.3 1866 1 3
1			
23 NB MainMain Dep	AG270559.284795.270556.285029.	470.11.5	0. 44. 30.
1			
24 SB MainMain Appr	AG270535.285030.270539.284802.	180.11.5	0. 44. 30.
2			
25 SB MainSB Queue	AG270538.284828.270537.284906.	0. 24.	2
60	36	2.0 180	73.3 1483 1 3
1			
26 SB MainMain Dep	AG270539.284802.270543.284513.	120.11.5	0. 44. 30.
1.0	04 1000.	0Y 5 0 72	
Brent Spence Bridge	60.0175.0.0000.000480.30480000	1	1
R1 EB 82	269739.	284764.	5.
R2 SW Corner	269811.	284765.	5.
R3 SB 82	269812.	284693.	5.

R4 SB 164	269813.	284611.	5.
R5 NB 164	269868.	284612.	5.
R6 NB 82	269867.	284694.	5.
R7 SE Corner	269866.	284766.	5.
R8 EB 82	269938.	284768.	5.
R9 EB 164	270018.	284770.	5.
R10 EB 82	270099.	284760.	5.
R10 SW Corner	270171.	284761.	5.
R12 SE Corner	270217.	284772.	5.
R13 EB 82r	270289.	284773.	5.
R14 EB 164	270368.	284774.	5.
R15 EB 82	270447.	284775.	5.
R16 SW Corner	270519.	284776.	5.
R17 SB 82	270520.	284704.	5.
R18 SB 164	270521.	284622.	5.
R19 NB 164	270583.	284618.	5.
R20 NB 82	270581.	284700.	5.
R21 SE Corner	270580.	284773.	5.
R22 SB 82	270652.	284773.	5.
R23 WB 82	270652.	284829.	5.
R24 NE Corner	270580.	284829.	5.
R25 NB 82	270579.	284901.	5.
R26 NB 164	270577.	284983.	5.
R27 SB 164	270525.	284975.	5.
R28 SB 82	270527.	284893.	5.
R29 NW Corner	270518.	284821.	5.
R30 WB 82	270446.	284821.	5.
R31 WB 164	270368.	284820.	5.
R32 WB 82	270288.	284819.	5.
R33 NE Corner	270216.	284818.	5.
R34 NB 82	270215.	284890.	5.
R35 NB 164	270214.	284972.	5.
R36 SB 164	270168.	284972.	5.
R37 SB 82	270169.	284890.	5.
R38 NW Corner	270170.	284818.	5.
R39 WB 82	270098.	284817.	5.
R40 WB 164	270017.	284815.	5.
R41 WB 82	269937.	284814.	5.
R42 NE Corner	269865.	284813.	5.
R43 NB 82	269864.	284885.	5.
R44 NB 164	269863.	284967.	5.
R45 SB 164	269809.	284966.	5.
R46 SB 82	269810.	284884.	5.
R47 NW Corner	269811.	284812.	5.
R48 WB 82	269738.	284810.	5.
W 5th Street & Bakewell	26	1	1
1			
1 EB 5th Phil Appr	AG269695.284787.269838.284789.	1130.11.5	0. 44. 30.
2			
2 EB 5th EB Queue	AG269805.284789.269726.284788.	0. 24.	2
60	32	2.0 1130	73.3 1754 1 3
1			
3 EB 5th Bake Appr	AG269838.284789.270093.284793.	1180.11.5	0. 44. 30.
1			
4 EB 5th Bake LT	AG270093.284793.270194.284795.	1160.11.5	0. 44. 30.
1			
5 EB 5th EB Rt	AG270093.284776.270189.284778.	20.11.5	0. 44. 30.
1			
6 EB 5th Main Appr	AG270194.284795.270550.284799.	1430.11.5	0. 44. 30.
2			
7 EB 5th EB Queue	AG270491.284798.270385.284797.	0. 24.	2
60	24	2.0 1430	73.3 1706 1 3
1			
8 EB 5th Main Dep	AG270550.284799.270695.284801.	1180.11.5	0. 44. 30.
1			
9 NB Phil 5th Appr	AG269851.284462.269847.284786.	580.11.5	0. 44. 30.
2			
10 NB PhilNB Queue	AG269848.284750.269849.284672.	0. 24.	2
60	33	2.0 580	73.3 721 1 3
1			
11 NB Phil5th Dep	AG269847.284786.269841.285143.	850.11.5	0. 44. 30.
1			
12 SB Phil5th Appr	AG269823.285126.269830.284793.	170.11.5	0. 44. 30.
2			
13 SB PhilSB Queue	AG269829.284819.269828.284898.	0. 24.	2
60	33	2.0 170	73.3 1113 1 3
1			
14 SB PhilPhil Dep	AG269830.284793.269835.284461.	90.11.5	0. 44. 30.
1			
15 NB Park5th Appr	AG270203.284576.270200.284791.	30.11.5	0. 32. 30.
2			
16 NB ParkNB Queue	AG270201.284761.270202.284696.	0. 12.	1
40	20	2.0 30	73.3 800 1 3
1			
17 NB Bake5th Dep	AG270200.284791.270194.285216.	50.11.5	0. 32. 30.
1			
18 SB Bake5th Appr	AG270180.285216.270189.284778.	100.11.5	0. 32. 30.
2			
19 SB BakeSB Queue	AG270188.284828.270186.284943.	0. 12.	1
40	20	2.0 100	73.3 800 1 3
1			
20 SB BakeBake Dep	AG270189.284778.270192.284577.	70.11.5	0. 32. 30.
1			
21 NB MainMain Appr	AG270564.284513.270559.284795.	210.11.5	0. 32. 30.
2			
22 NB MainNB Queue	AG270560.284768.270561.284691.	0. 12.	1
60	40	2.0 210	73.3 1845 1 3
1			

23 NB MainMain Dep AG270559.284795.270556.285029. 490.11.5 0. 32. 30.
 1
 24 SB MainMain Appr AG270535.285030.270539.284802. 180.11.5 0. 44. 30.
 2
 25 SB MainSB Queue AG270538.284828.270537.284906. 0. 24. 2
 60 40 2.0 180 73.3 1373 1 3
 1
 26 SB MainMain Dep AG270539.284802.270543.284513. 150.11.5 0. 44. 30.
 1.0 04 1000. 0Y 5 0 72
 Brent Spence Bridge 60.0175.0.0000.000480.30480000 1 1
 R1 EB 82 269739. 284764. 5.
 R2 SW Corner 269811. 284765. 5.
 R3 SB 82 269812. 284693. 5.
 R4 SB 164 269813. 284611. 5.
 R5 NB 164 269868. 284612. 5.
 R6 NB 82 269867. 284694. 5.
 R7 SE Corner 269866. 284766. 5.
 R8 EB 82 269938. 284768. 5.
 R9 EB 164 270018. 284770. 5.
 R10 EB 82 270099. 284760. 5.
 R10 SW Corner 270171. 284761. 5.
 R12 SE Corner 270217. 284772. 5.
 R13 EB 82r 270289. 284773. 5.
 R14 EB 164 270368. 284774. 5.
 R15 EB 82 270447. 284775. 5.
 R16 SW Corner 270519. 284776. 5.
 R17 SB 82 270520. 284704. 5.
 R18 SB 164 270521. 284622. 5.
 R19 NB 164 270583. 284618. 5.
 R20 NB 82 270581. 284700. 5.
 R21 SE Corner 270580. 284773. 5.
 R22 SB 82 270652. 284773. 5.
 R23 WB 82 270652. 284829. 5.
 R24 NE Corner 270580. 284829. 5.
 R25 NB 82 270579. 284901. 5.
 R26 NB 164 270577. 284983. 5.
 R27 SB 164 270525. 284975. 5.
 R28 SB 82 270527. 284893. 5.
 R29 NW Corner 270518. 284821. 5.
 R30 WB 82 270446. 284821. 5.
 R31 WB 164 270368. 284820. 5.
 R32 WB 82 270288. 284819. 5.
 R33 NE Corner 270216. 284818. 5.
 R34 NB 82 270215. 284890. 5.
 R35 NB 164 270214. 284972. 5.
 R36 SB 164 270168. 284972. 5.
 R37 SB 82 270169. 284890. 5.
 R38 NW Corner 270170. 284818. 5.
 R39 WB 82 270098. 284817. 5.
 R40 WB 164 270017. 284815. 5.
 R41 WB 82 269937. 284814. 5.
 R42 NE Corner 269865. 284813. 5.
 R43 NB 82 269864. 284885. 5.
 R44 NB 164 269863. 284967. 5.
 R45 SB 164 269809. 284966. 5.
 R46 SB 82 269810. 284884. 5.
 R47 NW Corner 269811. 284812. 5.
 R48 WB 82 269738. 284810. 5.
 W 5th Street & Bakewell 26 1 1
 1
 1 EB 5th Phil Appr AG269695.284787.269838.284789. 890.11.5 0. 44. 30.
 2
 2 EB 5th EB Queue AG269805.284789.269726.284788. 0. 24. 2
 60 25 2.0 890 73.3 1750 1 3
 1
 3 EB 5th Bake Appr AG269838.284789.270093.284793. 850.11.5 0. 44. 30.
 1
 4 EB 5th Bake Appr AG270093.284793.270194.284795. 840.11.5 0. 44. 30.
 1
 5 EB 5th EB Rt AG270093.284776.270189.284778. 10.11.5 0. 44. 30.
 1
 6 EB 5th Main Appr AG270194.284795.270550.284799. 1080.11.5 0. 44. 30.
 2
 7 EB 5th EB Queue AG270491.284798.270385.284797. 0. 24. 2
 60 30 2.0 1080 73.3 1680 1 3
 1
 8 EB 5th Main Dep AG270550.284799.270695.284801. 850.11.5 0. 44. 30.
 1
 9 NB Phil 5th Appr AG269851.284462.269847.284786. 310.11.5 0. 44. 30.
 2
 10 NB PhilNB Queue AG269848.284750.269849.284672. 0. 24. 2
 60 30 2.0 310 73.3 1731 1 3
 1
 11 NB Phil5th Dep AG269847.284786.269841.285143. 400.11.5 0. 44. 30.
 1
 12 SB Phil5th Appr AG269823.285126.269830.284793. 850.11.5 0. 44. 30.
 2
 13 SB PhilSB Queue AG269829.284819.269828.284898. 0. 24. 2
 60 30 2.0 850 73.3 1441 1 3
 1
 14 SB PhilPhil Dep AG269830.284793.269835.284461. 580.11.5 0. 44. 30.
 1
 15 NB Park5th Appr AG270203.284576.270200.284791. 70.11.5 0. 32. 30.
 2
 16 NB ParkNB Queue AG270201.284761.270202.284696. 0. 12. 1
 40 20 2.0 70 73.3 800 1 3
 1
 17 NB Bake5th Dep AG270200.284791.270194.285216. 70.11.5 0. 32. 30.

1
18 SB Bake5th Appr AG270180.285216.270189.284778. 80.11.5 0. 32. 30.
2
19 SB BakeSB Queue AG270188.284828.270186.284943. 0. 12. 1
40 20 2.0 80 73.3 800 1 3
1
20 SB BakeBake Dep AG270189.284778.270192.284577. 40.11.5 0. 32. 30.
1
21 NB MainMain Appr AG270564.284513.270559.284795. 210.11.5 0. 32. 30.
2
22 NB MainNB Queue AG270560.284768.270561.284691. 0. 12. 1
60 36 2.0 210 73.3 1869 1 3
1
23 NB MainMain Dep AG270559.284795.270556.285029. 540.11.5 0. 32. 30.
1
24 SB MainMain Appr AG270535.285030.270539.284802. 250.11.5 0. 44. 30.
2
25 SB MainSB Queue AG270538.284828.270537.284906. 0. 24. 2
100 36 2.0 250 73.3 1424 1 3
1
26 SB MainMain Dep AG270539.284802.270543.284513. 150.11.5 0. 44. 30.
1.0 04 1000. 0Y 5 0 72
Brent Spence Bridge 60.0175.0.0000.000220.30480000 1
R1 SE Mid 270140. 289517. 5.
R2 SE 164 270124. 289585. 5.
R3 SE 82 270105. 289664. 5.
R4 SE Corner 270088. 289735. 5.
R5 SE 82 270158. 289749. 5.
R6 SE 164 270239. 289766. 5.
R7 SE Mid 270274. 289773. 5.
R8 NE Mid 270256. 289830. 5.
R9 NE 164 270223. 289823. 5.
R10 NE 82 270142. 289806. 5.
R11 NE Corner 270072. 289791. 5.
R12 NE 82 270057. 289862. 5.
R13 NE 164 270040. 289942. 5.
R14 NE Mid 270034. 289968. 5.
R15 NW 164 269944. 290010. 5.
R16 NW 82 269961. 289930. 5.
R17 NW Corner 269976. 289859. 5.
R18 SW Corner 270010. 289716. 5.
R19 SW 82 270028. 289646. 5.
R20 SW 164 270046. 289566. 5.
R21 SW Mid 270055. 289525. 5.
R22 Near CD 269775. 289723. 5.
W 4th & Central Alt E AM 50 1 1
1
1 NB Cent McF Appr AG270186.289164.270108.289529. 310.12.6 0. 44. 30.
1
2 NB Thr W 4th ApprAG270117.289531.270060.289759. 240.12.6 0. 44. 30.
2
3 NB Cent NB Queue AG270067.289730.270089.289644. 0. 24. 2
60 35 2.0 240 73.3 1522 1 3
1
4 NB Cen W 4th DeprAG270060.289759.270043.289808. 500.12.6 0. 44. 30.
1
5 NB Cen W 4th DeptAG270043.289808.269933.290337. 500.12.6 0. 44. 30.
1
6 NB Lt W 4th ApprAG270099.289527.270042.289755. 70.12.6 0. 44. 30.
2
7 NB LefttNB Queue AG270049.289728.270070.289641. 0. 24. 2
60 55 2.0 70 73.3 1474 1 3
1
10 SB CentSB Appr AG269902.290330.270023.289751. 220.12.6 0. 44. 30.
2
11 SB CentSB Queue AG270007.289828.269982.289947. 0. 24. 2
60 40 2.0 220 73.3 1501 1 3
1
12 SB CentSB Dep AG270023.289751.270080.289522. 230.12.6 0. 44. 30.
1
13 SB CentSB Dep AG270080.289522.270159.289159. 230.12.6 0. 44. 30.
1
14 WB W 4tTo Plum AG270636.289880.270490.289851. 560.12.6 0. 44. 30.
1
15 WB W 4tFr Plum AG270490.289851.270352.289819. 560.12.6 0. 44. 30.
1
16 WB W 4tTo Cent AG270352.289819.270042.289755. 560.12.6 0. 56. 30.
2
17 WB W 4tWB Queue AG270089.289764.270191.289786. 0. 36. 3
60 38 2.0 560 73.3 1504 1 3
1
16 WB W 4tFrom Cent AG270040.289746.269741.289687. 360.12.6 0. 56. 30.
1
16 WB W 4tTo CD AG269740.289694.269544.289656. 250.12.6 0. 44. 30.
2
18 WB W 4tRt Queue AG269564.289660.269670.289680. 0. 24. 2
60 34 2.0 250 73.3 1349 1 3
1
19 WB W 4tRt to CD AG269544.289656.269495.289688. 250.12.6 0. 44. 30.
1
20 WB W 4tLt to CD AG269743.289676.269548.289635. 110.12.6 0. 32. 30.
2
21 WB W 4tLt Queue AG269568.289639.269672.289661. 0. 12. 1
60 33 2.0 110 73.3 1550 1 3
1
22 WB W 4tLt to CD AG269548.289635.269512.289576. 110.12.6 0. 32. 30.
1
23 NB CD To W 4th AG269358.289340.269495.289688. 1070.12.6 0. 44. 30.

2
 24 NB CD NB Queue AG269451.289575.269397.289438. 0. 24. 2
 60 33 2.0 1070 73.3 1707 1 3
 1
 25 NB CD Fr W 4th AG269495.289688.269471.289839. 1320.12.6 0. 56. 30.
 1
 26 NB CD Fr W 4th AG269471.289839.269432.290034. 1320.12.6 0. 68. 30.
 1
 27 SB CD To W 4th AG269353.290020.269416.289697. 1470.12.6 0. 56. 30.
 2
 27 SB CD SB Queue AG269408.289737.269373.289916. 0. 36. 3
 60 34 2.0 1470 73.3 1628 1 3
 1
 28 SB CD @ W 4th AG269416.289697.269512.289576. 1470.12.6 0. 56. 30.
 1
 29 SB CD @ W 4th AG269512.289576.269537.289433. 1580.12.6 0. 56. 30.
 1
 30 WB Off 3rd-SB 75 BR270480.289330.270388.289332. 280.12.1 0. 32. 30.
 1
 31 WB Off 3rd-SB 75 BR270388.289332.270294.289352. 280.12.1 0. 32. 30.
 1
 32 WB Off 3rd-SB 75 BR270294.289352.270197.289396. 280.12.1 0. 32. 30.
 1
 33 WB Off 3rd-SB 75 BR270197.289396.270134.289442. 280.12.1 0. 32. 30.
 1
 34 WB Off 3rd-SB 75 BR270134.289442.269989.289567. 280.12.1 0. 32. 30.
 1
 35 WB Off 3rd-SB 75 BR269989.289567.269874.289640. 280.12.1 0. 32. 30.
 1
 36 WB Off 3rd-SB 75 AG269874.289640.269770.289675. 280.12.1 0. 32. 30.
 1
 37 WB Off 71-SB 75 BR270428.289285.270297.289305. 2500.12.1 0. 44. 30.
 1
 38 WB Off 71-SB 75 BR270297.289305.270202.289342. 2500.12.1 0. 44. 30.
 1
 39 WB Off 71-SB 75 BR270202.289342.270133.289389. 2500.12.1 0. 44. 30.
 1
 40 WB Off 71-SB 75 BR270133.289389.270002.289505. 2500.12.1 0. 44. 30.
 1
 41 WB Off 71-SB 75 BR270002.289505.269880.289607. 2500.12.1 0. 44. 30.
 1
 42 WB Off 71-SB 75 BR269880.289607.269770.289675. 2500.12.1 0. 44. 30.
 1
 43 WB Off 71-SB 75 BR269770.289675.269688.289703. 2780.12.1 0. 56. 30.
 1
 44 WB Off 71-SB 75 BR269688.289703.269608.289715. 2780.12.1 0. 56. 30.
 1
 45 WB Off 71-SB 75 BR269608.289715.269523.289714. 2780.12.1 0. 56. 30.
 1
 46 WB Off 71-SB 75 BR269523.289714.269442.289700. 2780.12.1 0. 56. 30.
 1
 47 WB Off 71-SB 75 BR269442.289700.269379.289680. 2780.12.1 0. 56. 30.
 1
 48 WB Off 71-SB 75 BR269379.289680.269317.289651. 2780.12.1 0. 56. 30.
 1
 49 WB Off 71-SB 75 BR269317.289651.269246.289603. 2780.12.1 0. 56. 30.
 1.0 04 1000. 0Y 5 0 72
 Brent Spence Bridge 60.0175.0.0000.000220.30480000 1
 R1 SE Mid 270140. 289517. 5.
 R2 SE 164 270124. 289585. 5.
 R3 SE 82 270105. 289664. 5.
 R4 SE Corner 270088. 289735. 5.
 R5 SE 82 270158. 289749. 5.
 R6 SE 164 270239. 289766. 5.
 R7 SE Mid 270274. 289773. 5.
 R8 NE Mid 270256. 289830. 5.
 R9 NE 164 270223. 289823. 5.
 R10 NE 82 270142. 289806. 5.
 R11 NE Corner 270072. 289791. 5.
 R12 NE 82 270057. 289862. 5.
 R13 NE 164 270040. 289942. 5.
 R14 NE Mid 270034. 289968. 5.
 R15 NW 164 269944. 290010. 5.
 R16 NW 82 269961. 289930. 5.
 R17 NW Corner 269976. 289859. 5.
 R18 SW Corner 270010. 289716. 5.
 R19 SW 82 270028. 289646. 5.
 R20 SW 164 270046. 289566. 5.
 R21 SW Mid 270055. 289525. 5.
 R22 Near CD 269775. 289723. 5.
 W 4th & Central Alt E PM 50 1 1
 1
 1 NB Cent McF Appr AG270186.289164.270108.289529. 1310.12.6 0. 44. 30.
 1
 2 NB Thr W 4th ApprAG270117.289531.270060.289759. 540.12.6 0. 44. 30.
 2
 3 NB Cent NB Queue AG270067.289730.270089.289644. 0. 24. 2
 120 65 2.0 540 73.3 1522 1 3
 1
 4 NB Cen W 4th DeprAG270060.289759.270043.289808. 950.12.6 0. 44. 30.
 1
 5 NB Cen W 4th DeptAG270043.289808.269933.290337. 950.12.6 0. 44. 30.
 1
 6 NB Lt W 4th ApprAG270099.289527.270042.289755. 770.12.6 0. 44. 30.
 2
 7 NB LefttNB Queue AG270049.289728.270070.289641. 0. 24. 2
 120 85 2.0 770 73.3 1474 1 3
 1

10 SB CentSB Appr AG269902.290330.270023.289751. 280.12.6 0. 44. 30.
2
11 SB CentSB Queue AG270007.289828.269982.289947. 0. 24. 2
120 103 2.0 280 73.3 1376 1 3
1
12 SB CentSB Dep AG270023.289751.270080.289522. 220.12.6 0. 44. 30.
1
13 SB CentSB Dep AG270080.289522.270159.289159. 220.12.6 0. 44. 30.
1
14 WB W 4tTo Plum AG270636.289880.270490.289851. 1660.12.6 0. 44. 30.
1
15 WB W 4tFr Plum AG270490.289851.270352.289819. 1660.12.6 0. 44. 30.
1
16 WB W 4tTo Cent AG270352.289819.270042.289755. 1660.12.6 0. 56. 30.
2
17 WB W 4tWB Queue AG270089.289764.270191.289786. 0. 36. 3
120 67 2.0 1660 73.3 1534 1 3
1
16 WB W 4tFrom Cent AG270040.289746.269741.289687. 2080.12.6 0. 56. 30.
1
16 WB W 4tTo CD AG269740.289694.269544.289656. 1790.12.6 0. 44. 30.
2
18 WB W 4tRt Queue AG269564.289660.269670.289680. 0. 24. 2
120 38 2.0 1790 73.3 1349 1 3
1
19 WB W 4tRt to CD AG269544.289656.269495.289688. 1790.12.6 0. 44. 30.
1
20 WB W 4tLt to CD AG269743.289676.269548.289635. 290.12.6 0. 32. 30.
2
21 WB W 4tLt Queue AG269568.289639.269672.289661. 0. 12. 1
120 89 2.0 290 73.3 1550 1 3
1
22 WB W 4tLt to CD AG269548.289635.269512.289576. 290.12.6 0. 32. 30.
1
23 NB CD To W 4th AG269358.289340.269495.289688. 740.12.6 0. 44. 30.
2
24 NB CD NB Queue AG269451.289575.269397.289438. 0. 24. 2
120 89 2.0 740 73.3 1707 1 3
1
25 NB CD Fr W 4th AG269495.289688.269471.289839. 2540.12.6 0. 56. 30.
1
26 NB CD Fr W 4th AG269471.289839.269432.290034. 2540.12.6 0. 68. 30.
1
27 SB CD To W 4th AG269353.290020.269416.289697. 1720.12.6 0. 56. 30.
2
27 SB CD SB Queue AG269408.289737.269373.289916. 0. 36. 3
120 38 2.0 1720 73.3 1628 1 3
1
28 SB CD @ W 4th AG269416.289697.269512.289576. 1720.12.6 0. 56. 30.
1
29 SB CD @ W 4th AG269512.289576.269537.289433. 2010.12.6 0. 56. 30.
1
30 WB Off 3rd-SB 75 BR270480.289330.270388.289332. 1450.12.6 0. 32. 30.
1
31 WB Off 3rd-SB 75 BR270388.289332.270294.289352. 1450.12.6 0. 32. 30.
1
32 WB Off 3rd-SB 75 BR270294.289352.270197.289396. 1450.12.6 0. 32. 30.
1
33 WB Off 3rd-SB 75 BR270197.289396.270134.289442. 1450.12.6 0. 32. 30.
1
34 WB Off 3rd-SB 75 BR270134.289442.269989.289567. 1450.12.6 0. 32. 30.
11
35 WB Off 3rd-SB 75 BR269989.289567.269874.289640. 1450.12.6 0. 32. 30.
1
36 WB Off 3rd-SB 75 AG269874.289640.269770.289675. 1450.12.6 0. 32. 30.
1
37 WB Off 71-SB 75 BR270428.289285.270297.289305. 3490.12.6 0. 44. 30.
1
38 WB Off 71-SB 75 BR270297.289305.270202.289342. 3490.12.6 0. 44. 30.
1
39 WB Off 71-SB 75 BR270202.289342.270133.289389. 3490.12.6 0. 44. 30.
1
40 WB Off 71-SB 75 BR270133.289389.270002.289505. 3490.12.6 0. 44. 30.
1
41 WB Off 71-SB 75 BR270002.289505.269880.289607. 3490.12.6 0. 44. 30.
1
42 WB Off 71-SB 75 BR269880.289607.269770.289675. 3490.12.6 0. 44. 30.
1
43 WB Off 71-SB 75 BR269770.289675.269688.289703. 4940.12.6 0. 56. 30.
1
44 WB Off 71-SB 75 BR269688.289703.269608.289715. 4940.12.6 0. 56. 30.
1
45 WB Off 71-SB 75 BR269608.289715.269523.289714. 4940.12.6 0. 56. 30.
1
46 WB Off 71-SB 75 BR269523.289714.269442.289700. 4940.12.6 0. 56. 30.
1
47 WB Off 71-SB 75 BR269442.289700.269379.289680. 4910.12.6 0. 56. 30.
1
48 WB Off 71-SB 75 BR269379.289680.269317.289651. 4940.12.6 0. 56. 30.
1
49 WB Off 71-SB 75 BR269317.289651.269246.289603. 4940.12.6 0. 56. 30.
1.0 04 1000. OY 5 0 72
Brent Spence Bridge 60.0175.0.0000.000210.30480000 1 1
R1 SE Mid 270140. 289517. 5.
R2 SE 164 270124. 289585. 5.
R3 SE 82 270105. 289664. 5.
R4 SE Corner 270088. 289735. 5.
R5 SE 82 270158. 289749. 5.

R18 SW Corner 270010. 289716. 5.
R19 SW 82 270028. 289646. 5.
R20 SW 164 270046. 289566. 5.
R21 SW Mid 270055. 289525. 5.
W 4th & Central Alt I PM 29 1 1
1
1 NB Cent McF Appr AG270186.289164.270108.289529. 810.12.6 0. 44. 30.
1
2 NB Thr W 4th ApprAG270117.289531.270060.289759. 480.12.6 0. 44. 30.
2
3 NB Cent NB Queue AG270067.289730.270089.289644. 0. 24. 2
70 45 2.0 480 73.3 1522 1 3
1
4 NB Cen W 4th DeprAG270060.289759.270043.289808. 620.12.6 0. 44. 30.
1
5 NB Cen W 4th DeptAG270043.289808.269933.290337. 620.12.6 0. 44. 30.
1
6 NB Lt W 4th ApprAG270099.289527.270042.289755. 330.12.6 0. 44. 30.
2
7 NB LefttNB Queue AG270049.289728.270070.289641. 0. 24. 2
70 58 2.0 330 73.3 1474 1 3
1
8 NB Ramp From W 4thAG270042.289755.269974.289811. 1430.12.6 0. 44. 30.
1
9 NB Ramp From W 4thAG269974.289811.269755.290270. 1430.12.6 0. 44. 30.
1
10 SB CentSB Appr AG269902.290330.270023.289751. 180.12.6 0. 44. 30.
2
11 SB CentSB Queue AG270007.289828.269982.289947. 0. 24. 2
70 56 2.0 180 73.3 1420 1 3
1
12 SB CentSB Dep AG270023.289751.270080.289522. 180.12.6 0. 44. 30.
1
13 SB CentSB Dep AG270080.289522.270159.289159. 180.12.6 0. 44. 30.
1
14 WB W 4tTo Plum AG270636.289880.270490.289851. 1320.12.6 0. 44. 30.
1
15 WB W 4tFr Plum AG270490.289851.270352.289819. 1320.12.6 0. 44. 30.
1
16 WB W 4tTo Cent AG270352.289819.270042.289755. 1320.12.6 0. 56. 30.
2
17 WB W 4tWB Queue AG270089.289764.270191.289786. 0. 36. 3
70 37 2.0 1320 73.3 1535 1 3
1
18 WB Off 3rd-SB 75 BR270473.289330.270387.289337. 1450.12.1 0. 32. 30.
1
19 WB Off 3rd-SB 75 BR270387.289337.270291.289353. 1450.12.1 0. 32. 30.
1
20 WB Off 3rd-SB 75 BR270291.289353.270209.289396. 1450.12.1 0. 32. 30.
1
21 WB Off 3rd-SB 75 BR270209.289396.269996.289555. 1450.12.1 0. 28. 30.
1
22 WB Off 3rd-SB 75 BR269996.289555.269861.289614. 1450.12.1 0. 32. 30.
1
23 WB Off 71- SB 75 BR270427.289288.270271.289320. 320.12.1 0. 44. 30.
1
24 WB Off 71- SB 75 BR270271.289320.270153.289385. 320.12.1 0. 44. 30.
1
25 WB Off 71- SB 75 BR270153.289385.269986.289528. 320.12.1 0. 44. 30.
1
26 WB Off 71- SB 75 BR269986.289528.269861.289614. 320.12.1 0. 44. 30.
1
27 WB Off 71- SB 75 BR269861.289614.269702.289652. 1770.12.1 0. 44. 30.
1
28 WB Off 71- SB 75 BR269702.289652.269576.289645. 1770.12.1 0. 44. 30.
1
29 WB Off 71- SB 75 BR269576.289645.269470.289614. 1770.12.1 0. 44. 30.
1.0 04 1000. 0Y 5 0 72
Brent Spence Bridge 60.0175.0.0000.000220.30480000 1 1
R1 SE Mid 270140. 289517. 5.
R2 SE 164 270124. 289585. 5.
R3 SE 82 270105. 289664. 5.
R4 SE Corner 270088. 289735. 5.
R5 SE 82 270158. 289749. 5.
R6 SE 164 270239. 289766. 5.
R7 SE Mid 270274. 289773. 5.
R8 NE Mid 270256. 289830. 5.
R9 NE 164 270223. 289823. 5.
R10 NE 82 270142. 289806. 5.
R11 NE Corner 270072. 289791. 5.
R12 NE 82 270057. 289862. 5.
R13 NE 164 270040. 289942. 5.
R14 NE Mid 270034. 289968. 5.
R15 NW 164 269944. 290010. 5.
R16 NW 82 269961. 289930. 5.
R17 NW Corner 269976. 289859. 5.
R18 SW Corner 270010. 289716. 5.
R19 SW 82 270028. 289646. 5.
R20 SW 164 270046. 289566. 5.
R21 SW Mid 270055. 289525. 5.
R22 Near CD 269775. 289723. 5.
W 4th & Central No Bld AM 43 1 1
1
1 NB Cent McF Appr AG270186.289164.270108.289529. 370.12.6 0. 44. 30.
1
2 NB Thr W 4th ApprAG270117.289531.270060.289759. 270.12.6 0. 44. 30.
2
3 NB Cent NB Queue AG270067.289730.270089.289644. 0. 24. 2

60 33 2.0 270 73.3 1522 1 3
 1
 4 NB Cen W 4th DeprAG270060.289759.270043.289808. 340.12.6 0. 44. 30.
 1
 5 NB Cen W 4th DeptAG270043.289808.269933.290337. 340.12.6 0. 44. 30.
 1
 6 NB Lt W 4th ApprAG270099.289527.270042.289755. 100.12.6 0. 44. 30.
 2
 7 NB LefttNB Queue AG270049.289728.270070.289641. 0. 24. 2
 60 54 2.0 100 73.3 1474 1 3
 1
 8 NB Ramp From W 4thAG270042.289755.269974.289811. 290.12.6 0. 44. 30.
 1
 9 NB Ramp From W 4thAG269974.289811.269755.290270. 290.12.6 0. 44. 30.
 1
 10 SB CentSB Appr AG269902.290330.270023.289751. 130.12.6 0. 44. 30.
 2
 11 SB CentSB Queue AG27007.289828.269982.289947. 0. 24. 2
 60 40 2.0 130 73.3 1522 1 3
 1
 12 SB CentSB Dep AG270023.289751.270080.289522. 280.12.6 0. 44. 30.
 1
 13 SB CentSB Dep AG270080.289522.270159.289159. 280.12.6 0. 44. 30.
 1
 14 WB W 4tTo Plum AG270636.289880.270490.289851. 410.12.6 0. 44. 30.
 1
 15 WB W 4tFr Plum AG270490.289851.270352.289819. 410.12.6 0. 44. 30.
 1
 16 WB W 4tTo Cent AG270352.289819.270042.289755. 410.12.6 0. 56. 30.
 2
 17 WB W 4tWB Queue AG270089.289764.270191.289786. 0. 36. 3
 60 39 2.0 410 73.3 1487 1 3
 1
 18 WB Off 3rd-SB 75 BR270473.289330.270387.289337. 260.12.1 0. 32. 30.
 1
 19 WB Off 3rd-SB 75 BR270387.289337.270291.289353. 260.12.1 0. 32. 30.
 1
 20 WB Off 3rd-SB 75 BR270291.289353.270209.289396. 260.12.1 0. 32. 30.
 1
 21 WB Off 3rd-SB 75 BR270209.289396.269996.289555. 260.12.1 0. 28. 30.
 1
 22 WB Off 3rd-SB 75 BR269996.289555.269861.289614. 260.12.1 0. 32. 30.
 1
 23 WB Off 71- SB 75 BR270427.289288.270271.289320. 2420.12.1 0. 44. 30.
 1
 24 WB Off 71- SB 75 BR270271.289320.270153.289385. 2420.12.1 0. 44. 30.
 1
 25 WB Off 71- SB 75 BR270153.289385.269986.289528. 2420.12.1 0. 44. 30.
 1
 26 WB Off 71- SB 75 BR269986.289528.269861.289614. 2420.12.1 0. 44. 30.
 1
 27 WB Off 71- SB 75 BR269861.289614.269702.289652. 2680.12.1 0. 44. 30.
 1
 28 WB Off 71- SB 75 BR269702.289652.269576.289645. 2680.12.1 0. 44. 30.
 1
 29 WB Off 71- SB 75 BR269576.289645.269470.289614. 2680.12.1 0. 44. 30.
 1
 30 WB Off WB 71- 6thBR270360.289236.270239.289258. 2850.12.1 0. 44. 30.
 1
 31 WB Off WB 71- 6thBR270239.289258.270109.289317. 2850.12.1 0. 44. 30.
 1
 32 WB Off WB 71- 6thBR270109.289317.270024.289390. 2850.12.1 0. 44. 30.
 1
 33 WB Off WB 71- 6thBR270024.289390.269967.289470. 2850.12.1 0. 44. 30.
 1
 34 WB Off WB 71- 6thBR269967.289470.269923.289566. 2850.12.1 0. 44. 30.
 1
 35 WB Off WB 71- 6thBR269923.289566.269895.289698. 2850.12.1 0. 44. 30.
 1
 36 WB Off WB 71- 75 AG269895.289698.269888.289755. 1910.12.1 0. 32. 30.
 1
 37 WB Off WB 71- 75 AG269888.289755.269844.289970. 1910.12.1 0. 32. 30.
 1
 38 WB Off WB 71- 75 AG269844.289970.269818.290061. 1910.12.1 0. 32. 30.
 1
 39 WB Off WB 71- 75 AG269818.290061.269729.290257. 1910.12.1 0. 32. 30.
 1
 40 WB Off WB 71-6th AG269895.289698.269874.289754. 940.12.1 0. 32. 30.
 1
 41 WB Off WB 71-6th AG269874.289754.269831.289896. 940.12.1 0. 32. 30.
 1
 42 WB Off WB 71-6th AG269831.289896.269791.289993. 940.12.1 0. 32. 30.
 1
 43 WB Off WB 71-6th AG269791.289993.269680.290221. 940.12.1 0. 32. 30.
 1.0 04 1000. 0Y 5 0 72
 Brent Spence Bridge 60.0175.0.0000.000220.30480000 1 1
 R1 SE Mid 270140. 289517. 5.
 R2 SE 164 270124. 289585. 5.
 R3 SE 82 270105. 289664. 5.
 R4 SE Corner 270088. 289735. 5.
 R5 SE 82 270158. 289749. 5.
 R6 SE 164 270239. 289766. 5.
 R7 SE Mid 270274. 289773. 5.
 R8 NE Mid 270256. 289830. 5.
 R9 NE 164 270223. 289823. 5.
 R10 NE 82 270142. 289806. 5.
 R11 NE Corner 270072. 289791. 5.
 R12 NE 82 270057. 289862. 5.

42 WB Off WB 71-6th AG269831.289896.269791.289993. 1450.12.1 0. 32. 30.
 1
 43 WB Off WB 71-6th AG269791.289993.269680.290221. 1450.12.1 0. 32. 30.
 1.0 04 1000. OY 5 0 72
 Central & McMillan Alt E AM 60.0321.0.0000.000210.30480000 1 1
 SE MID S 266089. 298420. 5.0
 SE 164 S 266017. 298537. 5.0
 SE 82 S 265980. 298608. 5.0
 SE CNR 265952. 298689. 5.0
 SE 82 E 266009. 298754. 5.0
 SE 164 E 266067. 298814. 5.0
 SE MID E 266130. 298970. 5.0
 SE 164 S 266081. 299220. 5.0
 SE 82 S 266044. 299294. 5.0
 SE CNR 266014. 299370. 5.0
 SE 82 E 266072. 299443. 5.0
 SE 164 E 266129. 299503. 5.0
 SE MID E 266236. 299603. 5.0
 NE MID E 266197. 299656. 5.0
 NE 164 E 266064. 299530. 5.0
 NE 82 E 266006. 299471. 5.0
 NE CNR 265950. 299412. 5.0
 NE CNR 265869. 299339. 5.0
 NE 82 N 265872. 299412. 5.0
 NE 164 N 265876. 299494. 5.0
 NE MID N 265881. 299614. 5.0
 Central & McMillan Alt E AM 66 1 0
 1
 EB McM BR264826.298986.265320.298926. 239012.1 15 56 30.
 1
 EB McM BR265320.298926.265465.298936. 239012.1 15 56 30.
 1
 EB McM BR265465.298936.265632.298995. 239012.1 15 56 30.
 1
 EB McM BR265632.298995.265738.299076. 239012.1 15 56 30.
 1
 EB McM TH BR265738.299076.265818.299184. 93012.1 15 44 30.
 1
 EB McM TH BR265818.299184.265950.299333. 93012.1 15 44 30.
 2
 EB McM TH BR265928.299309.265822.299188. 15 24 2
 60 33 2.0 930 73.3 1691 1 3
 1
 EB McM RT BR265738.299076.265889.299231. 146012.1 15 44 30.
 1
 EB McM RT BR265889.299231.265954.299262. 146012.1 15 44 30.
 1
 EB McM RT BR265954.299262.266019.299236. 146012.1 15 44 30.
 1
 EB McM RT BR266019.299236.266061.299150. 146012.1 15 44 30.
 1
 EB McM dep AG265950.299333.266013.299414. 108012.1 0 44 30.
 1
 EB McM dep AG266013.299414.266179.299586. 108012.1 0 44 30.
 1
 EB McM dep AG266179.299586.266265.299652. 108012.1 0 44 30.
 1
 EB McM dep AG266265.299652.266419.299706. 108012.1 0 44 30.
 1
 WB McM aprch AG266393.299727.266254.299670. 30012.1 0 44 30.
 1
 WB McM aprch AG266254.299670.266166.299603. 30012.1 0 44 30.
 1
 WB McM aprch BR266166.299603.265955.299385. 30012.1 15 44 30.
 2
 WB McM TH BR265993.299424.266107.299542. 15 24 2
 60 33 2.0 300 73.3 1691 1 3
 1
 WB McM departBR265955.299385.265793.299222. 50012.1 15 44 30.
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 WB McM departBR265793.299222.265665.299086. 50012.1 15 56 30.
 1
 WB McM departBR265665.299086.265558.299020. 50012.1 15 56 30.
 1
 WB McM departBR265558.299020.265431.298984. 50012.1 15 56 30.
 1
 WB McM departBR265431.298984.265282.298980. 50012.1 15 56 30.
 1
 WB McM departBR265282.298980.264828.299042. 50012.1 15 56 30.
 1
 WB Conn ap AG266061.299150.266083.299066. 146012.1 0 56 30.
 1
 WB Conn ap AG266083.299066.266082.298968. 146012.1 0 56 30.
 1
 WB Conn ap AG266082.298968.266046.298872. 146012.1 0 56 30.
 1
 WB Conn ap AG266046.298872.265993.298803. 146012.1 0 56 30.
 1
 WB Conn ap AG265993.298803.265875.298712. 146012.1 0 56 30.
 2
 WB Conn ap AG265916.298744.265990.298801. 0 36 3
 60 27 2.0 1460 73.3 1506 1 3
 1
 NB Cen ap AG266302.298032.266154.298263. 53012.1 0 56 30.
 1
 NB Cen ap AG266154.298263.265990.298522. 53012.1 0 68 30.
 1
 NB Cen ap AG265990.298522.265910.298684. 53012.1 0 68 30.

2	NB	Cen ap	AG265918.298668.265987.298527.	0 48 4
60	39	2.0 530 73.3 1399 1 3		
1	NB	Cen depart	AG265910.298684.265863.298827.	39012.1 0 56 30.
1	NB	Cen depart	AG265863.298827.265839.298979.	39012.1 0 56 30.
1	NB	Cen depart	AG265839.298979.265832.299119.	39012.1 0 56 30.
1	NB	Cen depart	AG265832.299119.265857.299590.	39012.1 0 56 30.
1	NB	Cen depart	AG265857.299590.265854.299736.	39012.1 0 56 30.
1	NB	Cen depart	AG265854.299736.265839.299907.	39012.1 0 56 30.
1	SB	Cen ap	AG265813.299907.265830.299690.	64012.1 0 44 30.
1	SB	Cen ap	AG265830.299690.265832.299574.	64012.1 0 44 30.
1	SB	Cen ap	AG265832.299574.265822.299461.	64012.1 0 44 30.
1	SB	Cen ap	AG265822.299461.265786.299087.	64012.1 0 44 30.
1	SB	Cen ap	AG265786.299087.265808.298897.	64012.1 0 44 30.
1	SB	Cen ap	AG265808.298897.265855.298729.	64012.1 0 56 30.
2	SB	Cen ap	AG265846.298759.265809.298892.	0 36 3
60	39	2.0 640 73.3 1403 1 3		
1	SB	Cen depart	AG265855.298729.265878.298636.	189012.1 0 44 30.
1	SB	Cen depart	AG265878.298636.265930.298525.	189012.1 0 44 30.
1	SB	Cen depart	AG265930.298525.266171.298181.	189012.1 0 44 30.
1	SB	Cen depart	AG266171.298181.266281.298020.	189012.1 0 44 30.
1	NB	Conn dep	AG265886.298692.265989.298763.	35012.1 0 44 30.
1	NB	Conn dep	AG265989.298763.266061.298843.	35012.1 0 44 30.
1	NB	Conn dep	AG266061.298843.266101.298938.	35012.1 0 44 30.
1	NB	Conn dep	AG266101.298938.266114.299035.	35012.1 0 44 30.
1	NB	Conn dep	AG266114.299035.266099.299124.	35012.1 0 44 30.
1	NB	Conn dep	AG266099.299124.266074.299186.	35012.1 0 44 30.
1	NB	Conn dep	BR266074.299186.265986.299361.	35012.1 15 44 30.
2	NB	Conn dep	BR266000.299333.266073.299188.	15 36 3
60	33	2.0 350 73.3 1630 1 3		
1	NB	I-75	AG265327.298041.265368.298889.	507012.9 0 80 30.
1	NB	I-75	AG265368.298889.265421.299301.	507012.9 0 80 30.
1	NB	I-75	AG265421.299301.265572.299874.	507012.9 0 80 30.
1	SB	I-75	AG265463.299836.265358.299399.	787012.9 0 80 30.
1	SB	I-75	AG265358.299399.265280.298741.	787012.9 0 80 30.
1	SB	I-75	AG265280.298741.265243.298097.	787012.9 0 80 30.
1.0	04	1000. 0Y 5 0 72		
		Central & McMillan Alt E PM	60.0321.0.0000.000210.30480000	1 1
		SE MID S	266089. 298420.	5.0
		SE 164 S	266017. 298537.	5.0
		SE 82 S	265980. 298608.	5.0
		SE CNR	265952. 298689.	5.0
		SE 82 E	266009. 298754.	5.0
		SE 164 E	266067. 298814.	5.0
		SE MID E	266130. 298970.	5.0
		SE 164 S	266081. 299220.	5.0
		SE 82 S	266044. 299294.	5.0
		SE CNR	266014. 299370.	5.0
		SE 82 E	266072. 299443.	5.0
		SE 164 E	266129. 299503.	5.0
		SE MID E	266236. 299603.	5.0
		NE MID E	266197. 299656.	5.0
		NE 164 E	266064. 299530.	5.0
		NE 82 E	266006. 299471.	5.0
		NE CNR	265950. 299412.	5.0
		NE CNR	265869. 299339.	5.0
		NE 82 N	265872. 299412.	5.0
		NE 164 N	265876. 299494.	5.0
		NE MID N	265881. 299614.	5.0
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1	EB	McM	BR264826.298986.265320.298926.	113012.1 15 56 30.
1	EB	McM	BR265320.298926.265465.298936.	113012.1 15 56 30.
1	EB	McM	BR265465.298936.265632.298995.	113012.1 15 56 30.
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EB	McM	BR265632.298995.265738.299076.	113012.1 15 56 30.
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EB	McM TH	BR265738.299076.265818.299184.	39012.1 15 44 30.
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EB	McM TH	BR265818.299184.265950.299333.	39012.1 15 44 30.
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EB	McM TH	BR265928.299309.265822.299188.	15 24 2
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EB	McM RT	BR265738.299076.265889.299231.	74012.1 15 44 30.
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EB	McM RT	BR265889.299231.265954.299262.	74012.1 15 44 30.
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EB	McM RT	BR265954.299262.266019.299236.	74012.1 15 44 30.
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EB	McM RT	BR266019.299236.266061.299150.	74012.1 15 44 30.
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EB	McM dep	AG265950.299333.266013.299414.	48012.1 0 44 30.
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EB	McM dep	AG266013.299414.266179.299586.	48012.1 0 44 30.
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EB	McM dep	AG266179.299586.266265.299652.	48012.1 0 44 30.
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EB	McM dep	AG266265.299652.266419.299706.	48012.1 0 44 30.
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WB	McM aprch	AG266393.299727.266254.299670.	89012.1 0 44 30.
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WB	McM aprch	AG266254.299670.266166.299603.	89012.1 0 44 30.
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WB	McM aprch	BR266166.299603.265955.299385.	89012.1 15 44 30.
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WB	McM TH	BR265993.299424.266107.299542.	15 24 2
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WB	McM depart	BR265793.299222.265665.299086.	209012.1 15 56 30.
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WB	McM depart	BR265665.299086.265558.299020.	209012.1 15 56 30.
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WB	McM depart	BR265558.299020.265431.298984.	209012.1 15 56 30.
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WB	McM depart	BR265431.298984.265282.298980.	209012.1 15 56 30.
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WB	McM depart	BR265282.298980.264828.299042.	209012.1 15 56 30.
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WB	Conn ap	AG266061.299150.266083.299066.	74012.1 0 56 30.
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WB	Conn ap	AG266083.299066.266082.298968.	74012.1 0 56 30.
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WB	Conn ap	AG266082.298968.266046.298872.	74012.1 0 56 30.
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WB	Conn ap	AG266046.298872.265993.298803.	74012.1 0 56 30.
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WB	Conn ap	AG265993.298803.265875.298712.	74012.1 0 56 30.
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WB	Conn ap	AG265916.298744.265990.298801.	0 36 3
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NB	Cen ap	AG266302.298032.266154.298263.	210012.1 0 56 30.
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NB	Cen ap	AG266154.298263.265990.298522.	210012.1 0 68 30.
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NB	Cen ap	AG265990.298522.265910.298684.	210012.1 0 68 30.
2			
NB	Cen ap	AG265918.298668.265987.298527.	0 48 4
60	32	2.0 2100 73.3 1555 1 3	
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NB	Cen depart	AG265910.298684.265863.298827.	98012.1 0 56 30.
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NB	Cen depart	AG265863.298827.265839.298979.	98012.1 0 56 30.
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NB	Cen depart	AG265839.298979.265832.299119.	98012.1 0 56 30.
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NB	Cen depart	AG265832.299119.265857.299590.	98012.1 0 56 30.
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NB	Cen depart	AG265857.299590.265854.299736.	98012.1 0 56 30.
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NB	Cen depart	AG265854.299736.265839.299907.	98012.1 0 56 30.
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SB	Cen ap	AG265813.299907.265830.299690.	78012.1 0 44 30.
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SB	Cen ap	AG265832.299574.265822.299461.	78012.1 0 44 30.
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SB	Cen ap	AG265822.299461.265786.299087.	78012.1 0 44 30.
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SB	Cen ap	AG265786.299087.265808.298897.	78012.1 0 44 30.
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SB	Cen ap	AG265808.298897.265855.298729.	78012.1 0 56 30.
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SB	Cen ap	AG265846.298759.265809.298892.	0 36 3
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1			
SB	Cen depart	AG265855.298729.265878.298636.	135012.1 0 44 30.
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SB	Cen depart	AG265878.298636.265930.298525.	135012.1 0 44 30.

1	SB	Cen depart	AG265929.298554.266278.298019.	132012.1	0	44	30.
1	EB	McM aprch	BR264648.299034.265403.298932.	154012.1	15	44	30.
1	EB	McM thru+I	BR265403.298932.265612.298913.	91012.1	15	44	30.
1	EB	McM thru+I	AG265612.298913.265821.298881.	91012.1	0	44	30.
2	EB	McM thr+lt	AG265773.298888.265617.298912.	0.	24	2	
65			34 2.0 910 73.3 1650 1 3				
1	EB	McM right	AG265403.298932.265757.298877.	63012.1	0	32	30.
2	EB	McM right	AG265751.298878.265603.298901.	0.	12	1	
65			34 2.0 630 73.3 1509 1 3				
1	EB	McM right	AG265757.298877.265798.298862.	63012.1	0	32	30.
1	EB	McM right	AG265798.298862.265827.298834.	63012.1	0	32	30.
1	EB	McM depart	AG265821.298884.265876.298929.	71012.1	0	44	30.
1	EB	McM depart	AG265876.298929.265913.298986.	71012.1	0	44	30.
1	EB	McM depart	AG265912.298988.265938.299116.	72012.1	0	44	30.
1	EB	McM depart	AG265938.299116.265975.299226.	72012.1	0	44	30.
1	EB	McM depart	AG265975.299226.266163.299539.	72012.1	0	44	30.
1	EB	McM depart	AG266163.299539.266220.299610.	72012.1	0	44	30.
1	EB	McM depart	AG266220.299610.266293.299664.	72012.1	0	44	30.
1	EB	McM depart	AG266293.299664.266414.299711.	72012.1	0	44	30.
1	WB	McM aprch	AG266380.299736.266244.299666.	20012.1	0	44	30.
1	WB	McM aprch	AG266244.299666.266173.299596.	20012.1	0	44	30.
1	WB	McM aprch	AG266173.299596.265969.299259.	20012.1	0	44	30.
1	WB	McM aprch	AG265969.299259.265933.299173.	20012.1	0	44	30.
1	WB	McM aprch	AG265933.299173.265909.299091.	20012.1	0	44	30.
1	WB	McM aprch	AG265909.299091.265892.299010.	20012.1	0	44	30.
1	WB	McM aprch	AG265892.299010.265856.298942.	20012.1	0	44	30.
2	WB	McM aprch	AG265892.299011.265868.298965.	0.	24	2	
65			47 2.0 200 73.3 1678 1 3				
1	WB	McM depart	AG265856.298942.265752.298914.	37012.1	0	44	30.
1	WB	McM depart	BR265752.298914.264661.299060.	37012.1	15	44	30.
1	NB	I-75	AG265324.298040.265380.298899.	584012.9	0	80	30.
1	NB	I-75	AG265380.298899.265402.299143.	584012.9	0	80	30.
1	NB	I-75	AG265402.299143.265454.299420.	584012.9	0	80	30.
1	NB	I-75	AG265454.299420.265576.299875.	584012.9	0	80	30.
1	SB	I-75	AG265474.299844.265416.299648.	875012.9	0	80	30.
1	SB	I-75	AG265416.299648.265345.299344.	875012.9	0	80	30.
1	SB	I-75	AG265345.299344.265316.299152.	875012.9	0	80	30.
1	SB	I-75	AG265316.299152.265292.298925.	875012.9	0	80	30.
1	SB	I-75	AG265292.298925.265238.298100.	875012.9	0	80	30.
1.0			04 1000. 0Y 5 0 72				
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	SE	164 S	265938. 298713. 5.0				
	SE	82 S	265912. 298793. 5.0				
	SE	CNR	265918. 298875. 5.0				
	SE	82 E	265934. 298958. 5.0				
	SE	164 E	265949. 299039. 5.0				
	SE	MID E	265999. 299214. 5.0				
	NE	MID E	265976. 299319. 5.0				
	NE	164 E	265908. 299163. 5.0				
	NE	82 E	265886. 299084. 5.0				
	NE	CNR	265865. 298999. 5.0				
	NE	82 N	265859. 299083. 5.0				
	NE	164 N	265860. 299164. 5.0				
	NE	MID N	265871. 299350. 5.0				
		Central & McMillan Alt I	PM 58 1 0				
1	NB	Cen aprch	AG266300.298030.265981.298520.	160012.1	0	56	30.
1	NB	Cen aprch	AG265981.298520.265930.298621.	160012.1	0	56	30.
1	NB	Cen th+rt	AG265930.298621.265887.298770.	99012.1	0	44	30.

WB McM departBR265752.298914.264661.299060. 134012.1 15 44 30.
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 NB I-75 AG265324.298040.265380.298899. 785612.9 0 80 30.
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 NB I-75 AG265454.299420.265576.299875. 785612.9 0 80 30.
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 SB I-75 AG265316.299152.265292.298925. 672012.9 0 80 30.
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 SB I-75 AG265292.298925.265238.298100. 672012.9 0 80 30.
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 Central & McMillan No Bld AM 60.0321.0.0000.000140.30480000 1 1
 SE MID S 265957. 298638. 5.0
 SE 164 S 265938. 298713. 5.0
 SE 82 S 265912. 298793. 5.0
 SE CNR 265918. 298875. 5.0
 SE 82 E 265934. 298958. 5.0
 SE 164 E 265949. 299039. 5.0
 SE MID E 265999. 299214. 5.0
 NE MID E 265976. 299319. 5.0
 NE 164 E 265908. 299163. 5.0
 NE 82 E 265886. 299084. 5.0
 NE CNR 265865. 298999. 5.0
 NE 82 N 265859. 299083. 5.0
 NE 164 N 265860. 299164. 5.0
 NE MID N 265871. 299350. 5.0
 Central & McMillan No Bld AM 89 1 0
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 NB Cen aprch AG266300.298030.265981.298520. 40012.1 0 56 30.
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 NB Cen aprch AG265981.298520.265930.298621. 40012.1 0 56 30.
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 NB Cen th+rt AG265930.298621.265887.298770. 25012.1 0 44 30.
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 NB Cen thru AG265887.298770.265848.298926. 24012.1 0 44 30.
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 NB Cen thru AG265860.298880.265887.298772. 0. 24 2
 65 24 2.0 240 73.3 1691 1 3
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 NB Cen right AG265896.298777.265889.298867. 1012.1 0 32 30.
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 NB Cen right AG265890.298859.265896.298777. 0. 12 1
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 NB Cen right AG265889.298867.265913.298986. 1012.1 0 32 30.
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 NB Cen left AG265930.298621.265871.298749. 15012.1 0 44 30.
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 NB Cen left AG265871.298749.265834.298915. 15012.1 0 44 30.
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 NB Cen left AG265843.298876.265868.298761. 0. 24 2
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 NB Cen departAG265848.298926.265835.299123. 45012.1 0 56 30.
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 NB Cen departAG265835.299123.265854.299553. 45012.1 0 56 30.
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 NB Cen departAG265854.299553.265853.299734. 45012.1 0 56 30.
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 NB Cen departAG265853.299734.265840.299908. 45012.1 0 56 30.
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 SB Cen aprch AG265814.299905.265829.299697. 72012.1 0 44 30.
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 SB Cen aprch AG265829.299697.265831.299539. 72012.1 0 44 30.
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 SB Cen aprch AG265805.298976.265800.299111. 0. 36 3
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 SB Cen departAG265807.298918.265870.298694. 132012.1 0 44 30.
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 EB McM aprch BR264648.299034.265403.298932. 154012.1 15 44 30.
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 EB McM thru+IBR265403.298932.265612.298913. 91012.1 15 44 30.
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 EB McM thru+IAG265612.298913.265821.298881. 91012.1 0 44 30.
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 EB McM thr+ItAG265773.298888.265617.298912. 0. 24 2
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 EB McM right AG265403.298932.265757.298877. 63012.1 0 32 30.
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EB	McM right	AG265798.298862.265827.298834.	63012.1 0 32 30.
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EB	McM depart	AG265821.298884.265876.298929.	71012.1 0 44 30.
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EB	McM depart	AG265876.298929.265913.298986.	71012.1 0 44 30.
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EB	McM depart	AG266220.299610.266293.299664.	72012.1 0 44 30.
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WB	McM aprch	AG266244.299666.266173.299596.	20012.1 0 44 30.
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WB	McM aprch	AG265969.299259.265933.299173.	20012.1 0 44 30.
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WB	McM aprch	AG265933.299173.265909.299091.	20012.1 0 44 30.
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WB	McM aprch	AG265909.299091.265892.299010.	20012.1 0 44 30.
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WB	McM aprch	AG265892.299010.265856.298942.	20012.1 0 44 30.
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WB	McM aprch	AG265892.299011.265868.298965.	0. 24 2
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WB	McM depart	AG265856.298942.265752.298914.	37012.1 0 44 30.
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WB	McM depart	BR265752.298914.264661.299060.	37012.1 15 44 30.
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EB	south loop	AG265839.298518.265812.298456.	76012.1 0 32 30.
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EB	south loop	AG265713.298377.265652.298363.	76012.1 0 32 30.
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EB	south loop	AG265652.298363.265590.298367.	76012.1 0 32 30.
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EB	south loop	AG265590.298367.265531.298389.	76012.1 0 32 30.
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EB	south loop	AG265477.298437.265443.298496.	76012.1 0 32 30.
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WB	north loop	AG265353.299266.265381.299332.	29312.1 0 32 30.
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WB	north loop	AG265381.299332.265459.299404.	29312.1 0 32 30.
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WB	north loop	AG265605.299422.265670.299394.	29312.1 0 32 30.
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WB	north loop	AG265724.299345.265757.299282.	29312.1 0 32 30.
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WB	north loop	AG265757.299282.265766.299216.	29312.1 0 32 30.
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WB	north loop	AG265766.299216.265750.299137.	29312.1 0 32 30.
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WB	north loop	AG265750.299137.265713.299078.	29312.1 0 32 30.
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WB	north loop	AG265713.299078.265656.299025.	29312.1	0	32	30.
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WB	north loop	AG265656.299025.265590.298989.	29312.1	0	32	30.
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WB	north loop	AG265590.298989.265525.298971.	29312.1	0	32	30.
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WB	north loop	AG265525.298971.265373.298968.	29312.1	0	32	30.
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NB	I-75	AG265311.298053.265356.298545.	489212.9	0	68	30.
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NB	I-75	AG265356.298545.265415.298994.	489212.9	0	68	30.
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NB	I-75	AG265415.298994.265521.299559.	489212.9	0	68	30.
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SB	I-75	AG265415.299817.265341.299495.	767412.9	0	68	30.
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SB	I-75	AG265297.299275.265264.299008.	767412.9	0	68	30.
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SB	I-75	AG265250.298765.265228.298107.	767412.9	0	68	30.
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Central & McMillan No Bld PM 60.0321.0.0000.000140.30480000 1 1						
SE	MID S	265957.	298638.	5.0		
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SE	82 S	265912.	298793.	5.0		
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SE	82 E	265934.	298958.	5.0		
SE	164 E	265949.	299039.	5.0		
SE	MID E	265999.	299214.	5.0		
NE	MID E	265976.	299319.	5.0		
NE	164 E	265908.	299163.	5.0		
NE	82 E	265886.	299084.	5.0		
NE	CNR	265865.	298999.	5.0		
NE	82 N	265859.	299083.	5.0		
NE	164 N	265860.	299164.	5.0		
NE	MID N	265871.	299350.	5.0		
Central & McMillan No Bld PM 89 1 0						
NB	Cen aprch	AG266300.298030.265981.298520.	160012.1	0	56	30.
1						
NB	Cen aprch	AG265981.298520.265930.298621.	160012.1	0	56	30.
1						
NB	Cen th+rt	AG265930.298621.265887.298770.	99012.1	0	44	30.
1						
NB	Cen thru	AG265887.298770.265848.298926.	97012.1	0	44	30.
2						
NB	Cen thru	AG265860.298880.265887.298772.	0.	24	2	
120	56	2.0	970	73.3	1691	1 3
1						
NB	Cen right	AG265896.298777.265889.298867.	2012.1	0	32	30.
2						
NB	Cen right	AG265890.298859.265896.298777.	0.	12	1	
120	56	2.0	20	73.3	1509	1 3
1						
NB	Cen right	AG265889.298867.265913.298986.	2012.1	0	32	30.
1						
NB	Cen left	AG265930.298621.265871.298749.	61012.1	0	44	30.
1						
NB	Cen left	AG265871.298749.265834.298915.	61012.1	0	44	30.
2						
NB	Cen left	AG265843.298876.265868.298761.	0.	24	2	
120	90	2.0	610	73.3	1638	1 3
1						
NB	Cen depart	AG265848.298926.265835.299123.	115012.1	0	56	30.
1						
NB	Cen depart	AG265835.299123.265854.299553.	115012.1	0	56	30.
1						
NB	Cen depart	AG265854.299553.265853.299734.	115012.1	0	56	30.
1						
NB	Cen depart	AG265853.299734.265840.299908.	115012.1	0	56	30.
1						
SB	Cen aprch	AG265814.299905.265829.299697.	82012.1	0	44	30.
1						
SB	Cen aprch	AG265829.299697.265831.299539.	82012.1	0	44	30.
1						
SB	Cen aprch	AG265831.299539.265800.299112.	82012.1	0	44	30.
1						
SB	Cen aprch	AG265800.299112.265807.298918.	82012.1	0	56	30.
2						
SB	Cen aprch	AG265805.298976.265800.299111.	0.	36	3	
120	87	2.0	820	73.3	1630	1 3
1						
SB	Cen depart	AG265807.298918.265870.298694.	91012.1	0	44	30.
1						
SB	Cen depart	AG265870.298694.265929.298554.	91012.1	0	44	30.
1						
SB	Cen depart	AG265929.298554.266278.298019.	91012.1	0	44	30.
1						
EB	McM aprch	BR264648.299034.265403.298932.	66012.1	15	44	30.
1						
EB	McM thru+IBR	265403.298932.265612.298913.	43012.1	15	44	30.
1						
EB	McM thru+IAG	265612.298913.265821.298881.	43012.1	0	44	30.

2	EB	McM thr+ltAG265773.298888.265617.298912.	0. 24 2
120		76 2.0 430 73.3 1732 1 3	
1	EB	McM right AG265403.298932.265757.298877.	23012.1 0 32 30.
2	EB	McM right AG265751.298878.265603.298901.	0. 12 1
120		76 2.0 230 73.3 1687 1 3	
1	EB	McM right AG265757.298877.265798.298862.	23012.1 0 32 30.
1	EB	McM right AG265798.298862.265827.298834.	23012.1 0 32 30.
1	EB	McM departAG265821.298884.265876.298929.	27012.1 0 44 30.
1	EB	McM departAG265876.298929.265913.298986.	27012.1 0 44 30.
1	EB	McM departAG265912.298988.265938.299116.	29012.1 0 44 30.
1	EB	McM departAG265938.299116.265975.299226.	29012.1 0 44 30.
1	EB	McM departAG265975.299226.266163.299539.	29012.1 0 44 30.
1	EB	McM departAG266163.299539.266220.299610.	29012.1 0 44 30.
1	EB	McM departAG266220.299610.266293.299664.	29012.1 0 44 30.
1	EB	McM departAG266293.299664.266414.299711.	29012.1 0 44 30.
1	WB	McM aprch AG266380.299736.266244.299666.	61012.1 0 44 30.
1	WB	McM aprch AG266244.299666.266173.299596.	61012.1 0 44 30.
1	WB	McM aprch AG266173.299596.265969.299259.	61012.1 0 44 30.
1	WB	McM aprch AG265969.299259.265933.299173.	61012.1 0 44 30.
1	WB	McM aprch AG265933.299173.265909.299091.	61012.1 0 44 30.
1	WB	McM aprch AG265909.299091.265892.299010.	61012.1 0 44 30.
1	WB	McM aprch AG265892.299010.265856.298942.	61012.1 0 44 30.
2	WB	McM aprch AG265892.299011.265868.298965.	0. 24 2
120		87 2.0 610 73.3 1682 1 3	
1	WB	McM departAG265856.298942.265752.298914.	134012.1 0 44 30.
1	WB	McM departBR265752.298914.264661.299060.	134012.1 15 44 30.
1	EB	south loopAG265447.298923.265645.298862.	37012.1 0 32 30.
1	EB	south loopAG265645.298862.265771.298755.	37012.1 0 32 30.
1	EB	south loopAG265771.298755.265821.298673.	37012.1 0 32 30.
1	EB	south loopAG265821.298673.265843.298597.	37012.1 0 32 30.
1	EB	south loopAG265843.298597.265839.298518.	37012.1 0 32 30.
1	EB	south loopAG265839.298518.265812.298456.	37012.1 0 32 30.
1	EB	south loopAG265812.298456.265766.298407.	37012.1 0 32 30.
1	EB	south loopAG265766.298407.265713.298377.	37012.1 0 32 30.
1	EB	south loopAG265713.298377.265652.298363.	37012.1 0 32 30.
1	EB	south loopAG265652.298363.265590.298367.	37012.1 0 32 30.
1	EB	south loopAG265590.298367.265531.298389.	37012.1 0 32 30.
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1	EB	south loopAG265477.298437.265443.298496.	37012.1 0 32 30.
1	EB	south loopAG265443.298496.265425.298562.	37012.1 0 32 30.
1	EB	south loopAG265425.298562.265430.298755.	37012.1 0 32 30.
1	WB	north loopAG265332.298608.265338.299177.	49312.1 0 32 30.
1	WB	north loopAG265338.299177.265353.299266.	49312.1 0 32 30.
1	WB	north loopAG265353.299266.265381.299332.	49312.1 0 32 30.
1	WB	north loopAG265381.299332.265459.299404.	49312.1 0 32 30.
1	WB	north loopAG265459.299404.265525.299426.	49312.1 0 32 30.
1	WB	north loopAG265525.299426.265605.299422.	49312.1 0 32 30.
1	WB	north loopAG265605.299422.265670.299394.	49312.1 0 32 30.
1	WB	north loopAG265670.299394.265724.299345.	49312.1 0 32 30.
1	WB	north loopAG265724.299345.265757.299282.	49312.1 0 32 30.
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WB north loopAG265757.299282.265766.299216. 49312.1 0 32 30.
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 WB north loopAG265713.299078.265656.299025. 49312.1 0 32 30.
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 WB north loopAG265525.298971.265373.298968. 49312.1 0 32 30.
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 NB I-75 AG265311.298053.265356.298545. 789312.9 0 68 30.
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 NB I-75 AG265356.298545.265415.298994. 789312.9 0 68 30.
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 NB I-75 AG265415.298994.265521.299559. 789312.9 0 68 30.
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 NB I-75 AG265521.299559.265592.299877. 789312.9 0 68 30.
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 SB I-75 AG265415.299817.265341.299495. 603012.9 0 68 30.
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 SB I-75 AG265341.299495.265297.299275. 603012.9 0 68 30.
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 SB I-75 AG265297.299275.265264.299008. 603012.9 0 68 30.
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 SB I-75 AG265264.299008.265250.298765. 603012.9 0 68 30.
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 SB I-75 AG265250.298765.265228.298107. 603012.9 0 68 30.
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 Brent Spence Bridge T1alltpm.dat 60.0175.0.0000.000240.30480000 1 1
 R1 SB Mid 264384. 276323. 5.
 R2 SB 164 264321. 276211. 5.
 R3 SB 82 264290. 276136. 5.
 R4 SB Corner 264262. 276069. 5.
 R5 SB Corner 264230. 275990. 5.
 R6 SB 82 264193. 275900. 5.
 R7 SB 164 264151. 275798. 5.
 R8 SB Mid 264103. 275678. 5.
 R9 NB Mid 264155. 275655. 5.
 R10 NB 164 264184. 275729. 5.
 R11 NB 82 264215. 275805. 5.
 R12 NB Corner 264242. 275872. 5.
 R13 EB Corner 264272. 275903. 5.
 R14 EB 82 264340. 275765. 5.
 R15 EB 164 264378. 275678. 5.
 R16 EB Mid 264408. 275600. 5.
 R17 WB Mid 264455. 275722. 5.
 R18 WB 164 264399. 275833. 5.
 R19 WB 82 264362. 275906. 5.
 R20 WB Corner 264330. 275971. 5.
 R21 NB Corner 264319. 276046. 5.
 R22 NB 82 264343. 276114. 5.
 R23 NB 164 264376. 276189. 5.
 R24 NB Mid 264447. 276280. 5.
 Kyles Lane & Dixie Hwy-Trunc 37 1 1
 1
 01 Dixie NB Appr AG264099.275553.264162.275726. 760.11.5 0. 44. 30.
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 02 Dixie NB Appr AG264162.275726.264197.275813. 760.11.5 0. 44. 30.
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 03 Dixie NB Appr AG264197.275813.264240.275916. 760.11.5 0. 44. 30.
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 04 Dixie NB Queue AG264228.275888.264205.275831. 0. 24. 2
 100 75 2.0 760 73.3 1511 1 3
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 05 Dixie NB @ KylesAG264240.275916.264280.276013. 540.11.5 0. 44. 30.
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 06 Dixie NB Depart AG264280.276013.264303.276071. 465.11.5 0. 44. 30.
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 07 Dixie NB Depart AG264303.276071.264360.276209. 1295.11.5 0. 44. 30.
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 08 Dixie NB Depart AG264360.276209.264406.276278. 1295.11.5 0. 44. 30.
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 09 Dixie NB Depart AG264406.276278.264446.276325. 1295.11.5 0. 44. 30.
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 10 Dixie NB Depart AG264446.276325.264529.276400. 1295.11.5 0. 44. 30.
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 11 Dixie SB Appr AG264499.276415.264439.276361. 1600.11.5 0. 44. 30.
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 12 Dixie SB Appr AG264439.276361.264381.276288. 1600.11.5 0. 44. 30.
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 13 Dixie SB Appr AG264381.276288.264351.276234. 1600.11.5 0. 44. 30.
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 14 Dixie SB Appr AG264351.276234.264252.275994. 1600.11.5 0. 44. 30.
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 15 Dixie SB QTRUNC AG264276.276054.264351.276234. 197.100. 0. 24. 30.
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 16 Dixie SB QTRUNC AG264351.276234.264365.276261. 197.100. 0. 24. 30.
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 17 Dixie SB @ KylesAG264252.275994.264236.275956. 965.11.5 0. 40. 30.
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 18 Dixie SB Depart AG264236.275956.264179.275824. 1345.11.5 0. 44. 30.
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 19 Dixie SB Depart AG264179.275824.264143.275732. 1345.11.5 0. 44. 30.
 1

20 Dixie SB Depart AG264143.275732.264083.275564. 1345.11.5 0. 44. 30.
1
21 Dixie NB Rt. AG264240.275916.264284.275929. 310.11.5 0. 32. 30.
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22 Kyles EB @ DixieAG264252.275994.264284.275929. 650.11.5 0. 32. 30.
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23 Kyles EB Depart AG264284.275929.264483.275522. 960.11.5 0. 44. 30.
1
24 Kyles WB Appr AG264516.275540.264468.275639. 1240.11.5 0. 56. 30.
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25 Kyles WB Appr AG264468.275639.264359.275852. 1240.11.5 0. 56. 30.
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26 Kyles WB Rt. AG264359.275852.264347.275900. 830.11.5 0. 32. 30.
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27 Kyles WB Rt. AG264347.275900.264300.276003. 830.11.5 0. 32. 30.
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28 Kyles WB Rt. QuAG264313.275975.264339.275917. 0. 12. 1
100 59 2.0 830 73.3 1599 1 3
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29 Kyles WB Rt. @ DAG264300.276003.264303.276071. 830.11.5 0. 32. 30.
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30 Kyles WB Appr AG264359.275852.264296.275980. 30.11.5 0. 32. 30.
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31 WB Kyles LAG264307.275957.264338.275894. 0. 12. 1
100 59 2.0 30 73.3 1881 1 3
1
32 Kyles WB @ DixieAG264296.275980.264280.276013. 15.11.5 0. 32. 30.
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33 Kyles WB Lt. AG264296.275980.264252.275994. 15.11.5 0. 32. 30.
1
34 Kyles WB Lt. AG264359.275852.264325.275892. 380.11.5 0. 32. 30.
1
35 Kyles WB Lt. AG264325.275892.264287.275965. 380.11.5 0. 32. 30.
2
36 Kyles WB Lt. QueAG264295.275951.264321.275898. 0. 12. 1
100 59 2.0 380 73.3 1357 1 3
1
37 Kyles WB Lt. @ DAG264287.275965.264236.275956. 380.11.5 0. 32. 30.
1.0 04 1000. 0Y 5 0 72

JOB: Brent Spence Bridge NB-AM S1altEam.dat RUN: Kyles Lane & Dixie Hwy
 DATE: 08/30/2010 TIME: 11:48:09.42

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	*	184.	20.	AG	1520.	11.5	.0	44.0		
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	*	94.	22.	AG	1520.	11.5	.0	44.0		
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	*	112.	23.	AG	1520.	11.5	.0	44.0		
4. 03 Dixie NB Queue	* 264228.0	275888.0	263366.3	273751.5	*	2304.	202.	AG	240.	100.0	.0	24.0	1.35	117.0
5. 04 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	*	105.	22.	AG	1240.	11.5	.0	44.0		
6. 05 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	*	62.	22.	AG	1245.	11.5	.0	44.0		
7. 06 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	*	149.	22.	AG	1955.	11.5	.0	44.0		
8. 07 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	*	83.	34.	AG	1955.	11.5	.0	44.0		
9. 08 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	*	62.	40.	AG	1955.	11.5	.0	44.0		
10. 09 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	*	112.	48.	AG	1955.	11.5	.0	44.0		
11. 10 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	*	81.	228.	AG	1020.	11.5	.0	44.0		
12. 11 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	*	93.	218.	AG	1020.	11.5	.0	44.0		
13. 12 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	*	62.	209.	AG	1020.	11.5	.0	44.0		
14. 13 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	*	260.	202.	AG	1020.	11.5	.0	44.0		
15. 14 Dixie SB Queue	* 264276.0	276054.0	264319.2	276156.8	*	112.	23.	AG	175.	100.0	.0	24.0	.55	5.7
16. 14 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	*	41.	203.	AG	505.	11.5	.0	40.0		
17. 15 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	*	144.	203.	AG	665.	11.5	.0	44.0		
18. 16 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	*	99.	201.	AG	665.	11.5	.0	44.0		
19. 17 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	*	178.	200.	AG	665.	11.5	.0	44.0		
20. 18 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	*	46.	74.	AG	280.	11.5	.0	32.0		
21. 19 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	*	72.	154.	AG	520.	11.5	.0	32.0		
22. 20 Kyles EB Depart	* 264284.0	275929.0	264483.0	275522.0	*	453.	154.	AG	800.	11.5	.0	44.0		
23. 21 Kyles WB Appr	* 264516.0	275540.0	264468.0	275639.0	*	110.	334.	AG	880.	11.5	.0	56.0		
24. 22 Kyles WB Appr	* 264468.0	275639.0	264359.0	275852.0	*	239.	333.	AG	880.	11.5	.0	56.0		
25. 23 Kyles WB Rt.	* 264359.0	275852.0	264347.0	275900.0	*	49.	346.	AG	710.	11.5	.0	32.0		
26. 24 Kyles WB Rt.	* 264347.0	275900.0	264300.0	276003.0	*	113.	335.	AG	710.	11.5	.0	32.0		
27. 25 Kyles WB Rt. Qu	* 264313.0	275975.0	265401.9	273547.2	*	2661.	156.	AG	129.	100.0	.0	12.0	1.48	135.2
28. 25 Kyles WB Rt. @ D	* 264300.0	276003.0	264303.0	276071.0	*	68.	3.	AG	710.	11.5	.0	32.0		
29. 26 Kyles WB Appr	* 264359.0	275852.0	264296.0	275980.0	*	143.	334.	AG	10.	11.5	.0	32.0		
30. 28 WB Kyles L	* 264307.0	275957.0	264308.4	275954.1	*	3.	154.	AG	129.	100.0	.0	12.0	.02	.2
31. 27 Kyles WB @ Dixie	* 264296.0	275980.0	264280.0	276013.0	*	37.	334.	AG	5.	11.5	.0	32.0		
32. 28 Kyles WB Lt.	* 264296.0	275980.0	264252.0	275994.0	*	46.	288.	AG	5.	11.5	.0	32.0		
33. 29 Kyles WB Lt.	* 264359.0	275852.0	264325.0	275892.0	*	53.	320.	AG	160.	11.5	.0	32.0		
34. 30 Kyles WB Lt.	* 264325.0	275892.0	264287.0	275965.0	*	82.	333.	AG	160.	11.5	.0	32.0		
35. 33 Kyles WB Lt. Que	* 264295.0	275951.0	264317.7	275904.7	*	52.	154.	AG	129.	100.0	.0	12.0	.40	2.6
36. 31 Kyles WB Lt. @ D	* 264287.0	275965.0	264236.0	275956.0	*	52.	260.	AG	140.	11.5	.0	32.0		

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JOB: Brent Spence Bridge NB-AM S1altEam.dat RUN: Kyles Lane & Dixie Hwy
 DATE: 08/30/2010 TIME: 11:48:09.42

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	EM	FAC	TYPE	RATE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
4. 03 Dixie NB Queue	* 90	55	2.0	1520	1641	73.30	1	3
15. 14 Dixie SB Queue	* 90	40	2.0	1020	1829	73.30	1	3
27. 25 Kyles WB Rt. Qu	* 90	59	2.0	710	1599	73.30	1	3
30. 28 WB Kyles L	* 90	59	2.0	10	1881	73.30	1	3
35. 33 Kyles WB Lt. Que	* 90	59	2.0	160	1343	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	*
1. R1 SB Mid	* 264384.0	276323.0		5.0 *
2. R2 SB 164	* 264321.0	276211.0		5.0 *
3. R3 SB 82	* 264290.0	276136.0		5.0 *
4. R4 SB Corner	* 264262.0	276069.0		5.0 *
5. R5 SB Corner	* 264230.0	275990.0		5.0 *
6. R6 SB 82	* 264193.0	275900.0		5.0 *
7. R7 SB 164	* 264151.0	275798.0		5.0 *
8. R8 SB Mid	* 264103.0	275678.0		5.0 *
9. R9 NB Mid	* 264155.0	275655.0		5.0 *
10. R10 NB 164	* 264184.0	275729.0		5.0 *
11. R11 NB 82	* 264215.0	275805.0		5.0 *
12. R12 NB Corner	* 264242.0	275872.0		5.0 *
13. R13 EB Corner	* 264272.0	275903.0		5.0 *
14. R14 EB 82	* 264340.0	275765.0		5.0 *
15. R15 EB 164	* 264378.0	275678.0		5.0 *
16. R16 EB Mid	* 264408.0	275600.0		5.0 *
17. R17 WB Mid	* 264455.0	275722.0		5.0 *
18. R18 WB 164	* 264399.0	275833.0		5.0 *
19. R19 WB 82	* 264362.0	275906.0		5.0 *
20. R20 WB Corner	* 264330.0	275971.0		5.0 *
21. R21 NB Corner	* 264319.0	276046.0		5.0 *
22. R22 NB 82	* 264343.0	276114.0		5.0 *
23. R23 NB 164	* 264376.0	276189.0		5.0 *
24. R24 NB Mid	* 264447.0	276280.0		5.0 *

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

0.	*	.1	.1	.1	.1	.1	.1	.1	.1	2.3	2.2	2.1	1.4	1.3	1.1	.9	.8	.1	.1	.5	1.0
5.	*	.1	.1	.2	.3	.3	.2	.2	.1	2.5	2.3	2.1	1.5	1.4	1.1	.8	.7	.1	.0	.3	.7
10.	*	.1	.3	.2	.5	.5	.3	.2	.3	2.5	2.3	2.0	1.6	1.5	.9	.8	.7	.0	.0	.2	.6
15.	*	.1	.3	.5	.7	.6	.6	.6	.6	2.3	2.1	1.7	1.5	1.6	.9	.8	.7	.0	.0	.0	.5
20.	*	.1	.4	.7	1.1	1.0	.7	.9	1.0	2.1	1.8	1.6	1.4	1.4	.8	.7	.7	.0	.0	.0	.3
25.	*	.2	.8	1.2	1.4	1.2	.9	1.1	1.3	1.4	1.6	1.2	1.4	1.1	.7	.7	.7	.0	.0	.0	.2
30.	*	.3	.9	1.4	1.8	1.3	1.2	1.3	1.6	1.0	1.2	1.2	1.1	1.0	.7	.7	.7	.0	.0	.0	.0
35.	*	.4	1.1	1.6	2.0	1.8	1.1	1.3	1.5	.9	.8	.8	.9	.7	.7	.7	.7	.0	.0	.0	.0
40.	*	.5	1.2	1.9	2.2	1.6	1.3	1.6	1.6	.6	.6	.6	.7	.6	.7	.7	.7	.0	.0	.0	.0
45.	*	.7	1.5	1.9	2.1	1.4	1.1	1.4	1.7	.5	.5	.5	.7	.7	.7	.7	.7	.0	.0	.0	.0
50.	*	.8	1.4	1.9	2.0	1.4	1.1	1.7	1.8	.3	.3	.3	.5	.7	.7	.7	.6	.0	.0	.0	.0
55.	*	.9	1.5	1.8	1.9	1.2	1.0	1.7	1.7	.4	.3	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
60.	*	1.2	1.4	1.7	1.9	1.1	1.1	1.6	1.6	.4	.4	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
65.	*	1.1	1.3	1.8	1.8	.9	1.1	1.7	1.7	.4	.4	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
70.	*	1.1	1.2	1.7	1.7	1.0	1.2	1.8	1.8	.4	.4	.4	.6	.7	.7	.7	.6	.0	.0	.0	.0
75.	*	1.2	1.1	1.5	1.5	1.1	1.2	1.4	1.6	.4	.4	.4	.4	.7	.7	.7	.6	.0	.0	.0	.0
80.	*	1.2	1.2	1.5	1.6	1.0	1.1	1.6	1.6	.4	.4	.4	.5	.6	.7	.7	.6	.0	.0	.0	.0
85.	*	1.0	1.0	1.5	1.6	.9	1.2	1.6	1.5	.4	.4	.3	.5	.7	.7	.7	.7	.0	.0	.0	.0
90.	*	1.0	1.1	1.5	1.6	.7	1.1	1.6	1.5	.2	.3	.3	.4	.8	.7	.7	.7	.0	.0	.0	.0
95.	*	1.0	1.0	1.5	1.5	1.0	1.0	1.6	1.4	.2	.3	.3	.5	.8	.7	.7	.7	.0	.0	.0	.0
100.	*	.9	1.0	1.5	1.4	1.1	1.1	1.5	1.4	.2	.3	.3	.4	.6	.7	.7	.7	.0	.0	.0	.0
105.	*	1.0	1.1	1.5	1.5	1.0	1.3	1.6	1.5	.2	.3	.3	.4	.7	.8	.8	.7	.0	.0	.0	.0
110.	*	1.0	1.0	1.6	1.6	1.0	1.4	1.6	1.4	.1	.2	.3	.4	.8	.8	.8	.7	.0	.0	.0	.0
115.	*	.9	1.0	1.6	1.5	1.1	1.5	1.6	1.4	.1	.2	.3	.4	.8	.8	.8	.6	.0	.0	.0	.0
120.	*	.9	1.0	1.6	1.5	1.3	1.6	1.5	1.3	.1	.2	.3	.4	.8	.8	.8	.6	.0	.1	.0	.1
125.	*	.9	1.0	1.5	1.4	1.3	1.6	1.5	1.3	.1	.2	.3	.4	.8	.8	.8	.6	.1	.1	.0	.1
130.	*	.9	1.0	1.5	1.4	1.4	1.7	1.5	1.3	.1	.1	.2	.5	.9	1.0	.8	.6	.1	.1	.0	.1
135.	*	1.0	1.0	1.6	1.5	1.5	1.6	1.4	1.4	.2	.1	.2	.5	.9	1.0	.7	.4	.1	.1	.2	.2
140.	*	.9	1.0	1.6	1.6	1.4	1.6	1.4	1.4	.2	.1	.3	.6	.9	.9	.7	.4	.2	.3	.2	.4
145.	*	1.0	1.0	1.7	1.6	1.3	1.5	1.4	1.4	.2	.1	.2	.5	.8	.9	.7	.4	.4	.4	.4	.6
150.	*	.9	1.2	1.8	1.7	1.3	1.5	1.5	1.3	.2	.1	.2	.3	.8	.7	.5	.3	.5	.6	.7	.8
155.	*	1.2	1.3	2.3	1.8	1.4	1.5	1.6	1.4	.1	.1	.2	.3	.7	.6	.4	.3	.7	1.0	.8	1.1
160.	*	1.1	1.4	2.3	2.0	1.3	1.6	1.4	1.4	.1	.0	.1	.2	.4	.4	.3	.1	.9	1.1	1.1	1.3
165.	*	1.2	1.6	2.4	1.9	1.1	1.5	1.5	1.4	.1	.0	.1	.1	.3	.3	.2	.1	.9	1.2	1.3	1.5
170.	*	1.2	1.7	2.6	1.4	1.2	1.6	1.6	1.5	.2	.1	.1	.1	.2	.1	.1	.0	.9	1.2	1.2	1.4
175.	*	1.3	1.7	2.5	1.6	1.1	1.8	1.7	1.5	.2	.2	.2	.2	.1	.1	.0	.0	1.0	1.2	1.1	1.4
180.	*	1.5	1.9	2.3	1.4	1.2	1.7	1.7	1.5	.4	.3	.3	.3	.1	.1	.0	.0	1.1	1.0	1.2	1.4
185.	*	1.5	2.1	2.2	1.5	1.5	1.8	1.9	1.5	.6	.5	.6	.2	.1	.0	.0	1.0	1.0	1.2	1.2	
190.	*	1.7	2.0	2.1	1.6	1.5	1.9	1.7	1.3	.9	.9	.8	.9	.2	.0	.0	.0	1.0	1.0	1.0	1.3
195.	*	1.6	1.9	1.9	1.4	1.4	1.7	1.6	1.2	1.3	1.4	1.3	1.4	.7	.1	.0	.0	.9	1.1	1.1	1.4
200.	*	1.6	1.7	1.7	1.3	1.3	1.4	1.4	1.0	1.7	1.7	1.8	1.9	.9	.1	.1	.0	.9	1.1	1.2	1.5
205.	*	1.4	1.3	1.2	1.1	1.1	1.2	1.0	.8	2.0	2.1	2.1	2.3	1.1	.2	.1	.1	.9	1.1	1.3	1.8

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

210.	*	1.2	.9	.8	.9	.7	.8	.7	.5	2.1	2.5	2.4	2.6	1.6	.3	.2	.1	.9	1.0	1.3	1.9
215.	*	.9	.5	.5	.3	.4	.5	.6	.3	2.1	2.5	2.5	2.7	1.7	.3	.2	.2	1.0	1.0	1.3	1.8
220.	*	.5	.3	.3	.2	.2	.2	.2	.2	2.3	2.5	2.3	2.5	1.7	.4	.2	.2	1.0	1.2	1.3	1.9
225.	*	.4	.2	.1	.1	.0	.1	.1	.1	2.1	2.3	2.3	2.3	1.6	.4	.2	.2	1.0	1.1	1.2	1.8
230.	*	.2	.1	.1	.1	.0	.1	.1	.1	2.0	2.2	2.2	2.2	1.4	.4	.2	.2	1.0	1.1	1.4	1.8
235.	*	.1	.1	.1	.1	.0	.1	.1	.0	2.0	2.0	2.2	2.2	1.2	.4	.2	.2	1.0	1.1	1.4	1.6
240.	*	.1	.1	.1	.1	.0	.1	.1	.0	1.9	2.0	2.0	2.1	1.1	.4	.3	.2	1.0	1.2	1.3	1.5
245.	*	.1	.1	.1	.1	.0	.0	.0	.0	1.8	1.9	1.8	1.8	1.1	.4	.3	.2	1.1	1.2	1.4	1.4
250.	*	.1	.1	.1	.1	.0	.0	.0	.0	1.8	1.8	1.8	1.8	1.0	.5	.3	.2	1.1	1.2	1.4	1.3
255.	*	.0	.1	.1	.0	.0	.0	.0	.0	1.7	1.7	1.7	1.7	.9	.4	.3	.2	1.1	1.1	1.3	1.2
260.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.9	.4	.3	.2	1.0	1.2	1.3	1.1
265.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.6	1.6	.7	.4	.4	.2	1.0	1.2	1.3	1.0
270.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.6	.8	.4	.3	.2	1.1	1.2	1.2	1.1
275.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.7	1.6	1.6	.8	.4	.3	.2	1.0	1.1	1.4	1.1
280.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.5	.7	.5	.4	.2	1.1	1.1	1.2	1.1
285.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.5	.7	.4	.4	.2	1.1	1.2	1.3	1.0
290.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.7	1.5	.8	.4	.3	.2	1.2	1.2	1.3	.9
295.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.5	.7	.4	.3	.2	1.1	1.3	1.3	.7
300.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.4	.8	.4	.3	.3	1.1	1.1	1.3	.9
305.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.4	.6	.6	.4	.2	1.1	.9	1.3	1.0
310.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.3	1.3	.6	.6	.3	.2	1.1	1.1	1.2	.9
315.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.2	.6	.4	.3	.3	1.0	1.1	1.1	1.0
320.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.2	.6	.4	.3	.3	.9	1.2	1.0	1.0
325.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.1	.7	.6	.4	.3	.8	.9	1.1	1.0
330.	*	.0	.0	.1	.1	.0	.0	.0	.0	1.7	1.7	1.7	1.2	.9	.5	.4	.4	.9	1.1	1.2	1.0
335.	*	.0	.0	.1	.1	.0	.0	.0	.0	1.8	1.8	1.8	1.1	1.0	.6	.5	.4	.7	.8	1.0	1.1
340.	*	.0	.0	.1	.1	.0	.0	.0	.0	2.0	1.8	1.8	1.1	.9	.6	.7	.5	.5	.6	.8	1.2
345.	*	.0	.1	.1	.1	.0	.1	.1	.0	2.1	2.1	1.9	1.1	.9	.9	.8	.5	.5	.6	.8	1.1

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350. * .1 .1 .1 .1 .0 .1 .1 .1 2.2 2.2 1.9 1.2 1.3 1.1 .8 .7 .2 .3 .5 1.0
355. * .1 .1 .1 .1 .1 .1 .1 .1 2.1 2.2 2.0 1.2 1.3 1.0 1.0 .9 .1 .2 .5 1.0
360. * .1 .1 .1 .1 .1 .1 .1 .1 2.3 2.2 2.1 1.4 1.3 1.1 .9 .8 .1 .1 .5 1.0
-----*-----
MAX * 1.7 2.1 2.6 2.2 1.8 1.9 1.9 1.8 2.5 2.5 2.5 2.7 1.7 1.1 1.0 .9 1.2 1.3 1.4 1.9
DEGR.* 190 185 170 40 35 190 185 50 5 210 215 215 215 0 355 355 290 295 230 210

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1

JOB: Brent Spence Bridge NB-AM S1altEam.dat

PAGE 5
 RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to
 the maximum concentration, only the first
 angle, of the angles with same maximum
 concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24

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-----*-----
0. * 1.7 1.5 1.3 .9
5. * 1.6 1.5 1.3 1.0
10. * 1.4 1.6 1.3 .9
15. * 1.3 1.5 1.4 .9
20. * 1.1 1.5 1.4 .9
25. * 1.0 1.2 1.3 .8
30. * .6 .9 1.2 .8
35. * .4 .7 .9 .7
40. * .1 .6 .6 .5
45. * .1 .3 .4 .3
50. * .0 .2 .3 .2
55. * .0 .1 .1 .1
60. * .0 .1 .0 .1
65. * .0 .1 .0 .0
70. * .0 .1 .0 .0
75. * .0 .1 .0 .0
80. * .0 .1 .0 .0
85. * .0 .1 .0 .0
90. * .0 .0 .0 .0
95. * .0 .0 .0 .0
100. * .0 .0 .0 .0
105. * .0 .0 .0 .0
110. * .0 .0 .0 .0
115. * .0 .0 .0 .0
120. * .0 .0 .0 .0
125. * .0 .0 .0 .0
130. * .0 .0 .0 .0
135. * .0 .0 .0 .0
140. * .1 .1 .0 .0
145. * .1 .1 .1 .0
150. * .3 .2 .1 .0
155. * .6 .2 .2 .0
160. * .6 .4 .2 .1
165. * .7 .5 .2 .1
170. * .9 .5 .3 .1
175. * 1.0 .6 .4 .1
180. * .8 .6 .5 .1
185. * 1.1 .6 .5 .2
190. * 1.2 1.1 .6 .3
195. * 1.3 1.4 1.2 .4
200. * 1.7 1.6 1.4 .3
205. * 1.7 1.7 1.7 .6

```

1

JOB: Brent Spence Bridge NB-AM S1altEam.dat

PAGE 6
 RUN: Kyles Lane & Dixie Hwy

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24

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-----*-----
210. * 1.9 1.8 1.8 .7
215. * 1.9 1.8 1.9 1.0
220. * 1.5 1.8 1.9 1.0
225. * 1.6 1.8 1.7 1.1
230. * 1.3 1.8 1.7 1.1
235. * 1.1 1.6 1.6 1.3
240. * 1.1 1.7 1.5 1.0
245. * 1.1 1.6 1.4 1.0
250. * 1.2 1.5 1.3 1.1
255. * 1.2 1.5 1.2 1.1
260. * 1.1 1.5 1.2 1.1
265. * 1.2 1.4 1.1 1.1
270. * 1.1 1.4 1.0 1.0
275. * 1.2 1.4 1.0 .9
280. * 1.3 1.4 1.0 .9
285. * 1.3 1.5 1.0 1.0
290. * 1.3 1.5 1.1 .9
295. * 1.4 1.5 1.1 .8
300. * 1.5 1.5 1.1 .9
305. * 1.4 1.4 1.0 .9
310. * 1.5 1.3 1.1 .9

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315. * 1.5 1.3 1.1 .9
 320. * 1.4 1.4 1.0 .9
 325. * 1.6 1.4 1.1 .9
 330. * 1.6 1.3 1.2 .8
 335. * 1.6 1.4 1.2 .9
 340. * 1.7 1.3 1.2 .9
 345. * 1.6 1.4 1.2 1.1
 350. * 1.6 1.5 1.4 1.0
 355. * 1.6 1.5 1.3 1.0
 360. * 1.7 1.5 1.3 .9

 MAX * 1.9 1.8 1.9 1.3
 DEGR. * 210 210 215 235

THE HIGHEST CONCENTRATION IS 2.70 PPM AT 215 DEGREES FROM REC12.
 THE 2ND HIGHEST CONCENTRATION IS 2.60 PPM AT 170 DEGREES FROM REC3 .
 THE 3RD HIGHEST CONCENTRATION IS 2.50 PPM AT 210 DEGREES FROM REC10.

1

JOB: Brent Spence Bridge NB-AM S1altEam.dat
 DATE: 08/30/2010 TIME: 11:48:09.42

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20	LINK #	190	185	170	40	35	190	185	50	5	210	215	215	215	0	355	355	290	295	230	210
1 *	.0	.0	.0	.0	.2	.4	.3	.7	.8	.3	.1	.1	.0	.0	.0	.0	.0	.1	.1		
2 *	.0	.0	.0	.0	.2	.2	.2	.3	.2	.7	.3	.2	.0	.0	.0	.1	.0	.1	.1		
3 *	.0	.0	.0	.0	.2	.0	.1	.1	.0	.0	.7	.4	.0	.0	.0	.1	.1	.1	.1		
4 *	.1	.1	.0	.0	.8	.8	.6	1.1	1.3	1.3	1.3	.8	.0	.0	.0	.1	.1	.3	.5		
5 *	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	
6 *	.0	.1	.2	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
7 *	.3	.6	.4	.6	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	
8 *	.4	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
9 *	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
10 *	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
12 *	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
13 *	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
14 *	.2	.7	.6	.6	.6	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	
15 *	.1	.3	.7	.7	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
16 *	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
17 *	.0	.0	.0	.0	.3	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	
18 *	.0	.0	.0	.0	.1	.3	.1	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	
19 *	.0	.0	.0	.0	.1	.2	.3	.1	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
22 *	.0	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.4	.4	.4	.2	.2	.2	.2	.2	.2	
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
24 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.4	.2	.0	.0	.0	.0	
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.2	.0	.0	.0	
26 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.3	.0	.0	
27 *	.1	.1	.2	.0	.0	.0	.1	.0	.0	.0	.0	.2	.2	.2	.3	.4	.3	.4	.0	.0	
28 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
29 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
33 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
34 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
35 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
36 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	

1

JOB: Brent Spence Bridge NB-AM S1altEam.dat
 DATE: 08/30/2010 TIME: 11:48:09.42

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24

LINK #	210	210	215	235
1 *	.1	.0	.0	.0
2 *	.1	.0	.0	.0
3 *	.1	.1	.0	.0
4 *	.4	.3	.2	.0
5 *	.3	.1	.1	.0
6 *	.3	.2	.1	.0
7 *	.0	.6	1.0	.2
8 *	.0	.0	.0	.5
9 *	.0	.0	.0	.2
10 *	.0	.0	.0	.0
11 *	.0	.0	.0	.0
12 *	.0	.0	.0	.0
13 *	.0	.0	.0	.1
14 *	.0	.2	.3	.2
15 *	.0	.1	.2	.1
16 *	.0	.0	.0	.0

17 * .1 .1 .0 .0
 18 * .0 .0 .0 .0
 19 * .0 .0 .0 .0
 20 * .0 .0 .0 .0
 21 * .1 .0 .0 .0
 22 * .0 .0 .0 .0
 23 * .0 .0 .0 .0
 24 * .0 .0 .0 .0
 25 * .0 .0 .0 .0
 26 * .1 .0 .0 .0
 27 * .0 .0 .0 .0
 28 * .3 .1 .0 .0
 29 * .0 .0 .0 .0
 30 * .0 .0 .0 .0
 31 * .0 .0 .0 .0
 32 * .0 .0 .0 .0
 33 * .0 .0 .0 .0
 34 * .0 .0 .0 .0
 35 * .0 .0 .0 .0
 36 * .0 .0 .0 .0

JOB: Brent Spence Bridge S1altEpm.dat RUN: Kyles Lane & Dixie Hwy
 DATE: 08/30/2010 TIME: 11:49:05.39

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	*	184.	20.	AG	760.	11.5	.0	44.0			
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	*	94.	22.	AG	760.	11.5	.0	44.0			
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	*	112.	23.	AG	760.	11.5	.0	44.0			
4. 03 Dixie NB Queue	* 264228.0	275888.0	263898.8	275071.9	*	880.	202.	AG	295.	100.0	.0	24.0	1.20	44.7	
5. 04 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	*	105.	22.	AG	450.	11.5	.0	44.0			
6. 05 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	*	62.	22.	AG	465.	11.5	.0	44.0			
7. 06 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	*	149.	22.	AG	1295.	11.5	.0	44.0			
8. 07 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	*	83.	34.	AG	1295.	11.5	.0	44.0			
9. 08 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	*	62.	40.	AG	1295.	11.5	.0	44.0			
10. 09 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	*	112.	48.	AG	1295.	11.5	.0	44.0			
11. 10 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	*	81.	228.	AG	1600.	11.5	.0	44.0			
12. 11 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	*	93.	218.	AG	1600.	11.5	.0	44.0			
13. 12 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	*	62.	209.	AG	1600.	11.5	.0	44.0			
14. 13 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	*	260.	202.	AG	1600.	11.5	.0	44.0			
15. 14 Dixie SB Queue	* 264276.0	276054.0	264343.8	276215.3	*	175.	23.	AG	157.	100.0	.0	24.0	.78	8.9	
16. 14 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	*	41.	203.	AG	505.	11.5	.0	40.0			
17. 15 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	*	144.	203.	AG	665.	11.5	.0	44.0			
18. 16 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	*	99.	201.	AG	1340.	11.5	.0	44.0			
19. 17 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	*	178.	200.	AG	1340.	11.5	.0	44.0			
20. 18 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	*	46.	74.	AG	310.	11.5	.0	32.0			
21. 19 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	*	72.	154.	AG	650.	11.5	.0	32.0			
22. 20 Kyles EB Depart	* 264284.0	275929.0	264483.0	275522.0	*	453.	154.	AG	960.	11.5	.0	44.0			
23. 21 Kyles WB Appr	* 264516.0	275540.0	264468.0	275639.0	*	110.	334.	AG	1240.	11.5	.0	56.0			
24. 22 Kyles WB Appr	* 264468.0	275639.0	264359.0	275852.0	*	239.	333.	AG	1240.	11.5	.0	56.0			
25. 23 Kyles WB Rt.	* 264359.0	275852.0	264347.0	275900.0	*	49.	346.	AG	830.	11.5	.0	32.0			
26. 24 Kyles WB Rt.	* 264347.0	275900.0	264300.0	276003.0	*	113.	335.	AG	830.	11.5	.0	32.0			
27. 25 Kyles WB Rt. Qu	* 264313.0	275975.0	265386.1	273582.4	*	2622.	156.	AG	114.	100.0	.0	12.0	1.37	133.2	
28. 25 Kyles WB Rt. @ D	* 264300.0	276003.0	264303.0	276071.0	*	68.	3.	AG	830.	11.5	.0	32.0			
29. 26 Kyles WB Appr	* 264359.0	275852.0	264296.0	275980.0	*	143.	334.	AG	30.	11.5	.0	32.0			
30. 28 WB Kyles L	* 264307.0	275957.0	264311.2	275948.5	*	10.	154.	AG	114.	100.0	.0	12.0	.04	.5	
31. 27 Kyles WB @ Dixie	* 264296.0	275980.0	264280.0	276013.0	*	37.	334.	AG	15.	11.5	.0	32.0			
32. 28 Kyles WB Lt.	* 264296.0	275980.0	264252.0	275994.0	*	46.	288.	AG	15.	11.5	.0	32.0			
33. 29 Kyles WB Lt.	* 264359.0	275852.0	264325.0	275892.0	*	53.	320.	AG	380.	11.5	.0	32.0			
34. 30 Kyles WB Lt.	* 264325.0	275892.0	264287.0	275965.0	*	82.	333.	AG	380.	11.5	.0	32.0			
35. 33 Kyles WB Lt. Que	* 264295.0	275951.0	264348.1	275842.7	*	121.	154.	AG	114.	100.0	.0	12.0	.74	6.1	
36. 31 Kyles WB Lt. @ D	* 264287.0	275965.0	264236.0	275956.0	*	52.	260.	AG	140.	11.5	.0	32.0			

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
	* LENGTH	TIME	LOSS	VOL	FLOW	RATE	EM	FAC
	* (SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)		TYPE	
4. 03 Dixie NB Queue	* 100	75	2.0	760	1511	73.30	1	3
15. 14 Dixie SB Queue	* 100	40	2.0	1600	1831	73.30	1	3
27. 25 Kyles WB Rt. Qu	* 100	58	2.0	830	1599	73.30	1	3
30. 28 WB Kyles L	* 100	58	2.0	30	1881	73.30	1	3
35. 33 Kyles WB Lt. Que	* 100	58	2.0	380	1357	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	X	Y	Z	*
1. R1 SB Mid	* 264384.0	276323.0	5.0	*	
2. R2 SB 164	* 264321.0	276211.0	5.0	*	
3. R3 SB 82	* 264290.0	276136.0	5.0	*	
4. R4 SB Corner	* 264262.0	276069.0	5.0	*	

5. R5 SB Corner	*	264230.0	275990.0	5.0	*
6. R6 SB 82	*	264193.0	275900.0	5.0	*
7. R7 SB 164	*	264151.0	275798.0	5.0	*
8. R8 SB Mid	*	264103.0	275678.0	5.0	*
9. R9 NB Mid	*	264155.0	275655.0	5.0	*
10. R10 NB 164	*	264184.0	275729.0	5.0	*
11. R11 NB 82	*	264215.0	275805.0	5.0	*
12. R12 NB Corner	*	264242.0	275872.0	5.0	*
13. R13 EB Corner	*	264272.0	275903.0	5.0	*
14. R14 EB 82	*	264340.0	275765.0	5.0	*
15. R15 EB 164	*	264378.0	275678.0	5.0	*
16. R16 EB Mid	*	264408.0	275600.0	5.0	*
17. R17 WB Mid	*	264455.0	275722.0	5.0	*
18. R18 WB 164	*	264399.0	275833.0	5.0	*
19. R19 WB 82	*	264362.0	275906.0	5.0	*
20. R20 WB Corner	*	264330.0	275971.0	5.0	*
21. R21 NB Corner	*	264319.0	276046.0	5.0	*
22. R22 NB 82	*	264343.0	276114.0	5.0	*
23. R23 NB 164	*	264376.0	276189.0	5.0	*
24. R24 NB Mid	*	264447.0	276280.0	5.0	*

1

JOB: Brent Spence Bridge S1altEpm.dat

RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	*	.1	.1	.2	.2	.2	.1	.2	.2	2.2	2.3	1.8	1.0	1.2	1.3	1.1	.9	.1	.1	.4	.9
5.	*	.1	.3	.3	.4	.4	.2	.3	.3	2.3	2.2	1.8	1.1	1.3	1.3	1.0	.9	.1	.0	.3	.6
10.	*	.1	.3	.6	.5	.5	.4	.5	.5	2.2	2.0	1.8	1.1	1.4	1.3	1.0	.9	.1	.0	.1	.7
15.	*	.2	.6	.7	.9	.9	.6	.5	.9	2.1	1.8	1.7	1.1	1.5	1.1	.9	.9	.1	.0	.0	.5
20.	*	.2	.7	1.2	1.3	1.0	.7	1.0	1.2	1.7	1.6	1.4	1.1	1.3	1.0	.9	.9	.1	.0	.0	.3
25.	*	.4	.9	1.4	1.8	1.3	.9	1.3	1.5	1.3	1.3	1.1	1.1	1.2	.9	.9	.7	.1	.0	.0	.0
30.	*	.5	1.2	1.8	2.0	1.5	1.0	1.3	1.8	1.0	.9	.7	1.0	1.1	.8	.8	.7	.0	.0	.0	.0
35.	*	.7	1.4	2.1	2.2	1.7	1.1	1.4	1.9	.7	.7	.8	.8	.9	.8	.8	.7	.0	.0	.0	.0
40.	*	.8	1.6	2.4	2.4	1.5	1.1	1.3	1.9	.4	.5	.6	.6	.9	.8	.7	.6	.0	.0	.0	.0
45.	*	.9	1.7	2.3	2.1	1.5	.8	1.6	1.9	.5	.4	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
50.	*	1.0	1.7	2.2	2.0	1.3	.8	1.7	1.9	.4	.3	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
55.	*	1.2	1.6	1.9	2.0	1.2	.8	1.8	1.9	.4	.4	.4	.7	1.0	.8	.8	.6	.0	.0	.0	.0
60.	*	1.2	1.6	1.9	1.8	1.1	.7	1.9	1.9	.4	.3	.3	.6	1.0	.8	.8	.7	.0	.0	.0	.0
65.	*	1.3	1.6	1.8	1.8	1.0	1.0	1.9	1.9	.4	.3	.4	.5	1.0	.8	.8	.7	.0	.0	.0	.0
70.	*	1.4	1.4	1.7	1.6	1.0	1.0	1.7	1.8	.3	.3	.4	.5	.9	.8	.8	.7	.0	.0	.0	.0
75.	*	1.3	1.3	1.6	1.6	.9	1.0	1.8	1.8	.3	.3	.3	.6	.9	.8	.7	.6	.0	.0	.0	.0
80.	*	1.2	1.4	1.6	1.7	.8	.9	1.7	1.7	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
85.	*	1.1	1.4	1.5	1.5	.8	1.0	1.7	1.6	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
90.	*	1.1	1.4	1.5	1.5	.7	.9	1.6	1.6	.3	.3	.3	.6	1.0	.8	.7	.7	.0	.0	.0	.0
95.	*	1.1	1.4	1.5	1.4	.9	1.0	1.6	1.6	.3	.3	.4	.6	1.0	.8	.8	.7	.0	.0	.0	.0
100.	*	1.0	1.5	1.5	1.5	.8	1.2	1.6	1.5	.2	.3	.4	.6	1.0	.8	.9	.7	.1	.0	.0	.0
105.	*	1.0	1.5	1.5	1.5	.8	1.3	1.6	1.5	.2	.3	.5	.5	1.1	.9	.8	.7	.1	.1	.0	.0
110.	*	.9	1.5	1.5	1.4	.8	1.3	1.6	1.5	.2	.4	.5	.5	1.0	.9	.9	.7	.1	.1	.0	.1
115.	*	.9	1.5	1.5	1.3	.9	1.3	1.6	1.4	.1	.3	.4	.5	1.2	1.0	.9	.8	.1	.1	.0	.1
120.	*	.9	1.5	1.5	1.3	1.0	1.4	1.6	1.4	.1	.2	.4	.5	1.3	1.0	1.0	.7	.1	.1	.0	.1
125.	*	.9	1.5	1.5	1.3	1.2	1.5	1.5	1.4	.1	.2	.3	.6	1.1	1.1	1.0	.6	.1	.1	.0	.1
130.	*	.9	1.5	1.5	1.3	1.3	1.5	1.5	1.4	.1	.1	.3	.6	1.1	1.2	1.0	.6	.1	.1	.0	.1
135.	*	.9	1.5	1.5	1.4	1.3	1.5	1.4	1.4	.1	.1	.2	.5	1.2	1.1	.9	.6	.1	.2	.2	.2
140.	*	1.0	1.5	1.5	1.4	1.3	1.4	1.4	1.4	.1	.1	.2	.4	1.1	1.1	.8	.4	.4	.3	.2	.4
145.	*	.9	1.6	1.7	1.7	1.2	1.4	1.6	1.6	.1	.1	.2	.4	1.0	1.0	.7	.4	.4	.5	.5	.5
150.	*	1.0	1.7	1.9	1.7	1.2	1.4	1.6	1.5	.0	.1	.1	.2	1.0	.9	.7	.3	.6	.9	.8	1.0
155.	*	1.1	1.8	2.2	1.8	1.0	1.3	1.5	1.5	.1	.0	.1	.2	.8	.8	.5	.2	.9	1.0	1.0	1.2
160.	*	1.1	2.1	2.3	1.9	1.1	1.2	1.7	1.7	.1	.0	.0	.2	.6	.5	.3	.2	1.0	1.2	1.4	1.5
165.	*	1.3	2.2	2.4	2.0	.8	1.4	1.9	1.7	.1	.0	.0	.1	.4	.4	.2	.1	1.1	1.3	1.3	1.5
170.	*	1.3	2.3	2.6	1.9	.9	1.5	1.9	1.7	.1	.0	.1	.1	.2	.2	.1	.0	1.2	1.4	1.4	1.6
175.	*	1.7	2.3	2.5	1.6	.9	1.5	2.0	1.7	.2	.2	.2	.1	.1	.1	.0	1.2	1.2	1.4	1.6	
180.	*	1.6	2.4	2.3	1.4	.9	1.8	2.1	1.7	.2	.2	.2	.2	.1	.1	.0	1.1	1.2	1.4	1.8	
185.	*	1.9	2.5	2.1	1.5	1.1	1.8	2.1	1.8	.4	.4	.4	.4	.2	.1	.0	1.1	1.3	1.4	1.7	
190.	*	2.0	2.3	2.0	1.5	1.2	1.8	2.0	1.6	.6	.8	.9	.8	.2	.1	.0	1.1	1.1	1.4	1.5	
195.	*	2.0	2.0	1.9	1.6	1.2	1.7	1.8	1.4	1.1	1.2	1.1	1.3	.4	.0	.0	1.0	1.0	1.4	1.5	
200.	*	2.0	1.8	1.5	1.5	1.2	1.5	1.5	1.3	1.4	1.6	1.5	1.7	.9	.1	.0	1.0	1.0	1.4	1.6	
205.	*	1.8	1.4	1.2	1.1	1.1	1.3	1.4	.9	1.8	2.0	2.0	2.0	1.2	.1	.0	1.0	1.1	1.4	1.8	

1

JOB: Brent Spence Bridge S1altEpm.dat

RUN: Kyles Lane & Dixie Hwy

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

210.	*	1.5	1.1	.9	.7	.7	.7	1.0	.6	2.0	2.2	2.1	2.2	1.4	.2	.1	.0	.9	1.1	1.4	2.2
215.	*	1.3	.7	.6	.4	.4	.6	.6	.4	2.1	2.4	2.4	2.4	1.5	.2	.1	.1	.9	1.2	1.5	2.1
220.	*	.8	.4	.4	.3	.2	.3	.4	.3	2.3	2.4	2.5	2.4	1.5	.3	.2	.1	.9	1.1	1.6	2.0
225.	*	.6	.2	.2	.2	.0	.1	.2	.1	2.2	2.3	2.4	2.3	1.4	.4	.2	.1	1.0	1.3	1.8	1.9
230.	*	.4	.2	.2	.1	.0	.1	.2	.1	2.1	2.1	2.3	2.2	1.2	.5	.2	.2	1.0	1.3	1.8	1.7
235.	*	.3	.1	.1	.1	.0	.1	.1	.1	2.0	2.0	2.1	2.1	1.2	.5	.2	.2	1.1	1.4	1.7	1.6
240.	*	.1	.1	.1	.1	.0	.1	.1	.1	2.1	2.0	2.0	1.9	1.1	.5	.2	.2	1.1	1.4	1.6	1.5
245.	*	.1	.1	.1	.1	.0	.0	.1	.1	1.9	1.8	1.8	1.8	1.0	.5	.3	.2	1.1	1.5	1.7	1.5

250.	*	.1	.1	.1	.1	.0	.0	.1	.1	1.8	1.9	1.8	1.7	.9	.5	.3	.2	1.2	1.5	1.9	1.3
255.	*	.1	.1	.1	.1	.0	.0	.1	.1	1.7	1.8	1.7	1.5	.8	.6	.4	.2	1.1	1.3	1.5	1.0
260.	*	.1	.1	.1	.1	.0	.0	.1	.1	1.7	1.8	1.7	1.5	.6	.6	.4	.2	1.1	1.3	1.5	1.0
265.	*	.1	.1	.1	.1	.0	.0	.1	.0	1.6	1.7	1.7	1.5	.5	.6	.4	.3	1.1	1.2	1.5	.8
270.	*	.1	.0	.0	.0	.0	.0	.1	.0	1.6	1.6	1.5	1.4	.5	.5	.4	.3	1.2	1.3	1.4	.8
275.	*	.1	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.6	.5	.3	.4	1.2	1.3	1.4	.9
280.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.5	.5	.3	.4	1.2	1.4	1.2	1.0
285.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.6	.5	.4	.3	1.3	1.4	1.3	.9
290.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.4	.5	.5	.3	.3	1.2	1.5	1.3	.9
295.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.5	.4	.3	.3	1.2	1.5	1.3	.8
300.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.3	.5	.5	.3	.3	1.2	1.2	1.4	.8
305.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.4	1.2	.4	.5	.3	.3	1.2	1.2	1.3	1.0
310.	*	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.4	1.1	.3	.5	.3	.3	1.2	1.2	1.3	1.1
315.	*	.0	.0	.0	.0	.0	.0	.1	.0	1.6	1.6	1.5	1.0	.3	.5	.3	.2	1.2	1.2	1.2	.9
320.	*	.0	.1	.1	.1	.0	.0	.1	.1	1.6	1.7	1.5	1.0	.3	.5	.2	.2	1.2	1.1	1.0	.9
325.	*	.0	.1	.1	.1	.0	.0	.1	.1	1.7	1.7	1.5	.9	.6	.6	.3	.2	1.2	1.0	1.0	1.0
330.	*	.0	.1	.1	.1	.0	.0	.1	.1	1.7	1.7	1.5	.8	.7	.4	.4	.3	1.0	.9	1.0	1.1
335.	*	.1	.1	.1	.1	.0	.0	.1	.1	1.9	1.8	1.6	.8	.8	.6	.6	.5	.8	.9	1.0	1.2
340.	*	.1	.1	.1	.1	.0	.0	.1	.1	2.0	1.9	1.6	.7	.7	.7	.9	.6	.5	.8	.9	1.1
345.	*	.1	.1	.1	.1	.0	.1	.1	.1	2.1	2.0	1.6	.9	.9	1.0	.9	.8	.4	.6	.8	1.1
350.	*	.1	.1	.1	.1	.1	.1	.1	.1	2.2	2.1	1.7	.8	1.0	1.1	1.0	.8	.3	.4	.6	.9
355.	*	.1	.1	.2	.2	.1	.1	.2	.1	2.3	2.2	1.8	.8	1.1	1.3	.9	1.0	.1	.4	.5	.9
360.	*	.1	.1	.2	.2	.2	.1	.2	.2	2.2	2.3	1.8	1.0	1.2	1.3	1.1	.9	.1	.1	.4	.9

MAX * 2.0 2.5 2.6 2.4 1.7 1.8 2.1 1.9 2.3 2.4 2.5 2.4 1.5 1.3 1.1 1.0 1.3 1.5 1.9 2.2
DEGR * 190 185 170 40 35 180 180 35 5 215 220 215 15 0 0 355 285 295 250 210

1

JOB: Brent Spence Bridge S1altEpm.dat

PAGE 5
RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24

0.	*	1.5	1.5	1.2	.9
5.	*	1.6	1.5	1.2	.9
10.	*	1.5	1.3	1.2	.8
15.	*	1.4	1.4	1.3	.8
20.	*	1.0	1.4	1.1	.7
25.	*	.7	1.1	1.1	.7
30.	*	.4	.8	.7	.5
35.	*	.2	.4	.7	.5
40.	*	.1	.4	.5	.4
45.	*	.0	.1	.3	.2
50.	*	.0	.1	.2	.1
55.	*	.0	.1	.1	.1
60.	*	.0	.1	.0	.0
65.	*	.0	.1	.0	.0
70.	*	.0	.1	.0	.0
75.	*	.0	.1	.0	.0
80.	*	.0	.0	.0	.0
85.	*	.0	.0	.0	.0
90.	*	.0	.0	.0	.0
95.	*	.0	.0	.0	.0
100.	*	.0	.0	.0	.0
105.	*	.0	.0	.0	.0
110.	*	.0	.0	.0	.0
115.	*	.0	.0	.0	.0
120.	*	.0	.0	.0	.0
125.	*	.0	.0	.0	.0
130.	*	.0	.0	.0	.0
135.	*	.0	.0	.0	.0
140.	*	.0	.0	.0	.0
145.	*	.2	.0	.0	.0
150.	*	.3	.2	.0	.0
155.	*	.5	.3	.2	.0
160.	*	.6	.4	.2	.1
165.	*	.9	.5	.3	.1
170.	*	1.0	.5	.4	.1
175.	*	.9	.6	.4	.1
180.	*	1.0	.6	.4	.3
185.	*	.9	.8	.6	.3
190.	*	.9	.9	.6	.4
195.	*	1.3	1.0	.8	.3
200.	*	1.4	1.1	1.0	.5
205.	*	1.6	1.2	1.3	.6

1

JOB: Brent Spence Bridge S1altEpm.dat

PAGE 6
RUN: Kyles Lane & Dixie Hwy

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24

210.	*	1.6	1.5	1.5	.7
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215. * 1.5 1.4 1.5 .8
 220. * 1.3 1.5 1.6 1.0
 225. * 1.1 1.5 1.7 1.2
 230. * 1.2 1.4 1.7 1.2
 235. * 1.1 1.6 1.6 1.0
 240. * 1.0 1.5 1.6 1.0
 245. * .9 1.4 1.5 1.1
 250. * 1.0 1.3 1.5 .9
 255. * 1.0 1.3 1.3 1.0
 260. * 1.0 1.3 1.3 1.0
 265. * 1.1 1.3 1.3 .8
 270. * 1.1 1.3 1.3 .9
 275. * 1.1 1.3 1.3 .9
 280. * 1.1 1.3 1.3 .9
 285. * 1.2 1.3 1.3 .9
 290. * 1.2 1.3 1.3 .8
 295. * 1.3 1.3 1.3 .7
 300. * 1.3 1.3 1.3 .8
 305. * 1.4 1.3 1.1 .8
 310. * 1.3 1.3 1.1 .9
 315. * 1.3 1.3 1.1 .9
 320. * 1.4 1.3 1.1 .8
 325. * 1.4 1.3 1.2 .8
 330. * 1.4 1.4 1.0 .8
 335. * 1.4 1.5 1.0 .8
 340. * 1.5 1.4 1.1 .9
 345. * 1.6 1.4 1.1 .9
 350. * 1.6 1.6 1.1 .8
 355. * 1.6 1.7 1.2 .9
 360. * 1.5 1.5 1.2 .9

MAX * 1.6 1.7 1.7 1.2
 DEGR. * 205 355 225 225

THE HIGHEST CONCENTRATION IS 2.60 PPM AT 170 DEGREES FROM REC3.
 THE 2ND HIGHEST CONCENTRATION IS 2.50 PPM AT 220 DEGREES FROM REC11.
 THE 3RD HIGHEST CONCENTRATION IS 2.50 PPM AT 185 DEGREES FROM REC2 .

1

JOB: Brent Spence Bridge S1altEpm.dat
 DATE: 08/30/2010 TIME: 11:49:05.39

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

LINK #	* 190	185	170	40	35	180	180	35	5	215	220	215	15	0	0	355	285	295	250	210
1 *	.0	.0	.0	.0	.0	.2	.1	.3	.4	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
2 *	.0	.0	.0	.0	.1	.1	.1	.1	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3 *	.0	.0	.0	.0	.2	.0	.1	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1
4 *	.1	.1	.0	.0	.9	.9	.6	1.3	1.5	1.5	1.5	.0	.0	.0	.2	.1	.3	.5	.5	.5
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.2	.4	.3	.4	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
8 *	.3	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.5	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.4	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.3	1.0	.9	1.0	.9	.0	.1	.1	.0	.0	.3	.1	.1	.1	.0	.0	.0	.0	.0	.0
15 *	.1	.7	.6	.7	.3	.0	.0	.0	.0	.0	.1	.1	.0	.0	.3	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.3	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1
18 *	.0	.0	.0	.0	.2	.6	.2	.2	.0	.3	.2	.0	.0	.0	.1	.0	.1	.1	.1	.1
19 *	.0	.0	.0	.0	.1	.3	.6	.2	.4	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.5	.5	.4	.2	.2	.2	.2	.2	.2
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.3	.3	.5	.4	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.2	.0	.0	.0	.0
26 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.4	.4	.4	.4
27 *	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.3	.3	.3	.4	.4	.4	.4
28 *	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
29 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
34 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0
35 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.2	.2	.2	.2	.2	.2	.2
36 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge S1altEpm.dat
 DATE: 08/30/2010 TIME: 11:49:05.39

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)

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* ANGLE (DEGREES)
* REC21 REC22 REC23 REC24
LINK # * 205 355 225 225
-----*
1 * .0 .0 .0 .0
2 * .0 .0 .0 .0
3 * .1 .0 .0 .0
4 * .4 .0 .1 .1
5 * .1 .0 .0 .0
6 * .1 .0 .0 .0
7 * .0 .7 .7 .2
8 * .0 .1 .0 .3
9 * .0 .0 .0 .0
10 * .0 .0 .0 .0
11 * .0 .0 .0 .0
12 * .0 .0 .0 .0
13 * .0 .1 .0 .1
14 * .0 .5 .6 .3
15 * .0 .3 .3 .2
16 * .0 .0 .0 .0
17 * .1 .0 .0 .0
18 * .1 .0 .0 .0
19 * .1 .0 .0 .0
20 * .0 .0 .0 .0
21 * .1 .0 .0 .0
22 * .1 .0 .0 .0
23 * .0 .0 .0 .0
24 * .0 .0 .0 .0
25 * .0 .0 .0 .0
26 * .1 .0 .0 .0
27 * .0 .0 .0 .0
28 * .3 .0 .0 .0
29 * .0 .0 .0 .0
30 * .0 .0 .0 .0
31 * .0 .0 .0 .0
32 * .0 .0 .0 .0
33 * .0 .0 .0 .0
34 * .0 .0 .0 .0
35 * .0 .0 .0 .0
36 * .0 .0 .0 .0

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JOB: Brent Spence Bridge S1altlam.dat RUN: Kyles Lane & Dixie Hwy
DATE: 08/30/2010 TIME: 11:45:54.86

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/M)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	*	184.	20.	AG	1520.	11.5	.0	.44.0		
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	*	94.	22.	AG	1520.	11.5	.0	.44.0		
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	*	112.	23.	AG	1520.	11.5	.0	.44.0		
4. 03 Dixie NB Queue	* 264228.0	275888.0	263366.3	273751.5	*	2304.	202.	AG	240.	100.0	.0	.24.0	1.35	117.0
5. 04 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	*	105.	22.	AG	1240.	11.5	.0	.44.0		
6. 05 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	*	62.	22.	AG	1245.	11.5	.0	.44.0		
7. 06 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	*	149.	22.	AG	1955.	11.5	.0	.44.0		
8. 07 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	*	83.	34.	AG	1955.	11.5	.0	.44.0		
9. 08 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	*	62.	40.	AG	1955.	11.5	.0	.44.0		
10. 09 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	*	112.	48.	AG	1955.	11.5	.0	.44.0		
11. 10 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	*	81.	228.	AG	1020.	11.5	.0	.44.0		
12. 11 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	*	93.	218.	AG	1020.	11.5	.0	.44.0		
13. 12 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	*	62.	209.	AG	1020.	11.5	.0	.44.0		
14. 13 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	*	260.	202.	AG	1020.	11.5	.0	.44.0		
15. 14 Dixie SB Queue	* 264276.0	276054.0	264319.2	276156.8	*	112.	23.	AG	175.	100.0	.0	.24.0	.55	5.7
16. 14 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	*	41.	203.	AG	505.	11.5	.0	.40.0		
17. 15 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	*	144.	203.	AG	665.	11.5	.0	.44.0		
18. 16 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	*	99.	201.	AG	665.	11.5	.0	.44.0		
19. 17 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	*	178.	200.	AG	665.	11.5	.0	.44.0		
20. 18 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	*	46.	74.	AG	280.	11.5	.0	.32.0		
21. 19 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	*	72.	154.	AG	520.	11.5	.0	.32.0		
22. 20 Kyles EB Depart	* 264284.0	275929.0	264483.0	275522.0	*	453.	154.	AG	800.	11.5	.0	.44.0		
23. 21 Kyles WB Appr	* 264516.0	275540.0	264468.0	275639.0	*	110.	334.	AG	880.	11.5	.0	.56.0		
24. 22 Kyles WB Appr	* 264468.0	275639.0	264359.0	275852.0	*	239.	333.	AG	880.	11.5	.0	.56.0		
25. 23 Kyles WB Rt.	* 264359.0	275852.0	264347.0	275900.0	*	49.	346.	AG	710.	11.5	.0	.32.0		
26. 24 Kyles WB Rt.	* 264347.0	275900.0	264300.0	276003.0	*	113.	335.	AG	710.	11.5	.0	.32.0		
27. 25 Kyles WB Rt. Qu*	264313.0	275975.0	265401.9	273547.2	*	2661.	156.	AG	129.	100.0	.0	.12.0	1.48	135.2
28. 25 Kyles WB Rt. @ D*	264300.0	276003.0	264303.0	276071.0	*	68.	3.	AG	710.	11.5	.0	.32.0		
29. 26 Kyles WB Appr	* 264359.0	275852.0	264296.0	275980.0	*	143.	334.	AG	10.	11.5	.0	.32.0		
30. 28 WB Kyles L*	264307.0	275957.0	264308.4	275954.1	*	3.	154.	AG	129.	100.0	.0	.12.0	.02	.2
31. 27 Kyles WB @ Dixie	* 264296.0	275980.0	264280.0	276013.0	*	37.	334.	AG	5.	11.5	.0	.32.0		
32. 28 Kyles WB Lt.	* 264296.0	275980.0	264252.0	275994.0	*	46.	288.	AG	5.	11.5	.0	.32.0		
33. 29 Kyles WB Lt.	* 264359.0	275852.0	264325.0	275892.0	*	53.	320.	AG	160.	11.5	.0	.32.0		
34. 30 Kyles WB Lt.	* 264325.0	275892.0	264287.0	275965.0	*	82.	333.	AG	160.	11.5	.0	.32.0		
35. 33 Kyles WB Lt. Que*	264295.0	275951.0	264317.7	275904.7	*	52.	154.	AG	129.	100.0	.0	.12.0	.40	2.6
36. 31 Kyles WB Lt. @ D*	264287.0	275965.0	264236.0	275956.0	*	52.	260.	AG	160.	11.5	.0	.32.0		

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* (SEC)	TIME	LOST	VOL	FLOW	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
4. 03 Dixie NB Queue	* 90	55	2.0	1520	1641	73.30	1	3
15. 14 Dixie SB Queue	* 90	40	2.0	1020	1829	73.30	1	3
27. 25 Kyles WB Rt. Qu*	90	59	2.0	710	1599	73.30	1	3
30. 28 WB Kyles L*	90	59	2.0	10	1881	73.30	1	3
35. 33 Kyles WB Lt. Que*	90	59	2.0	160	1343	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	* *
1. R1 SB Mid	* 264384.0	276323.0	5.0	*	
2. R2 SB 164	* 264321.0	276211.0	5.0	*	
3. R3 SB 82	* 264290.0	276136.0	5.0	*	
4. R4 SB Corner	* 264262.0	276069.0	5.0	*	
5. R5 SB Corner	* 264230.0	275990.0	5.0	*	
6. R6 SB 82	* 264193.0	275900.0	5.0	*	
7. R7 SB 164	* 264151.0	275798.0	5.0	*	
8. R8 SB Mid	* 264103.0	275678.0	5.0	*	
9. R9 NB Mid	* 264155.0	275655.0	5.0	*	
10. R10 NB 164	* 264184.0	275729.0	5.0	*	
11. R11 NB 82	* 264215.0	275805.0	5.0	*	
12. R12 NB Corner	* 264242.0	275872.0	5.0	*	
13. R13 EB Corner	* 264272.0	275903.0	5.0	*	
14. R14 EB 82	* 264340.0	275765.0	5.0	*	
15. R15 EB 164	* 264378.0	275678.0	5.0	*	
16. R16 EB Mid	* 264408.0	275600.0	5.0	*	
17. R17 WB Mid	* 264455.0	275722.0	5.0	*	
18. R18 WB 164	* 264399.0	275833.0	5.0	*	
19. R19 WB 82	* 264362.0	275906.0	5.0	*	
20. R20 WB Corner	* 264330.0	275971.0	5.0	*	
21. R21 NB Corner	* 264319.0	276046.0	5.0	*	
22. R22 NB 82	* 264343.0	276114.0	5.0	*	
23. R23 NB 164	* 264376.0	276189.0	5.0	*	
24. R24 NB Mid	* 264447.0	276280.0	5.0	*	

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JOB: Brent Spence Bridge S1altlam.dat

RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	.1	.1	.1	.1	.1	.1	.1	2.3	2.2	2.1	1.4	1.3	1.1	.9	.8	.1	.1	.5	1.0	
5. *	.1	.1	.2	.3	.3	.2	.2	.1	2.5	2.3	2.1	1.5	1.4	1.1	.8	.7	.1	.0	.3	.7
10. *	.1	.3	.2	.5	.5	.3	.2	.3	2.5	2.3	2.0	1.6	1.5	.9	.8	.7	.0	.0	.2	.6
15. *	.1	.3	.5	.7	.6	.6	.6	.6	2.3	2.1	1.7	1.5	1.6	.9	.8	.7	.0	.0	.0	.5
20. *	.1	.4	.7	1.1	1.0	.7	.9	1.0	2.1	1.8	1.6	1.4	1.4	.8	.7	.7	.0	.0	.0	.3
25. *	.2	.8	1.2	1.4	1.2	.9	1.1	1.3	1.4	1.6	1.2	1.4	1.1	.7	.7	.7	.0	.0	.0	.2
30. *	.3	.9	1.4	1.8	1.3	1.2	1.3	1.6	1.0	1.2	1.2	1.1	1.0	.7	.7	.7	.0	.0	.0	.0
35. *	.4	1.1	1.6	2.0	1.8	1.1	1.3	1.5	.9	.8	.8	.9	.7	.7	.7	.7	.0	.0	.0	.0
40. *	.5	1.2	1.9	2.2	1.6	1.3	1.6	1.6	.6	.6	.6	.7	.6	.7	.7	.7	.0	.0	.0	.0
45. *	.7	1.5	1.9	2.1	1.4	1.1	1.4	1.7	.5	.5	.7	.7	.7	.7	.7	.7	.0	.0	.0	.0
50. *	.8	1.4	1.9	2.0	1.4	1.1	1.7	1.8	.3	.3	.3	.5	.7	.7	.7	.6	.0	.0	.0	.0
55. *	.9	1.5	1.8	1.9	1.2	1.0	1.7	1.7	.4	.3	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
60. *	1.2	1.4	1.7	1.9	1.1	1.1	1.6	1.6	.4	.4	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
65. *	1.1	1.3	1.8	1.8	.9	1.1	1.7	1.7	.4	.4	.3	.6	.7	.7	.7	.6	.0	.0	.0	.0
70. *	1.1	1.2	1.7	1.7	1.0	1.2	1.8	1.8	.4	.4	.4	.6	.7	.7	.7	.6	.0	.0	.0	.0
75. *	1.2	1.1	1.5	1.5	1.1	1.2	1.4	1.6	.4	.4	.4	.4	.7	.7	.7	.6	.0	.0	.0	.0
80. *	1.2	1.2	1.5	1.6	1.0	1.1	1.6	1.6	.4	.4	.4	.5	.6	.7	.7	.6	.0	.0	.0	.0
85. *	1.0	1.0	1.5	1.6	.9	1.2	1.6	1.5	.4	.4	.3	.5	.7	.7	.7	.7	.0	.0	.0	.0
90. *	1.0	1.1	1.5	1.6	.7	1.1	1.6	1.5	.2	.3	.3	.4	.8	.7	.7	.7	.0	.0	.0	.0
95. *	1.0	1.0	1.5	1.5	1.0	1.0	1.6	1.4	.2	.3	.3	.5	.8	.7	.7	.7	.0	.0	.0	.0
100. *	.9	1.0	1.5	1.4	1.1	1.1	1.5	1.4	.2	.3	.3	.4	.6	.7	.7	.7	.0	.0	.0	.0
105. *	1.0	1.1	1.5	1.5	1.0	1.3	1.6	1.5	.2	.3	.3	.4	.7	.8	.8	.7	.0	.0	.0	.0
110. *	1.0	1.0	1.6	1.6	1.0	1.4	1.6	1.4	.1	.2	.3	.4	.8	.8	.8	.7	.0	.0	.0	.0
115. *	.9	1.0	1.6	1.5	1.1	1.5	1.6	1.4	.1	.2	.3	.4	.8	.8	.8	.6	.0	.0	.0	.0
120. *	.9	1.0	1.6	1.5	1.3	1.6	1.5	1.3	.1	.2	.3	.4	.8	.8	.8	.6	.0	.1	.0	.1
125. *	.9	1.0	1.5	1.4	1.3	1.6	1.5	1.3	.1	.2	.3	.4	.8	.8	.8	.6	.1	.1	.0	.1
130. *	.9	1.0	1.5	1.4	1.4	1.7	1.5	1.3	.1	.1	.2	.5	.9	1.0	.8	.6	.1	.1	.0	.1
135. *	1.0	1.0	1.6	1.5	1.5	1.6	1.4	1.4	.2	.1	.2	.5	.9	1.0	.7	.4	.1	.1	.2	.2
140. *	.9	1.0	1.6	1.6	1.4	1.6	1.4	1.4	.2	.1	.3	.6	.9	.9	.7	.4	.2	.3	.2	.4
145. *	1.0	1.0	1.7	1.6	1.3	1.5	1.4	1.4	.2	.1	.2	.5	.8	.9	.7	.4	.4	.4	.4	.6
150. *	.9	1.2	1.8	1.7	1.3	1.5	1.5	1.3	.2	.1	.2	.3	.8	.7	.5	.3	.5	.6	.7	.8
155. *	1.2	1.3	2.3	1.8	1.4	1.5	1.6	1.4	.1	.1	.2	.3	.7	.6	.4	.3	.7	1.0	.8	1.1
160. *	1.1	1.4	2.3	2.0	1.3	1.6	1.4	1.4	.1	.0	.1	.2	.4	.4	.3	.1	.9	1.1	1.1	1.3
165. *	1.2	1.6	2.4	1.9	1.1	1.5	1.5	1.4	.1	.0	.1	.1	.3	.3	.2	.1	.9	1.2	1.3	1.5
170. *	1.2	1.7	2.6	1.4	1.2	1.6	1.6	1.5	.2	.1	.1	.1	.2	.1	.1	.0	.9	1.2	1.2	1.4
175. *	1.3	1.7	2.5	1.6	1.1	1.8	1.7	1.5	.2	.2	.2	.2	.1	.1	.0	.0	1.0	1.2	1.1	1.4
180. *	1.5	1.9	2.3	1.4	1.2	1.7	1.7	1.5	.4	.3	.3	.3	.1	.1	.0	.0	1.1	1.0	1.2	1.4
185. *	1.5	2.1	2.2	1.5	1.5	1.8	1.9	1.5	.6	.5	.5	.6	.2	.1	.0	.0	1.0	1.0	1.2	1.2
190. *	1.7	2.0	2.1	1.6	1.5	1.9	1.7	1.3	.9	.9	.8	.9	.2	.0	.0	.0	1.0	1.0	1.0	1.3

195. * 1.6 1.9 1.9 1.4 1.4 1.7 1.6 1.2 1.3 1.4 1.3 1.4 .7 .1 .0 .0 .9 1.1 1.1 1.4
 200. * 1.6 1.7 1.7 1.3 1.3 1.4 1.4 1.0 1.7 1.7 1.8 1.9 .9 .1 .1 .0 .9 1.1 1.2 1.5
 205. * 1.4 1.3 1.2 1.1 1.1 1.2 1.0 .8 2.0 2.1 2.1 2.3 1.1 .2 .1 .1 .9 1.1 1.3 1.8

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JOB: Brent Spence Bridge S1altlam.dat

RUN: Kyles Lane & Dixie Hwy

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

ANGLE	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	1.2	.9	.8	.9	.7	.8	.7	.5	2.1	2.5	2.4	2.6	1.6	.3	.2	.1	.9	1.0	1.3	1.9
215.	.9	.5	.5	.3	.4	.5	.6	.3	2.1	2.5	2.5	2.7	1.7	.3	.2	.2	1.0	1.0	1.3	1.8
220.	.5	.3	.3	.2	.2	.2	.2	2.3	2.5	2.3	2.5	1.7	.4	.2	.2	1.0	1.2	1.3	1.9	
225.	.4	.2	.1	.1	.0	.1	.1	.1	2.1	2.3	2.3	2.3	1.6	.4	.2	.2	1.0	1.1	1.2	1.8
230.	.2	.1	.1	.1	.0	.1	.1	.1	2.0	2.2	2.2	2.2	1.4	.4	.2	.2	1.0	1.1	1.4	1.8
235.	.1	.1	.1	.1	.0	.1	.1	.0	2.0	2.0	2.2	2.2	1.2	.4	.2	.2	1.0	1.1	1.4	1.6
240.	.1	.1	.1	.1	.0	.1	.1	.0	1.9	2.0	2.0	2.1	1.1	.4	.3	.2	1.0	1.2	1.3	1.5
245.	.1	.1	.1	.1	.0	.0	.0	.0	1.8	1.9	1.8	1.8	1.1	.4	.3	.2	1.1	1.2	1.4	1.4
250.	.1	.1	.1	.1	.0	.0	.0	.0	1.8	1.8	1.8	1.8	1.0	.5	.3	.2	1.1	1.2	1.4	1.3
255.	.0	.1	.1	.1	.0	.0	.0	.0	1.7	1.7	1.7	1.7	.9	.4	.3	.2	1.1	1.1	1.3	1.2
260.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.9	.4	.3	.2	1.0	1.2	1.3	1.1
265.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.6	1.6	.7	.4	.4	.2	1.0	1.2	1.3	1.0
270.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.6	.8	.4	.3	.2	1.1	1.2	1.2	1.1
275.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.7	1.6	1.6	.8	.4	.3	.2	1.0	1.1	1.4	1.1
280.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.5	.7	.5	.4	.2	1.1	1.1	1.2	1.1
285.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.5	.7	.4	.4	.2	1.1	1.2	1.3	1.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.7	1.5	.8	.4	.3	.2	1.2	1.2	1.3	.9
295.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.5	.7	.4	.3	.2	1.1	1.3	1.3	.7
300.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.4	.8	.4	.3	.3	1.1	1.1	1.3	.9
305.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.5	1.4	.6	.6	.4	.2	1.1	.9	1.3	1.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.3	1.3	.6	.6	.3	.2	1.1	1.1	1.2	.9
315.	.0	.0	.0	.0	.0	.0	.0	.0	1.5	1.6	1.6	1.2	.6	.4	.3	.3	1.0	1.1	1.1	1.0
320.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.2	.6	.4	.3	.3	.9	1.2	1.0	1.0
325.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.1	.7	.6	.4	.3	.8	.9	1.1	1.0
330.	.0	.0	.1	.1	.0	.0	.0	.0	1.7	1.7	1.7	1.2	.9	.5	.4	.4	.9	1.1	1.2	1.0
335.	.0	.0	.1	.1	.0	.0	.0	.0	1.8	1.8	1.8	1.1	1.0	.6	.5	.4	.7	.8	1.0	1.1
340.	.0	.0	.1	.1	.0	.0	.0	.0	2.0	1.8	1.8	1.1	.9	.6	.7	.5	.5	.6	.8	1.2
345.	.0	.1	.1	.1	.0	.1	.1	.0	2.1	2.1	1.9	1.1	.9	.9	.8	.5	.5	.6	.8	1.1
350.	.1	.1	.1	.1	.0	.1	.1	.1	2.2	2.2	1.9	1.2	1.3	1.1	.8	.7	.2	.3	.5	1.0
355.	.1	.1	.1	.1	.1	.1	.1	.1	2.1	2.2	2.0	1.2	1.3	1.0	1.0	.9	.1	.2	.5	1.0
360.	.1	.1	.1	.1	.1	.1	.1	.1	2.3	2.2	2.1	1.4	1.3	1.1	.9	.8	.1	.1	.5	1.0

MAX * 1.7 2.1 2.6 2.2 1.8 1.9 1.9 1.8 2.5 2.5 2.5 2.7 1.7 1.1 1.0 .9 1.2 1.3 1.4 1.9
 DEGR. * 190 185 170 40 35 190 185 50 5 210 215 215 215 0 355 355 290 295 230 210

1

JOB: Brent Spence Bridge S1altlam.dat

RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24

ANGLE	REC21	REC22	REC23	REC24
0.	1.7	1.5	1.3	.9
5.	1.6	1.5	1.3	1.0
10.	1.4	1.6	1.3	.9
15.	1.3	1.5	1.4	.9
20.	1.1	1.5	1.4	.9
25.	1.0	1.2	1.3	.8
30.	.6	.9	1.2	.8
35.	.4	.7	.9	.7
40.	.1	.6	.6	.5
45.	.1	.3	.4	.3
50.	.0	.2	.3	.2
55.	.0	.1	.1	.1
60.	.0	.1	.0	.1
65.	.0	.1	.0	.0
70.	.0	.1	.0	.0
75.	.0	.1	.0	.0
80.	.0	.1	.0	.0
85.	.0	.1	.0	.0
90.	.0	.0	.0	.0
95.	.0	.0	.0	.0
100.	.0	.0	.0	.0
105.	.0	.0	.0	.0
110.	.0	.0	.0	.0
115.	.0	.0	.0	.0
120.	.0	.0	.0	.0
125.	.0	.0	.0	.0
130.	.0	.0	.0	.0
135.	.0	.0	.0	.0
140.	.1	.1	.0	.0
145.	.1	.1	.1	.0
150.	.3	.2	.1	.0
155.	.6	.2	.2	.0
160.	.6	.4	.2	.1

165. * .7 .5 .2 .1
 170. * .9 .5 .3 .1
 175. * 1.0 .6 .4 .1
 180. * .8 .6 .5 .1
 185. * 1.1 .6 .5 .2
 190. * 1.2 1.1 .6 .3
 195. * 1.3 1.4 1.2 .4
 200. * 1.7 1.6 1.4 .3
 205. * 1.7 1.7 1.7 .6

1

JOB: Brent Spence Bridge S1altlam.dat

RUN: Kyles Lane & Dixie Hwy

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24

210. * 1.9 1.8 1.8 .7
 215. * 1.9 1.8 1.9 1.0
 220. * 1.5 1.8 1.9 1.0
 225. * 1.6 1.8 1.7 1.1
 230. * 1.3 1.8 1.7 1.1
 235. * 1.1 1.6 1.6 1.3
 240. * 1.1 1.7 1.5 1.0
 245. * 1.1 1.6 1.4 1.0
 250. * 1.2 1.5 1.3 1.1
 255. * 1.2 1.5 1.2 1.1
 260. * 1.1 1.5 1.2 1.1
 265. * 1.2 1.4 1.1 1.1
 270. * 1.1 1.4 1.0 1.0
 275. * 1.2 1.4 1.0 .9
 280. * 1.3 1.4 1.0 .9
 285. * 1.3 1.5 1.0 1.0
 290. * 1.3 1.5 1.1 .9
 295. * 1.4 1.5 1.1 .8
 300. * 1.5 1.5 1.1 .9
 305. * 1.4 1.4 1.0 .9
 310. * 1.5 1.3 1.1 .9
 315. * 1.5 1.3 1.1 .9
 320. * 1.4 1.4 1.0 .9
 325. * 1.6 1.4 1.1 .9
 330. * 1.6 1.3 1.2 .8
 335. * 1.6 1.4 1.2 .9
 340. * 1.7 1.3 1.2 .9
 345. * 1.6 1.4 1.2 1.1
 350. * 1.6 1.5 1.4 1.0
 355. * 1.6 1.5 1.3 1.0
 360. * 1.7 1.5 1.3 .9

MAX * 1.9 1.8 1.9 1.3
 DEGR. * 210 210 215 235

THE HIGHEST CONCENTRATION IS 2.70 PPM AT 215 DEGREES FROM REC12.
 THE 2ND HIGHEST CONCENTRATION IS 2.60 PPM AT 170 DEGREES FROM REC3.
 THE 3RD HIGHEST CONCENTRATION IS 2.50 PPM AT 210 DEGREES FROM REC10.

1

JOB: Brent Spence Bridge S1altlam.dat
 DATE: 08/30/2010 TIME: 11:45:54.86

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

LINK #	* 190	185	170	40	35	190	185	50	5	210	215	215	215	0	355	355	290	295	230	210
1	* .0	.0	.0	.0	.0	.2	.4	.3	.7	.8	.3	.1	.1	.0	.0	.0	.0	.0	.1	.1
2	* .0	.0	.0	.0	.0	.2	.2	.2	.3	.2	.7	.3	.2	.0	.0	.0	.1	.0	.1	.1
3	* .0	.0	.0	.0	.0	.2	.0	.1	.1	.0	.0	.7	.4	.0	.0	.0	.1	.1	.1	.1
4	* .1	.1	.0	.0	.0	.8	.8	.6	1.1	1.3	1.3	1.3	.8	.0	.0	.0	.1	.1	.3	.5
5	* .0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
6	* .0	.1	.2	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7	* .3	.6	.4	.6	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
8	* .4	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9	* .0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10	* .0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12	* .3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13	* .2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	* .2	.7	.6	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
15	* .1	.3	.7	.7	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16	* .0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17	* .0	.0	.0	.0	.0	.3	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.1	.0	.0	.0
18	* .0	.0	.0	.0	.0	.1	.3	.1	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
19	* .0	.0	.0	.0	.0	.1	.2	.3	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
20	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22	* .0	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.4	.4	.4	.2	.2	.2	.2	.2
23	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	* .0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.4	.2	.0	.0	.0	.0
25	* .0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.2	.0	.0	.0
26	* .0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.3	.0	.0

27 * .1 .1 .2 .0 .0 .0 .1 .0 .0 .0 .0 .2 .2 .2 .3 .4 .3 .4
 28 * .0 .0 .1 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 29 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 30 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 31 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 32 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 33 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 34 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 35 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2
 36 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

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JOB: Brent Spence Bridge S1altlam.dat
 DATE: 08/30/2010 TIME: 11:45:54.86

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24
 LINK # * 210 210 215 235

1 * .1 .0 .0 .0
 2 * .1 .0 .0 .0
 3 * .1 .1 .0 .0
 4 * .4 .3 .2 .0
 5 * .3 .1 .1 .0
 6 * .3 .2 .1 .0
 7 * .0 .6 1.0 .2
 8 * .0 .0 .0 .5
 9 * .0 .0 .0 .2
 10 * .0 .0 .0 .0
 11 * .0 .0 .0 .0
 12 * .0 .0 .0 .0
 13 * .0 .0 .0 .1
 14 * .0 .2 .3 .2
 15 * .0 .1 .2 .1
 16 * .0 .0 .0 .0
 17 * .1 .1 .0 .0
 18 * .0 .0 .0 .0
 19 * .0 .0 .0 .0
 20 * .0 .0 .0 .0
 21 * .1 .0 .0 .0
 22 * .0 .0 .0 .0
 23 * .0 .0 .0 .0
 24 * .0 .0 .0 .0
 25 * .0 .0 .0 .0
 26 * .1 .0 .0 .0
 27 * .0 .0 .0 .0
 28 * .3 .1 .0 .0
 29 * .0 .0 .0 .0
 30 * .0 .0 .0 .0
 31 * .0 .0 .0 .0
 32 * .0 .0 .0 .0
 33 * .0 .0 .0 .0
 34 * .0 .0 .0 .0
 35 * .0 .0 .0 .0
 36 * .0 .0 .0 .0

1

JOB: Brent Spence Bridge S1altlpm.dat
 DATE: 08/30/2010 TIME: 11:51:25.23

RUN: Kyles Lane & Dixie Hwy

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	(FT) (DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	*	184.	20.	AG	760.	11.5	.0	44.0		
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	*	94.	22.	AG	760.	11.5	.0	44.0		
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	*	112.	23.	AG	760.	11.5	.0	44.0		
4. 03 Dixie NB Queue	* 264228.0	275888.0	263898.8	275071.9	*	880.	202.	AG	295.	100.0	.0	24.0	1.20	44.7
5. 04 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	*	105.	22.	AG	540.	11.5	.0	44.0		
6. 05 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	*	62.	22.	AG	465.	11.5	.0	44.0		
7. 06 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	*	149.	22.	AG	1295.	11.5	.0	44.0		
8. 07 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	*	83.	34.	AG	1295.	11.5	.0	44.0		
9. 08 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	*	62.	40.	AG	1295.	11.5	.0	44.0		
10. 09 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	*	112.	48.	AG	1295.	11.5	.0	44.0		
11. 10 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	*	81.	228.	AG	1600.	11.5	.0	44.0		
12. 11 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	*	93.	218.	AG	1600.	11.5	.0	44.0		
13. 12 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	*	62.	209.	AG	1600.	11.5	.0	44.0		
14. 13 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	*	260.	202.	AG	1600.	11.5	.0	44.0		
15. 14 Dixie SB Queue	* 264276.0	276054.0	264390.4	276326.2	*	295.	23.	AG	197.	100.0	.0	24.0	.95	15.0
16. 14 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	*	41.	203.	AG	965.	11.5	.0	40.0		
17. 15 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	*	144.	203.	AG	1345.	11.5	.0	44.0		
18. 16 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	*	99.	201.	AG	1345.	11.5	.0	44.0		
19. 17 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	*	178.	200.	AG	1345.	11.5	.0	44.0		
20. 18 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	*	46.	74.	AG	310.	11.5	.0	32.0		
21. 19 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	*	72.	154.	AG	650.	11.5	.0	32.0		
22. 20 Kyles EB Depart	* 264284.0	275929.0	264483.0	275522.0	*	453.	154.	AG	960.	11.5	.0	44.0		

23. 21 Kyles WB Appr * 264516.0 275540.0 264468.0 275639.0 * 110. 334. AG 1240. 11.5 .0 56.0
 24. 22 Kyles WB Appr * 264468.0 275639.0 264359.0 275852.0 * 239. 333. AG 1240. 11.5 .0 56.0
 25. 23 Kyles WB Rt. * 264359.0 275852.0 264347.0 275900.0 * 49. 346. AG 830. 11.5 .0 32.0
 26. 24 Kyles WB Rt. * 264347.0 275900.0 264300.0 276003.0 * 113. 335. AG 830. 11.5 .0 32.0
 27. 25 Kyles WB Rt. Qu* 264313.0 275975.0 265453.3 273432.6 * 2786. 156. AG 116. 100.0 .0 12.0 1.40 141.6
 28. 25 Kyles WB Rt. @ D* 264300.0 276003.0 264303.0 276071.0 * 68. 3. AG 830. 11.5 .0 32.0
 29. 26 Kyles WB Appr * 264359.0 275852.0 264296.0 275980.0 * 143. 334. AG 30. 11.5 .0 32.0
 30. 28 WB Kyles L* 264307.0 275957.0 264311.3 275948.3 * 10. 154. AG 116. 100.0 .0 12.0 .04 .5
 31. 27 Kyles WB @ Dixie* 264296.0 275980.0 264280.0 276013.0 * 37. 334. AG 15. 11.5 .0 32.0
 32. 28 Kyles WB Lt. * 264296.0 275980.0 264252.0 275994.0 * 46. 288. AG 15. 11.5 .0 32.0
 33. 29 Kyles WB Lt. * 264359.0 275852.0 264325.0 275892.0 * 53. 320. AG 380. 11.5 .0 32.0
 34. 30 Kyles WB Lt. * 264325.0 275892.0 264287.0 275965.0 * 82. 333. AG 380. 11.5 .0 32.0
 35. 33 Kyles WB Lt. Que* 264295.0 275951.0 264350.2 275838.5 * 125. 154. AG 116. 100.0 .0 12.0 .76 6.4
 36. 31 Kyles WB Lt. @ D* 264287.0 275965.0 264236.0 275956.0 * 52. 260. AG 380. 11.5 .0 32.0

JOB: Brent Spence Bridge S1altlpm.dat RUN: Kyles Lane & Dixie Hwy
 DATE: 08/30/2010 TIME: 11:51:25.23

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (gm/hr)	IDLE EM FAC	SIGNAL TYPE	ARRIVAL RATE
4. 03 Dixie NB Queue	* 100	75	2.0	760	1511	73.30	1 3	
15. 14 Dixie SB Queue	* 100	50	2.0	1600	1831	73.30	1 3	
27. 25 Kyles WB Rt. Qu*	100	59	2.0	830	1599	73.30	1 3	
30. 28 WB Kyles L*	100	59	2.0	30	1881	73.30	1 3	
35. 33 Kyles WB Lt. Que*	100	59	2.0	380	1357	73.30	1 3	

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 SB Mid	* 264384.0	276323.0	5.0	*	
2. R2 SB 164	* 264321.0	276211.0	5.0	*	
3. R3 SB 82	* 264290.0	276136.0	5.0	*	
4. R4 SB Corner	* 264262.0	276069.0	5.0	*	
5. R5 SB Corner	* 264230.0	275990.0	5.0	*	
6. R6 SB 82	* 264193.0	275900.0	5.0	*	
7. R7 SB 164	* 264151.0	275798.0	5.0	*	
8. R8 SB Mid	* 264103.0	275678.0	5.0	*	
9. R9 NB Mid	* 264155.0	275655.0	5.0	*	
10. R10 NB 164	* 264184.0	275729.0	5.0	*	
11. R11 NB 82	* 264215.0	275805.0	5.0	*	
12. R12 NB Corner	* 264242.0	275872.0	5.0	*	
13. R13 EB Corner	* 264272.0	275903.0	5.0	*	
14. R14 EB 82	* 264340.0	275765.0	5.0	*	
15. R15 EB 164	* 264378.0	275678.0	5.0	*	
16. R16 EB Mid	* 264408.0	275600.0	5.0	*	
17. R17 WB Mid	* 264455.0	275722.0	5.0	*	
18. R18 WB 164	* 264399.0	275833.0	5.0	*	
19. R19 WB 82	* 264362.0	275906.0	5.0	*	
20. R20 WB Corner	* 264330.0	275971.0	5.0	*	
21. R21 NB Corner	* 264319.0	276046.0	5.0	*	
22. R22 NB 82	* 264343.0	276114.0	5.0	*	
23. R23 NB 164	* 264376.0	276189.0	5.0	*	
24. R24 NB Mid	* 264447.0	276280.0	5.0	*	

JOB: Brent Spence Bridge S1altlpm.dat RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)	(DEGR)* REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18		
0. *	.2	.1	.3	.3	.2	.3	.2	2.3	2.4	2.1	1.3	1.6	1.3	1.2	1.0	.1	.2	.5	1.0	
5. *	.2	.4	.4	.4	.4	.3	.3	2.3	2.4	2.1	1.3	1.5	1.4	1.1	.9	.1	.1	.4	.7	
10. *	.2	.4	.7	.6	.6	.5	.7	.6	2.3	2.2	2.0	1.4	1.5	1.4	1.0	.9	.1	.0	.2	.8
15. *	.3	.8	.9	1.1	1.1	.9	.8	1.1	2.2	1.9	1.8	1.3	1.6	1.1	.9	.9	.1	.0	.0	.5
20. *	.3	1.0	1.4	1.5	1.2	1.2	1.2	1.3	1.8	1.7	1.5	1.3	1.4	1.0	.9	.9	.1	.0	.0	.4
25. *	.6	1.4	1.7	2.1	1.5	1.3	1.5	1.6	1.5	1.4	1.3	1.1	1.2	.9	.9	.7	.1	.0	.0	.0
30. *	.7	1.8	2.1	2.3	1.6	1.4	1.6	1.9	1.1	1.1	.9	1.0	1.2	.9	.8	.7	.0	.0	.0	.0
35. *	.9	2.1	2.4	2.5	1.8	1.5	1.7	2.0	.7	.7	.8	.9	.9	.8	.8	.7	.0	.0	.0	.0
40. *	1.0	2.4	2.7	2.6	1.6	1.4	1.6	2.0	.5	.5	.6	.6	.9	.8	.7	.6	.0	.0	.0	.0
45. *	1.2	2.4	2.6	2.3	1.6	1.3	1.8	2.0	.5	.5	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
50. *	1.3	2.4	2.5	2.2	1.5	1.3	1.8	1.9	.4	.3	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
55. *	1.6	2.3	2.1	2.1	1.3	1.3	2.0	1.9	.4	.4	.4	.7	1.0	.8	.8	.6	.0	.0	.0	.0
60. *	1.6	2.3	2.1	2.0	1.3	1.1	2.0	2.0	.4	.3	.3	.6	1.0	.8	.8	.7	.0	.0	.0	.0
65. *	1.7	2.1	2.0	2.0	1.1	1.3	2.0	1.9	.4	.3	.4	.5	1.0	.8	.8	.7	.0	.0	.0	.0
70. *	1.8	1.9	1.8	1.7	1.1	1.3	1.7	1.8	.3	.3	.4	.5	.9	.8	.8	.7	.0	.0	.0	.0
75. *	1.8	1.8	1.8	1.8	1.0	1.3	1.9	1.8	.3	.3	.3	.6	.9	.8	.7	.6	.0	.0	.0	.0
80. *	1.7	1.8	1.8	1.9	.9	1.3	1.7	1.7	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
85. *	1.7	1.7	1.6	1.6	1.0	1.2	1.7	1.6	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
90. *	1.7	1.6	1.6	1.6	1.0	1.1	1.6	1.6	.3	.3	.3	.6	1.0	.8	.7	.7	.0	.0	.0	.0

95.	*	1.7	1.6	1.6	1.5	1.1	1.2	1.6	1.6	.3	.3	.4	.6	1.0	.8	.8	.7	.0	.0	.0	.0
100.	*	1.5	1.7	1.6	1.6	1.0	1.4	1.6	1.5	.2	.3	.4	.6	1.0	.8	.9	.7	.1	.0	.0	.0
105.	*	1.5	1.6	1.6	1.6	1.2	1.5	1.6	1.5	.2	.3	.5	.5	1.1	.9	.9	.7	.1	.1	.0	.0
110.	*	1.5	1.6	1.6	1.5	1.2	1.5	1.6	1.5	.2	.4	.5	.6	1.1	.9	.9	.8	.1	.1	.0	.1
115.	*	1.5	1.6	1.6	1.5	1.3	1.5	1.6	1.4	.1	.3	.4	.5	1.2	1.0	.9	.8	.1	.1	.0	.1
120.	*	1.5	1.6	1.6	1.4	1.4	1.6	1.6	1.4	.1	.2	.4	.5	1.3	1.0	1.0	.7	.1	.1	.0	.1
125.	*	1.5	1.6	1.6	1.4	1.6	1.7	1.5	1.4	.1	.2	.3	.6	1.1	1.1	1.0	.6	.1	.1	.0	.1
130.	*	1.6	1.6	1.6	1.4	1.7	1.7	1.5	1.4	.1	.1	.3	.6	1.1	1.2	1.0	.6	.1	.1	.0	.1
135.	*	1.6	1.6	1.6	1.4	1.7	1.7	1.4	1.4	.1	.1	.2	.5	1.2	1.1	.9	.6	.1	.2	.2	.2
140.	*	1.7	1.6	1.6	1.5	1.8	1.6	1.5	1.4	.1	.1	.2	.5	1.1	1.1	.8	.4	.4	.3	.2	.4
145.	*	1.6	1.8	1.9	1.7	1.7	1.7	1.6	1.6	.1	.1	.2	.5	1.0	1.0	.7	.4	.4	.5	.5	.5
150.	*	1.8	1.9	2.1	1.7	1.6	1.7	1.6	1.5	.1	.1	.1	.2	1.0	.9	.7	.3	.6	.9	.8	1.1
155.	*	1.9	1.9	2.3	2.0	1.7	1.6	1.5	1.5	.1	.0	.1	.2	.8	.8	.5	.3	.9	1.0	1.0	1.3
160.	*	1.9	2.2	2.4	1.9	1.6	1.6	1.7	1.7	.1	.0	.0	.2	.6	.5	.3	.2	1.0	1.2	1.4	1.5
165.	*	2.2	2.4	2.5	2.0	1.2	1.8	1.9	1.7	.1	.0	.0	.1	.4	.4	.2	.1	1.1	1.3	1.3	1.6
170.	*	2.3	2.5	2.7	1.9	1.2	1.9	1.9	1.7	.1	.0	.1	.1	.2	.2	.1	.0	1.2	1.4	1.4	1.6
175.	*	2.8	2.4	2.6	1.8	1.2	1.9	2.0	1.7	.2	.2	.2	.2	.1	.1	.1	.0	1.3	1.2	1.4	1.7
180.	*	2.7	2.5	2.4	1.6	1.3	2.2	2.1	1.7	.2	.2	.2	.2	.1	.1	.0	.0	1.1	1.2	1.5	1.8
185.	*	3.2	2.6	2.5	1.6	1.6	2.2	2.1	1.8	.4	.4	.4	.4	.2	.1	.0	.0	1.1	1.3	1.4	1.7
190.	*	3.4	2.6	2.3	1.7	1.7	2.1	2.0	1.6	.6	.8	.9	.8	.2	.1	.0	.0	1.1	1.1	1.4	1.5
195.	*	3.4	2.2	2.1	1.8	1.6	2.0	1.8	1.4	1.1	1.2	1.1	1.3	.4	.0	.0	.0	1.0	1.0	1.4	1.5
200.	*	3.4	2.0	1.6	1.7	1.5	1.8	1.5	1.3	1.4	1.6	1.5	1.7	.9	.1	.0	.0	1.0	1.0	1.4	1.6
205.	*	3.1	1.6	1.3	1.3	1.4	1.5	1.4	.9	1.8	2.0	2.0	2.0	1.2	.1	.0	.0	1.0	1.1	1.4	1.8

1

JOB: Brent Spence Bridge S1altlpm.dat

RUN: Kyles Lane & Dixie Hwy

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC15 REC16 REC17 REC18 REC19 REC20

210.	*	2.7	1.3	1.1	.8	.9	.9	1.0	.6	2.0	2.2	2.1	2.3	1.5	.2	.1	.0	1.0	1.1	1.4	2.2
215.	*	2.4	.8	.7	.5	.5	.7	.6	.4	2.1	2.4	2.4	2.4	1.6	.2	.1	.1	.9	1.2	1.5	2.3
220.	*	1.7	.4	.5	.4	.3	.5	.4	.3	2.3	2.4	2.5	2.5	1.5	.3	.2	.1	.9	1.1	1.6	2.0
225.	*	1.4	.2	.2	.2	.2	.2	.2	.1	2.2	2.3	2.4	2.4	1.5	.4	.2	.1	1.0	1.3	1.8	2.0
230.	*	1.0	.2	.2	.1	.1	.2	.2	.1	2.1	2.1	2.3	2.4	1.3	.5	.2	.2	1.0	1.3	1.8	1.8
235.	*	.8	.1	.1	.1	.0	.1	.1	.1	2.0	2.0	2.1	2.2	1.4	.5	.2	.2	1.1	1.4	1.7	1.7
240.	*	.5	.1	.1	.1	.0	.1	.1	.1	2.1	2.0	2.0	2.1	1.3	.5	.2	.2	1.1	1.4	1.7	1.6
245.	*	.4	.1	.1	.1	.0	.1	.1	.1	1.9	1.8	1.8	2.0	1.1	.5	.3	.2	1.1	1.5	1.8	1.6
250.	*	.4	.1	.1	.1	.0	.1	.1	.1	1.8	1.9	1.8	1.9	1.0	.5	.3	.2	1.2	1.5	1.9	1.5
255.	*	.3	.1	.1	.1	.0	.1	.1	.1	1.7	1.8	1.7	1.7	.9	.6	.4	.2	1.1	1.3	1.5	1.3
260.	*	.3	.1	.1	.1	.0	.1	.1	.1	1.7	1.8	1.7	1.7	.7	.6	.4	.2	1.1	1.3	1.6	1.2
265.	*	.3	.1	.1	.1	.0	.1	.1	.0	1.6	1.7	1.7	1.7	.6	.6	.4	.3	1.1	1.3	1.6	1.1
270.	*	.3	.0	.0	.0	.0	.1	.1	.0	1.6	1.6	1.5	1.6	.6	.5	.4	.3	1.2	1.5	1.5	1.1
275.	*	.3	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.6	.7	.5	.3	.4	1.2	1.4	1.5	1.0
280.	*	.3	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.5	.3	.4	1.2	1.4	1.3	1.0
285.	*	.3	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.7	.6	.4	.3	1.3	1.4	1.3	1.0
290.	*	.3	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.6	.3	.3	1.2	1.6	1.4	1.1
295.	*	.3	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.5	.3	.3	1.3	1.5	1.6	.8
300.	*	.2	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.5	.6	.5	.3	.3	1.3	1.3	1.5	.8
305.	*	.2	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.6	.5	.4	.3	1.3	1.3	1.4	1.0
310.	*	.1	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.3	.5	.5	.4	.3	1.3	1.3	1.3	1.1
315.	*	.1	.0	.0	.0	.0	.0	.1	.0	1.6	1.6	1.6	1.2	.5	.5	.4	.2	1.3	1.3	1.3	1.0
320.	*	.1	.1	.1	.1	.0	.1	.1	.1	1.6	1.7	1.7	1.2	.6	.5	.3	.3	1.2	1.1	1.0	.9
325.	*	.1	.1	.1	.1	.0	.1	.1	.1	1.7	1.7	1.7	1.1	.8	.6	.4	.3	1.2	1.0	1.0	1.0
330.	*	.1	.1	.1	.1	.0	.1	.1	.1	1.7	1.7	1.7	1.0	.9	.5	.5	.4	1.1	.9	1.0	1.2
335.	*	.2	.1	.1	.1	.0	.1	.1	.1	1.9	1.8	1.8	1.0	.9	.7	.7	.5	.9	.9	1.0	1.2
340.	*	.2	.1	.1	.1	.0	.1	.1	.1	2.0	2.0	1.8	1.0	.9	.7	.9	.6	.6	.8	1.0	1.1
345.	*	.1	.1	.1	.1	.0	.1	.1	.1	2.1	2.1	1.8	1.2	1.2	1.0	1.0	.9	.5	.6	.9	1.2
350.	*	.1	.1	.1	.1	.1	.1	.1	.1	2.2	2.1	1.9	1.1	1.1	1.1	1.1	.9	.4	.4	.7	1.0
355.	*	.1	.1	.2	.2	.1	.1	.3	.1	2.4	2.3	2.0	1.1	1.4	1.3	1.1	1.1	.2	.4	.6	1.0
360.	*	.2	.1	.3	.3	.2	.2	.3	.2	2.3	2.4	2.1	1.3	1.6	1.3	1.2	1.0	.1	.2	.5	1.0

MAX * 3.4 2.6 2.7 2.6 1.8 2.2 2.1 2.0 2.4 2.4 2.5 2.5 1.6 1.4 1.2 1.1 1.3 1.6 1.9 2.3
 DEGR. * 195 185 40 40 140 180 180 35 355 5 220 220 0 5 0 355 315 290 250 215

1

JOB: Brent Spence Bridge S1altlpm.dat

RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24

0.	*	1.7	1.8	1.6	.9
5.	*	1.7	1.7	1.5	.9
10.	*	1.7	1.6	1.4	.8
15.	*	1.5	1.6	1.5	.8
20.	*	1.1	1.5	1.2	.7
25.	*	.8	1.2	1.2	.7
30.	*	.5	.9	.7	.5
35.	*	.2	.4	.7	.5
40.	*	.1	.4	.5	.4
45.	*	.0	.1	.3	.2
50.	*	.0	.1	.2	.1
55.	*	.0	.1	.1	.1
60.	*	.0	.1	.0	.0


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7 * .2 .4 .3 .4 .0 .0 .0 .0 .0 .0 .0 .0 .1 .1 .0 .0 .0 .0 .0
8 * .2 .0 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
9 * .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
10 * .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
11 * .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
12 * .5 .0 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
13 * .4 .0 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
14 * .3 1.0 .9 1.0 .0 .0 .0 .1 .0 .1 .0 .0 .3 .1 .1 .1 .0 .0 .0
15 * 1.6 .8 .9 .9 .0 .0 .0 .1 .0 .1 .0 .0 .2 .1 .1 .1 .0 .0 .0
16 * .0 .0 .0 .0 .4 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0
17 * .0 .0 .0 .0 .1 .7 .0 .1 .1 .2 .0 .2 .0 .0 .0 .1 .1 .1 .1
18 * .0 .0 .0 .0 .0 .2 .6 .2 .2 .2 .3 .2 .0 .0 .0 .0 .0 .1 .1
19 * .0 .0 .0 .0 .0 .1 .3 .6 .3 .0 .2 .1 .0 .0 .0 .0 .0 .0 .1
20 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0
21 * .0 .0 .0 .0 .2 .0 .0 .0 .0 .0 .0 .0 .2 .0 .0 .0 .0 .0 .0
22 * .0 .1 .0 .0 .3 .0 .0 .0 .0 .0 .0 .0 .2 .5 .5 .4 .2 .2 .2
23 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
24 * .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .2 .3 .3 .6 .4 .0 .0
25 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .1 .2 .0
26 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .2 .4
27 * .0 .1 .0 .0 .2 .0 .0 .0 .0 .0 .0 .0 .1 .2 .2 .3 .3 .3 .4
28 * .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0
29 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
30 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1
31 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
32 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
33 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .1 .0
34 * .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .1 .1
35 * .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .1 .2 .2 .2
36 * .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0

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JOB: Brent Spence Bridge S1altlpm.dat
DATE: 08/30/2010 TIME: 11:51:25.23

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21 REC22 REC23 REC24
LINK # * 210 355 225 225

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1 * .0 .0 .0 .0
2 * .0 .0 .0 .0
3 * .1 .0 .0 .0
4 * .4 .0 .1 .1
5 * .1 .0 .0 .0
6 * .1 .0 .0 .0
7 * .0 .7 .7 .2
8 * .0 .1 .0 .3
9 * .0 .0 .0 .0
10 * .0 .0 .0 .0
11 * .0 .0 .0 .0
12 * .0 .0 .0 .0
13 * .0 .1 .0 .1
14 * .1 .5 .6 .3
15 * .0 .5 .4 .3
16 * .1 .0 .0 .0
17 * .2 .0 .0 .0
18 * .1 .0 .0 .0
19 * .1 .0 .0 .0
20 * .0 .0 .0 .0
21 * .1 .0 .0 .0
22 * .0 .0 .0 .0
23 * .0 .0 .0 .0
24 * .0 .0 .0 .0
25 * .0 .0 .0 .0
26 * .1 .0 .0 .0
27 * .0 .0 .0 .0
28 * .3 .0 .0 .0
29 * .0 .0 .0 .0
30 * .0 .0 .0 .0
31 * .0 .0 .0 .0
32 * .0 .0 .0 .0
33 * .0 .0 .0 .0
34 * .0 .0 .0 .0
35 * .0 .0 .0 .0
36 * .0 .0 .0 .0

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1

JOB: Brent Spence Bridge NB-AM S1nbam.dat
DATE: 08/30/2010 TIME: 10:43:58.98

RUN: Kyles Lane & Dixie Hwy

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

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LINK DESCRIPTION * LINK COORDINATES (FT) * LENGTH BRG TYPE VPH EF H W V/C QUEUE
* X1 Y1 X2 Y2 * (FT) (DEG) (G/MI) (FT) (FT) (VEH)
-----*-----*-----*-----*-----*-----*-----*-----*-----*
1. 01 Dixie NB Appr * 264099.0 275553.0 264162.0 275726.0 * 184. 20. AG 1460. 11.5 .0 44.0
2. 02 Dixie NB Appr * 264162.0 275726.0 264197.0 275813.0 * 94. 22. AG 1460. 11.5 .0 44.0

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3. 03 Dixie NB Appr * 264197.0 275813.0 264240.0 275916.0 * 112. 23. AG 1460. 11.5 .0 44.0
4. 03 Dixie NB Queue * 264228.0 275888.0 263487.8 274052.7 * 1979. 202. AG 242. 100.0 .0 24.0 1.27 100.5
5. 04 Dixie NB @ Kyles* 264240.0 275916.0 264280.0 276013.0 * 105. 22. AG 1210. 11.5 .0 44.0
6. 05 Dixie NB Depart * 264280.0 276013.0 264303.0 276071.0 * 62. 22. AG 1215. 11.5 .0 44.0
7. 06 Dixie NB Depart * 264303.0 276071.0 264360.0 276209.0 * 149. 22. AG 1955. 11.5 .0 44.0
8. 07 Dixie NB Depart * 264360.0 276209.0 264406.0 276278.0 * 83. 34. AG 1955. 11.5 .0 44.0
9. 08 Dixie NB Depart * 264406.0 276278.0 264446.0 276325.0 * 62. 40. AG 1955. 11.5 .0 44.0
10. 09 Dixie NB Depart * 264446.0 276325.0 264529.0 276400.0 * 112. 48. AG 1955. 11.5 .0 44.0
11. 10 Dixie SB Appr * 264499.0 276415.0 264439.0 276361.0 * 81. 228. AG 1020. 11.5 .0 44.0
12. 11 Dixie SB Appr * 264439.0 276361.0 264381.0 276288.0 * 93. 218. AG 1020. 11.5 .0 44.0
13. 12 Dixie SB Appr * 264381.0 276288.0 264351.0 276234.0 * 62. 209. AG 1020. 11.5 .0 44.0
14. 13 Dixie SB Appr * 264351.0 276234.0 264252.0 275994.0 * 260. 202. AG 1020. 11.5 .0 44.0
15. 14 Dixie SB Queue * 264276.0 276054.0 264335.5 276195.4 * 153. 23. AG 180. 100.0 .0 24.0 .55 7.8
16. 14 Dixie SB @ Kyles* 264252.0 275994.0 264236.0 275956.0 * 41. 203. AG 485. 11.5 .0 40.0
17. 15 Dixie SB Depart * 264236.0 275956.0 264179.0 275824.0 * 144. 203. AG 625. 11.5 .0 44.0
18. 16 Dixie SB Depart * 264179.0 275824.0 264143.0 275732.0 * 99. 201. AG 625. 11.5 .0 44.0
19. 17 Dixie SB Depart * 264143.0 275732.0 264083.0 275564.0 * 178. 200. AG 625. 11.5 .0 44.0
20. 18 Dixie NB Rt. * 264240.0 275916.0 264284.0 275929.0 * 46. 74. AG 250. 11.5 .0 32.0
21. 19 Kyles EB @ Dixie* 264252.0 275994.0 264284.0 275929.0 * 72. 154. AG 540. 11.5 .0 32.0
22. 20 Kyles EB Depart * 264284.0 275929.0 264483.0 275522.0 * 453. 154. AG 790. 11.5 .0 44.0
23. 21 Kyles WB Appr * 264516.0 275540.0 264468.0 275639.0 * 110. 334. AG 890. 11.5 .0 56.0
24. 22 Kyles WB Appr * 264468.0 275639.0 264359.0 275852.0 * 239. 333. AG 890. 11.5 .0 56.0
25. 23 Kyles WB Rt. * 264359.0 275852.0 264347.0 275900.0 * 49. 346. AG 740. 11.5 .0 32.0
26. 24 Kyles WB Rt. * 264347.0 275900.0 264300.0 276003.0 * 113. 335. AG 740. 11.5 .0 32.0
27. 25 Kyles WB Rt. Qu* 264313.0 275975.0 265450.1 273439.7 * 2779. 156. AG 128. 100.0 .0 12.0 1.46 141.2
28. 25 Kyles WB Rt. @ D* 264300.0 276003.0 264303.0 276071.0 * 68. 3. AG 740. 11.5 .0 32.0
29. 26 Kyles WB Appr * 264359.0 275852.0 264296.0 275980.0 * 143. 334. AG 10. 11.5 .0 32.0
30. 28 WB Kyles L* 264307.0 275957.0 264308.9 275953.2 * 4. 154. AG 128. 100.0 .0 12.0 .02 .2
31. 27 Kyles WB @ Dixie* 264296.0 275980.0 264280.0 276013.0 * 37. 334. AG 5. 11.5 .0 32.0
32. 28 Kyles WB Lt. * 264296.0 275980.0 264252.0 275994.0 * 46. 288. AG 5. 11.5 .0 32.0
33. 29 Kyles WB Lt. * 264359.0 275852.0 264325.0 275892.0 * 53. 320. AG 140. 11.5 .0 32.0
34. 30 Kyles WB Lt. * 264325.0 275892.0 264287.0 275965.0 * 82. 333. AG 140. 11.5 .0 32.0
35. 33 Kyles WB Lt. Que* 264295.0 275951.0 264321.3 275897.4 * 60. 154. AG 128. 100.0 .0 12.0 .33 3.0
36. 31 Kyles WB Lt. @ D* 264287.0 275965.0 264236.0 275956.0 * 52. 260. AG 140. 11.5 .0 32.0

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JOB: Brent Spence Bridge NB-AM S1nbam.dat
DATE: 08/30/2010 TIME: 10:43:58.98

RUN: Kyles Lane & Dixie Hwy

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
4. 03 Dixie NB Queue *	120	74	2.0	1460	1642	73.30	1	3
15. 14 Dixie SB Queue *	120	55	2.0	1020	1829	73.30	1	3
27. 25 Kyles WB Rt. Qu*	120	78	2.0	740	1599	73.30	1	3
30. 28 WB Kyles L*	120	78	2.0	10	1881	73.30	1	3
35. 33 Kyles WB Lt. Que*	120	78	2.0	140	1350	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 SB Mid	* 264384.0	276323.0	5.0	*	
2. R2 SB 164	* 264321.0	276211.0	5.0	*	
3. R3 SB 82	* 264290.0	276136.0	5.0	*	
4. R4 SB Corner	* 264262.0	276069.0	5.0	*	
5. R5 SB Corner	* 264230.0	275990.0	5.0	*	
6. R6 SB 82	* 264193.0	275900.0	5.0	*	
7. R7 SB 164	* 264151.0	275798.0	5.0	*	
8. R8 SB Mid	* 264103.0	275678.0	5.0	*	
9. R9 NB Mid	* 264155.0	275655.0	5.0	*	
10. R10 NB 164	* 264184.0	275729.0	5.0	*	
11. R11 NB 82	* 264215.0	275805.0	5.0	*	
12. R12 NB Corner	* 264242.0	275872.0	5.0	*	
13. R13 EB Corner	* 264272.0	275903.0	5.0	*	
14. R14 EB 82	* 264340.0	275765.0	5.0	*	
15. R15 EB 164	* 264378.0	275678.0	5.0	*	
16. R16 EB Mid	* 264408.0	275600.0	5.0	*	
17. R17 WB Mid	* 264455.0	275722.0	5.0	*	
18. R18 WB 164	* 264399.0	275833.0	5.0	*	
19. R19 WB 82	* 264362.0	275906.0	5.0	*	
20. R20 WB Corner	* 264330.0	275971.0	5.0	*	
21. R21 NB Corner	* 264319.0	276046.0	5.0	*	
22. R22 NB 82	* 264343.0	276114.0	5.0	*	
23. R23 NB 164	* 264376.0	276189.0	5.0	*	
24. R24 NB Mid	* 264447.0	276280.0	5.0	*	

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JOB: Brent Spence Bridge NB-AM S1nbam.dat

RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24

```

-----*-----
0. * 1.7 1.7 1.3 .9
5. * 1.7 1.6 1.3 1.0
10. * 1.5 1.7 1.3 .9
15. * 1.4 1.6 1.4 .9
20. * 1.2 1.5 1.4 .9
25. * 1.0 1.2 1.3 .8
30. * .6 .9 1.2 .8
35. * .4 .7 .9 .7
40. * .1 .6 .6 .5
45. * .1 .3 .4 .3
50. * .0 .2 .3 .2
55. * .0 .1 .1 .1
60. * .0 .1 .0 .1
65. * .0 .1 .0 .0
70. * .0 .1 .0 .0
75. * .0 .1 .0 .0
80. * .0 .1 .0 .0
85. * .0 .1 .0 .0
90. * .0 .0 .0 .0
95. * .0 .0 .0 .0
100. * .0 .0 .0 .0
105. * .0 .0 .0 .0
110. * .0 .0 .0 .0
115. * .0 .0 .0 .0
120. * .0 .0 .0 .0
125. * .0 .0 .0 .0
130. * .0 .0 .0 .0
135. * .0 .0 .0 .0
140. * .1 .1 .0 .0
145. * .1 .1 .1 .0
150. * .3 .2 .1 .0
155. * .6 .2 .2 .0
160. * .6 .4 .2 .1
165. * .7 .5 .2 .1
170. * .8 .5 .3 .1
175. * 1.0 .6 .4 .1
180. * .9 .6 .5 .1
185. * 1.1 .6 .5 .2
190. * 1.2 1.1 .6 .3
195. * 1.2 1.4 1.1 .3
200. * 1.8 1.4 1.4 .3
205. * 1.7 1.6 1.7 .7

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1

JOB: Brent Spence Bridge NB-AM S1nbam.dat

PAGE 6
RUN: Kyles Lane & Dixie Hwy

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24

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-----*-----
210. * 1.9 1.8 1.8 .7
215. * 1.7 1.7 2.0 1.0
220. * 1.5 1.8 1.8 1.1
225. * 1.6 1.8 1.8 1.2
230. * 1.3 1.7 1.8 1.1
235. * 1.1 1.6 1.8 1.3
240. * 1.1 1.8 1.7 1.1
245. * 1.1 1.6 1.6 1.1
250. * 1.1 1.5 1.6 1.1
255. * 1.1 1.5 1.4 1.1
260. * 1.0 1.5 1.4 1.1
265. * 1.1 1.4 1.4 1.1
270. * 1.1 1.4 1.3 1.0
275. * 1.1 1.4 1.2 .9
280. * 1.3 1.4 1.2 .9
285. * 1.3 1.5 1.1 1.0
290. * 1.4 1.5 1.2 .9
295. * 1.4 1.5 1.2 .8
300. * 1.4 1.5 1.1 .9
305. * 1.4 1.4 1.0 .9
310. * 1.5 1.4 1.1 .9
315. * 1.5 1.4 1.1 .9
320. * 1.6 1.5 1.0 .9
325. * 1.6 1.5 1.1 .9
330. * 1.6 1.5 1.2 .8
335. * 1.6 1.6 1.2 .9
340. * 1.7 1.6 1.2 .9
345. * 1.7 1.6 1.2 1.1
350. * 1.8 1.7 1.4 1.0
355. * 1.7 1.7 1.3 1.0
360. * 1.7 1.7 1.3 .9

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MAX * 1.9 1.8 2.0 1.3
DEGR. * 210 210 215 235

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THE HIGHEST CONCENTRATION IS 2.60 PPM AT 170 DEGREES FROM REC3 .
 THE 2ND HIGHEST CONCENTRATION IS 2.60 PPM AT 220 DEGREES FROM REC12.
 THE 3RD HIGHEST CONCENTRATION IS 2.50 PPM AT 185 DEGREES FROM REC2 .

1

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

LINK #	* 190	185	170	40	35	175	60	50	5	215	210	220	15	0	355	355	310	295	230	205
1 *	.0	.0	.0	.0	.1	.0	.3	.7	.7	.3	.1	.0	.0	.0	.0	.0	.1	.1		
2 *	.0	.0	.0	.0	.2	.2	.2	.2	.2	.7	.2	.0	.0	.0	.0	.0	.0	.1	.1	
3 *	.0	.0	.0	.0	.4	.3	.1	.1	.0	.0	.7	.0	.0	.0	.1	.1	.1	.1		
4 *	.1	.1	.0	.0	.7	.6	.6	1.1	1.3	1.3	1.3	.0	.0	.0	.1	.1	.3	.4		
5 *	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.1	.0	.0	
6 *	.0	.1	.2	.0	.2	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	
7 *	.3	.6	.4	.6	.3	.0	.0	.0	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	
8 *	.4	.0	.0	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	
9 *	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
10 *	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
12 *	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
13 *	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
14 *	.2	.7	.6	.6	.6	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.0	.0	
15 *	.1	.7	.7	.8	.3	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	
16 *	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
17 *	.0	.0	.0	.0	.3	.1	.0	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.0	.0	
18 *	.0	.0	.0	.0	.1	.3	.1	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	
19 *	.0	.0	.0	.0	.0	.0	.3	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	
22 *	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.2	.4	.4	.4	.2	.2	.2	.2	.2	
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
24 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.5	.3	.0	.0	.0	
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.2	.0	.0	
26 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.4	.0	
27 *	.1	.1	.2	.0	.0	.1	.1	.0	.0	.0	.0	.1	.2	.2	.3	.4	.3	.4	.0	
28 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	
29 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
33 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
34 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	
35 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.2	
36 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	

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RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24

LINK #	* 210	210	215	235
1 *	.1	.0	.0	.0
2 *	.1	.0	.0	.0
3 *	.1	.1	.0	.0
4 *	.4	.3	.2	.0
5 *	.3	.1	.1	.0
6 *	.3	.2	.1	.0
7 *	.0	.6	1.0	.2
8 *	.0	.0	.0	.5
9 *	.0	.0	.0	.2
10 *	.0	.0	.0	.0
11 *	.0	.0	.0	.0
12 *	.0	.0	.0	.0
13 *	.0	.0	.0	.1
14 *	.0	.2	.3	.2
15 *	.0	.1	.3	.1
16 *	.0	.0	.0	.0
17 *	.1	.1	.0	.0
18 *	.0	.0	.0	.0
19 *	.0	.0	.0	.0
20 *	.0	.0	.0	.0
21 *	.1	.0	.0	.0
22 *	.0	.0	.0	.0
23 *	.0	.0	.0	.0
24 *	.0	.0	.0	.0
25 *	.0	.0	.0	.0
26 *	.1	.0	.0	.0
27 *	.0	.0	.0	.0
28 *	.3	.1	.0	.0
29 *	.0	.0	.0	.0
30 *	.0	.0	.0	.0
31 *	.0	.0	.0	.0
32 *	.0	.0	.0	.0
33 *	.0	.0	.0	.0
34 *	.0	.0	.0	.0

35 * .0 .0 .0 .0
36 * .0 .0 .0 .0

JOB: Brent Spence Bridge NB-PM S1nbpm.dat RUN: Kyles Lane & Dixie Hwy
DATE: 08/30/2010 TIME: 10:57:22.60

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	* 184.	20.	AG	720.	11.5	.0	44.0			
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	* 94.	22.	AG	720.	11.5	.0	44.0			
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	* 112.	23.	AG	720.	11.5	.0	44.0			
4. 03 Dixie NB Queue	* 264228.0	275888.0	263907.4	275093.1	* 857.	202.	AG	300.	100.0	.0	24.0	1.20	43.5	
5. 04 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	* 105.	22.	AG	430.	11.5	.0	44.0			
6. 05 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	* 62.	22.	AG	445.	11.5	.0	44.0			
7. 06 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	* 149.	22.	AG	1295.	11.5	.0	44.0			
8. 07 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	* 83.	34.	AG	1295.	11.5	.0	44.0			
9. 08 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	* 62.	40.	AG	1295.	11.5	.0	44.0			
10. 09 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	* 112.	48.	AG	1295.	11.5	.0	44.0			
11. 10 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	* 81.	228.	AG	1020.	11.5	.0	44.0			
12. 11 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	* 93.	218.	AG	1570.	11.5	.0	44.0			
13. 12 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	* 62.	209.	AG	1570.	11.5	.0	44.0			
14. 13 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	* 260.	202.	AG	1570.	11.5	.0	44.0			
15. 14 Dixie SB Queue	* 264276.0	276054.0	264371.4	276281.0	* 246.	23.	AG	186.	100.0	.0	24.0	.87	12.5	
16. 14 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	* 41.	203.	AG	915.	11.5	.0	40.0			
17. 15 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	* 144.	203.	AG	1265.	11.5	.0	44.0			
18. 16 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	* 99.	201.	AG	1265.	11.5	.0	44.0			
19. 17 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	* 178.	200.	AG	1265.	11.5	.0	44.0			
20. 18 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	* 46.	74.	AG	290.	11.5	.0	32.0			
21. 19 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	* 72.	154.	AG	670.	11.5	.0	32.0			
22. 20 Kyles EB Depart	* 264284.0	275929.0	264483.0	275522.0	* 453.	154.	AG	960.	11.5	.0	44.0			
23. 21 Kyles WB Appr	* 264516.0	275540.0	264468.0	275639.0	* 110.	334.	AG	1230.	11.5	.0	56.0			
24. 22 Kyles WB Appr	* 264468.0	275639.0	264359.0	275852.0	* 239.	333.	AG	1230.	11.5	.0	56.0			
25. 23 Kyles WB Rt.	* 264359.0	275852.0	264347.0	275900.0	* 49.	346.	AG	850.	11.5	.0	32.0			
26. 24 Kyles WB Rt.	* 264347.0	275900.0	264300.0	276003.0	* 113.	335.	AG	850.	11.5	.0	32.0			
27. 25 Kyles WB Rt. Qu*	* 264313.0	275975.0	265406.9	273536.2	* 2673.	156.	AG	113.	100.0	.0	12.0	1.36	135.8	
28. 25 Kyles WB Rt. @ D*	* 264300.0	276003.0	264303.0	276071.0	* 68.	3.	AG	850.	11.5	.0	32.0			
29. 26 Kyles WB Appr	* 264359.0	275852.0	264296.0	275980.0	* 143.	334.	AG	30.	11.5	.0	32.0			
30. 28 WB Kyles L*	* 264307.0	275957.0	264311.6	275947.7	* 10.	154.	AG	113.	100.0	.0	12.0	.04	.5	
31. 27 Kyles WB @ Dixie	* 264296.0	275980.0	264280.0	276013.0	* 37.	334.	AG	15.	11.5	.0	32.0			
32. 28 Kyles WB Lt.	* 264296.0	275980.0	264252.0	275994.0	* 46.	288.	AG	15.	11.5	.0	32.0			
33. 29 Kyles WB Lt.	* 264359.0	275852.0	264325.0	275892.0	* 53.	320.	AG	350.	11.5	.0	32.0			
34. 30 Kyles WB Lt.	* 264325.0	275892.0	264287.0	275965.0	* 82.	333.	AG	350.	11.5	.0	32.0			
35. 33 Kyles WB Lt. Que*	* 264295.0	275951.0	264348.1	275842.7	* 121.	154.	AG	113.	100.0	.0	12.0	.65	6.1	
36. 31 Kyles WB Lt. @ D*	* 264287.0	275965.0	264236.0	275956.0	* 52.	260.	AG	350.	11.5	.0	32.0			

JOB: Brent Spence Bridge NB-PM S1nbpm.dat RUN: Kyles Lane & Dixie Hwy
DATE: 08/30/2010 TIME: 10:57:22.60

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE (SEC)	RED (SEC)	CLEARANCE (VPH)	APPROACH (VPH)	SATURATION (gm/hr)	IDLE (VPH)	SIGNAL (gm/hr)	ARRIVAL (gm/hr)
4. 03 Dixie NB Queue	* 110	84	2.0	720	1505	73.30	1	3
15. 14 Dixie SB Queue	* 110	52	2.0	1570	1831	73.30	1	3
27. 25 Kyles WB Rt. Qu*	* 110	63	2.0	850	1599	73.30	1	3
30. 28 WB Kyles L*	* 110	63	2.0	30	1881	73.30	1	3
35. 33 Kyles WB Lt. Que*	* 110	63	2.0	350	1370	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	* HGT
1. R1 SB Mid	* 264384.0	276323.0	5.0	*
2. R2 SB 164	* 264321.0	276211.0	5.0	*
3. R3 SB 82	* 264290.0	276136.0	5.0	*
4. R4 SB Corner	* 264262.0	276069.0	5.0	*
5. R5 SB Corner	* 264230.0	275990.0	5.0	*
6. R6 SB 82	* 264193.0	275900.0	5.0	*
7. R7 SB 164	* 264151.0	275798.0	5.0	*
8. R8 SB Mid	* 264103.0	275678.0	5.0	*
9. R9 NB Mid	* 264155.0	275655.0	5.0	*
10. R10 NB 164	* 264184.0	275729.0	5.0	*
11. R11 NB 82	* 264215.0	275805.0	5.0	*
12. R12 NB Corner	* 264242.0	275872.0	5.0	*
13. R13 EB Corner	* 264272.0	275903.0	5.0	*
14. R14 EB 82	* 264340.0	275765.0	5.0	*
15. R15 EB 164	* 264378.0	275678.0	5.0	*
16. R16 EB Mid	* 264408.0	275600.0	5.0	*
17. R17 WB Mid	* 264455.0	275722.0	5.0	*
18. R18 WB 164	* 264399.0	275833.0	5.0	*
19. R19 WB 82	* 264362.0	275906.0	5.0	*
20. R20 WB Corner	* 264330.0	275971.0	5.0	*
21. R21 NB Corner	* 264319.0	276046.0	5.0	*
22. R22 NB 82	* 264343.0	276114.0	5.0	*

23. R23 NB 164 * 264376.0 276189.0 5.0 *
24. R24 NB Mid * 264447.0 276280.0 5.0 *

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PAGE 3
JOB: Brent Spence Bridge NB-PM S1nbpm.dat RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

Angle (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.1	.1	.2	.3	.2	.2	.3	.2	2.2	2.4	2.0	1.3	1.5	1.3	1.2	.9	.1	.2	.4	.9
5.	.1	.3	.4	.4	.4	.3	.3	.3	2.3	2.3	1.9	1.1	1.5	1.4	1.0	.9	.1	.0	.4	.8
10.	.1	.4	.6	.6	.5	.5	.6	.6	2.4	2.2	1.9	1.3	1.4	1.4	1.0	.9	.1	.0	.2	.7
15.	.2	.7	.9	1.0	.9	.9	.8	.9	2.2	1.9	1.7	1.4	1.6	1.1	.9	.9	.1	.0	.0	.5
20.	.2	.9	1.4	1.4	1.2	1.1	1.1	1.3	1.8	1.7	1.3	1.2	1.3	1.0	.9	.8	.1	.0	.0	.4
25.	.3	1.2	1.6	1.9	1.4	1.3	1.5	1.6	1.5	1.3	1.2	1.2	1.2	.9	.9	.7	.1	.0	.0	.0
30.	.5	1.5	1.9	2.2	1.5	1.3	1.4	1.7	1.1	1.0	.9	.9	1.2	.8	.8	.7	.0	.0	.0	.0
35.	.5	1.8	2.2	2.4	1.7	1.5	1.6	1.8	.5	.5	.8	.7	1.0	.8	.8	.6	.0	.0	.0	.0
40.	.7	2.2	2.5	2.6	1.6	1.4	1.6	2.0	.4	.4	.6	.6	.9	.8	.7	.6	.0	.0	.0	.0
45.	.9	2.3	2.4	2.2	1.5	1.2	1.7	2.0	.5	.4	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
50.	.9	2.2	2.3	2.1	1.3	1.2	1.9	1.9	.4	.3	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
55.	1.1	2.1	2.1	2.1	1.3	1.1	2.0	1.9	.4	.4	.7	1.0	.8	.8	.6	.0	.0	.0	.0	.0
60.	1.1	2.2	2.0	1.9	1.3	1.0	2.0	2.0	.4	.3	.3	.5	1.0	.8	.8	.7	.0	.0	.0	.0
65.	1.2	2.1	1.8	1.9	1.1	1.3	1.8	1.7	.3	.3	.4	.5	1.0	.8	.8	.7	.0	.0	.0	.0
70.	1.2	1.9	1.8	1.7	1.1	1.2	1.7	1.7	.3	.3	.4	.5	.9	.8	.8	.7	.0	.0	.0	.0
75.	1.2	1.7	1.7	1.7	1.0	1.1	1.8	1.7	.3	.3	.3	.6	.9	.8	.7	.6	.0	.0	.0	.0
80.	1.2	1.7	1.7	1.8	.9	1.1	1.8	1.7	.3	.3	.3	.5	.9	.8	.7	.6	.0	.0	.0	.0
85.	1.1	1.7	1.6	1.6	.9	1.2	1.8	1.7	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
90.	1.1	1.6	1.6	1.6	.9	1.2	1.7	1.7	.3	.3	.3	.6	1.0	.8	.7	.7	.0	.0	.0	.0
95.	1.1	1.6	1.6	1.5	1.0	1.2	1.7	1.7	.2	.3	.4	.6	1.0	.8	.8	.7	.0	.0	.0	.0
100.	1.0	1.7	1.6	1.6	.9	1.4	1.7	1.6	.2	.3	.4	.6	1.0	.8	.9	.7	.1	.0	.0	.0
105.	1.0	1.6	1.6	1.6	.9	1.5	1.6	1.6	.2	.3	.5	.5	.9	.8	.8	.7	.1	.1	.0	.0
110.	.9	1.6	1.6	1.4	1.1	1.5	1.6	1.5	.2	.3	.5	.5	1.0	.9	.9	.7	.1	.1	.0	.1
115.	.9	1.6	1.6	1.4	1.1	1.5	1.6	1.4	.1	.3	.4	.5	1.2	1.0	.9	.8	.1	.1	.0	.1
120.	.9	1.6	1.6	1.4	1.4	1.6	1.7	1.5	.1	.2	.4	.5	1.3	1.0	1.0	.7	.1	.1	.0	.1
125.	.9	1.6	1.6	1.3	1.6	1.6	1.6	1.5	.1	.2	.3	.6	1.1	1.1	1.0	.6	.1	.1	.0	.1
130.	.9	1.6	1.6	1.4	1.6	1.7	1.6	1.5	.1	.1	.3	.6	1.1	1.2	1.0	.6	.1	.1	.0	.1
135.	.9	1.6	1.6	1.4	1.6	1.7	1.5	1.5	.1	.1	.2	.5	1.2	1.1	.9	.6	.1	.2	.2	.2
140.	1.0	1.6	1.6	1.5	1.5	1.6	1.5	1.5	.1	.1	.2	.4	1.1	1.1	.8	.4	.4	.3	.2	.4
145.	.9	1.7	1.8	1.6	1.6	1.6	1.5	1.5	.1	.1	.2	.4	1.0	1.0	.7	.4	.4	.5	.5	.5
150.	1.0	1.8	2.0	1.7	1.5	1.6	1.5	1.5	.0	.1	.1	.2	1.0	.9	.7	.3	.6	.9	.8	1.0
155.	1.1	1.9	2.3	1.8	1.3	1.6	1.4	1.5	.0	.0	.1	.2	.8	.7	.5	.2	.9	1.0	1.0	1.2
160.	1.1	2.2	2.4	1.9	1.4	1.6	1.7	1.5	.1	.0	.0	.2	.6	.5	.3	.2	1.0	1.2	1.4	1.5
165.	1.4	2.3	2.4	2.0	1.2	1.7	1.8	1.7	.1	.0	.0	.0	.4	.4	.2	.1	1.1	1.3	1.3	1.5
170.	1.4	2.4	2.6	1.9	1.2	1.9	1.8	1.7	.1	.0	.1	.1	.2	.2	.1	.0	1.2	1.4	1.4	1.7
175.	1.9	2.4	2.6	1.9	1.2	1.9	1.8	1.7	.2	.2	.2	.2	.1	.1	.1	.0	1.2	1.2	1.4	1.6
180.	1.8	2.5	2.4	1.4	1.3	2.0	2.0	1.8	.2	.2	.2	.2	.1	.1	.0	.0	1.1	1.2	1.4	1.8
185.	2.1	2.6	2.4	1.6	1.5	2.1	2.1	1.8	.4	.4	.4	.4	.2	.1	.0	.0	1.1	1.3	1.4	1.7
190.	2.4	2.5	2.1	1.7	1.6	2.1	2.1	1.5	.6	.8	.9	.7	.2	.1	.0	.0	1.1	1.1	1.5	1.5
195.	2.2	2.2	1.9	1.8	1.5	2.0	1.7	1.4	1.1	1.0	1.1	1.4	.4	.0	.0	.0	1.0	1.0	1.4	1.5
200.	2.3	2.0	1.5	1.6	1.5	1.7	1.5	1.2	1.3	1.6	1.5	1.6	.9	.1	.0	.0	1.0	1.0	1.3	1.6
205.	2.1	1.6	1.3	1.2	1.4	1.4	1.2	.8	1.8	1.9	2.0	2.0	1.2	.1	.0	.0	1.0	1.1	1.5	1.9

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PAGE 4
JOB: Brent Spence Bridge NB-PM S1nbpm.dat RUN: Kyles Lane & Dixie Hwy

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

Angle (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210.	1.8	1.2	1.0	.7	.9	.9	.9	.6	2.0	2.2	2.1	2.4	1.5	.2	.1	.0	.9	1.1	1.4	2.1
215.	1.6	.8	.7	.5	.5	.7	.6	.3	2.2	2.4	2.3	2.4	1.6	.2	.1	.0	.9	1.2	1.5	2.2
220.	1.0	.4	.5	.3	.3	.5	.4	.3	2.2	2.4	2.4	2.4	1.5	.3	.2	.1	.9	1.1	1.6	2.1
225.	.8	.2	.2	.2	.2	.2	.2	.1	2.2	2.2	2.4	2.3	1.5	.4	.2	.1	1.0	1.3	1.8	1.9
230.	.5	.2	.2	.1	.0	.2	.1	.1	2.1	2.1	2.2	2.4	1.3	.5	.2	.2	1.0	1.3	1.8	1.8
235.	.3	.1	.1	.1	.0	.1	.1	.1	2.0	2.1	2.1	2.3	1.3	.5	.2	.2	1.1	1.4	1.7	1.8
240.	.1	.1	.1	.1	.0	.1	.1	.1	2.0	2.0	2.0	2.0	1.3	.5	.2	.2	1.1	1.4	1.7	1.6
245.	.1	.1	.1	.1	.0	.1	.1	.1	1.8	1.8	1.8	1.9	1.1	.5	.2	.2	1.1	1.5	1.8	1.6
250.	.1	.1	.1	.1	.0	.1	.1	.1	1.8	1.8	1.8	1.9	.9	.5	.3	.2	1.2	1.5	1.7	1.5
255.	.1	.1	.1	.1	.0	.1	.1	.1	1.7	1.7	1.7	1.7	.8	.5	.4	.2	1.1	1.3	1.5	1.3
260.	.1	.1	.1	.1	.0	.1	.1	.0	1.7	1.8	1.7	1.7	.7	.6	.4	.2	1.1	1.2	1.5	1.2
265.	.1	.1	.1	.1	.0	.1	.1	.0	1.7	1.7	1.6	1.7	.6	.6	.4	.3	1.1	1.3	1.6	1.1
270.	.1	.0	.0	.0	.0	.1	.1	.0	1.6	1.6	1.4	1.7	.6	.5	.4	.3	1.1	1.4	1.6	1.0
275.	.1	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.5	1.6	.7	.5	.3	.3	1.1	1.4	1.3	1.1
280.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.5	1.6	1.6	.6	.5	.3	.3	1.2	1.5	1.2	1.0
285.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.5	.6	.3	.3	1.2	1.4	1.2	1.0
290.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.6	1.6	.6	.5	.3	.3	1.2	1.4	1.4	1.0
295.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.7	1.6	.6	.6	.3	.3	1.3	1.4	1.3	.8
300.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.5	.6	.5	.3	.2	1.3	1.3	1.5	.8
305.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.6	.5	.3	.3	1.3	1.3	1.3	1.0
310.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.6	1.3	.5	.5	.4	.2	1.3	1.4	1.3	.8
315.	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.7	1.6	1.3	.5	.5	.4	.2	1.3	1.3	1.1	1.0
320.	.0	.1	.1	.1	.0	.1	.1	.0	1.7	1.7	1.5	1.2	.5	.5	.3	.3	1.2	1.1	1.0	.9
325.	.0	.1	.1	.1	.0	.1	.1	.1	1.7	1.7	1.7	1.1	.7	.6	.4	.3	1.2	1.0	1.1	1.0
330.	.0	.1	.1	.1	.0	.1	.1	.1	1.7	1.8	1.7	1.0	.7	.5	.5	.4	1.0	.9	1.0	1.1
335.	.1	.1	.1	.1	.0	.1	.1	.1	1.9	1.8	1.8	1.0	.8	.7	.7	.5	.9	.9	1.0	1.2

340.	*	.1	.1	.1	.1	.0	.1	.1	.1	1.9	2.1	1.8	.9	.9	.7	.9	.6	.6	.7	.9	1.1
345.	*	.1	.1	.1	.1	.0	.1	.1	.1	2.0	2.1	1.8	1.2	1.1	1.0	1.0	.8	.5	.6	.9	1.1
350.	*	.1	.1	.1	.1	.1	.1	.1	.1	2.2	2.0	1.8	1.0	1.0	1.1	1.1	.9	.4	.4	.7	1.0
355.	*	.1	.1	.2	.2	.1	.1	.1	.1	2.4	2.3	2.0	1.1	1.3	1.3	1.0	.9	.1	.4	.5	1.0
360.	*	.1	.1	.2	.3	.2	.2	.3	.2	2.2	2.4	2.0	1.3	1.5	1.3	1.2	.9	.1	.2	.4	.9

MAX	*	2.4	2.6	2.6	2.6	1.7	2.1	2.1	2.0	2.4	2.4	2.4	2.4	1.6	1.4	1.2	.9	1.3	1.5	1.8	2.2
DEGR	*	190	185	170	40	35	185	185	40	10	215	220	210	15	5	0	0	315	280	225	215

1

JOB: Brent Spence Bridge NB-PM S1nbpm.dat PAGE 5
 RUN: Kyles Lane & Dixie Hwy

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24

0.	*	1.6	1.7	1.4	.8
5.	*	1.6	1.7	1.3	.8
10.	*	1.6	1.5	1.2	.7
15.	*	1.5	1.5	1.3	.7
20.	*	1.1	1.4	1.1	.6
25.	*	.7	1.1	1.1	.6
30.	*	.5	.8	.7	.5
35.	*	.2	.4	.6	.5
40.	*	.1	.4	.4	.3
45.	*	.0	.1	.3	.2
50.	*	.0	.1	.2	.1
55.	*	.0	.1	.1	.1
60.	*	.0	.1	.0	.0
65.	*	.0	.1	.0	.0
70.	*	.0	.1	.0	.0
75.	*	.0	.1	.0	.0
80.	*	.0	.0	.0	.0
85.	*	.0	.0	.0	.0
90.	*	.0	.0	.0	.0
95.	*	.0	.0	.0	.0
100.	*	.0	.0	.0	.0
105.	*	.0	.0	.0	.0
110.	*	.0	.0	.0	.0
115.	*	.0	.0	.0	.0
120.	*	.0	.0	.0	.0
125.	*	.0	.0	.0	.0
130.	*	.0	.0	.0	.0
135.	*	.0	.0	.0	.0
140.	*	.0	.0	.0	.0
145.	*	.2	.0	.0	.0
150.	*	.3	.2	.0	.0
155.	*	.5	.3	.2	.0
160.	*	.6	.4	.2	.1
165.	*	1.0	.5	.3	.1
170.	*	1.0	.5	.4	.1
175.	*	.9	.6	.4	.1
180.	*	1.0	.6	.4	.3
185.	*	.9	.8	.6	.3
190.	*	1.0	.9	.7	.3
195.	*	1.4	1.0	.9	.3
200.	*	1.5	1.2	1.2	.5
205.	*	1.5	1.3	1.4	.6

1

JOB: Brent Spence Bridge NB-PM S1nbpm.dat PAGE 6
 RUN: Kyles Lane & Dixie Hwy

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24

210.	*	1.7	1.4	1.6	.7
215.	*	1.7	1.4	1.6	.9
220.	*	1.4	1.6	1.6	1.0
225.	*	1.2	1.6	1.7	1.3
230.	*	1.3	1.5	1.7	1.3
235.	*	1.2	1.5	1.6	1.2
240.	*	1.2	1.5	1.5	1.2
245.	*	.9	1.5	1.5	1.3
250.	*	1.0	1.4	1.5	1.1
255.	*	1.0	1.4	1.4	1.1
260.	*	1.0	1.4	1.4	1.2
265.	*	1.1	1.4	1.4	1.0
270.	*	1.1	1.4	1.4	1.0
275.	*	1.1	1.4	1.4	1.0
280.	*	1.1	1.4	1.4	1.0
285.	*	1.1	1.4	1.4	.9
290.	*	1.2	1.4	1.4	.8
295.	*	1.2	1.4	1.4	.7
300.	*	1.2	1.4	1.4	.7

305. * 1.3 1.4 1.3 .8
 310. * 1.3 1.4 1.3 .9
 315. * 1.3 1.4 1.4 .9
 320. * 1.5 1.4 1.3 .8
 325. * 1.5 1.4 1.5 .8
 330. * 1.5 1.5 1.4 .8
 335. * 1.5 1.5 1.4 .7
 340. * 1.6 1.5 1.5 .8
 345. * 1.6 1.5 1.5 .9
 350. * 1.7 1.7 1.4 .8
 355. * 1.7 1.8 1.5 .8
 360. * 1.6 1.7 1.4 .8

MAX * 1.7 1.8 1.7 1.3
 DEGR. * 210 355 225 225

THE HIGHEST CONCENTRATION IS 2.60 PPM AT 40 DEGREES FROM REC4 .
 THE 2ND HIGHEST CONCENTRATION IS 2.60 PPM AT 185 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS 2.60 PPM AT 170 DEGREES FROM REC3 .

1

JOB: Brent Spence Bridge NB-PM S1nbpm.dat
 DATE: 08/30/2010 TIME: 10:57:22.60

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

LINK # * 190 185 170 40 35 185 185 40 10 215 220 210 15 5 0 0 315 280 225 215

1 *	.0	.0	.0	.0	.1	.2	.1	.3	.4	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
2 *	.0	.0	.0	.0	.1	.1	.1	.1	.1	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
3 *	.0	.0	.0	.0	.1	.0	.1	.1	.1	.0	.3	.0	.0	.0	.0	.1	.0	.1	.0	.1
4 *	.1	.1	.0	.0	.9	.9	.7	1.3	1.5	1.5	1.5	.0	.0	.0	.0	.2	.4	.5	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.2	.4	.3	.4	.2	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0
8 *	.3	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.4	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.3	1.0	.9	1.0	.9	.0	.0	.0	.1	.0	.0	.3	.1	.1	.0	.0	.0	.0	.0	.0
15 *	.5	.8	.7	.9	.3	.0	.0	.0	.1	.0	.0	.2	.1	.1	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.6	.0	.1	.1	.0	.0	.1	.0	.0	.0	.0	.1	.1	.0	.1	.1
18 *	.0	.0	.0	.0	.2	.6	.2	.2	.0	.2	.2	.0	.0	.0	.0	.0	.0	.1	.1	.1
19 *	.0	.0	.0	.0	.1	.3	.6	.1	.4	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.1	.1	.1	.0	.0	.0	.1	.0	.0	.0	.2	.5	.5	.4	.2	.2	.2	.2	.2	.2
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.6	.4	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.3	.0	.0	.0
26 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.4	.0	.0	.0
27 *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.3	.3	.3	.3	.3	.3	.3
28 *	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
29 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
34 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
35 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.2	.2	.2	.2
36 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge NB-PM S1nbpm.dat
 DATE: 08/30/2010 TIME: 10:57:22.60

RUN: Kyles Lane & Dixie Hwy

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24
 LINK # * 210 355 225 225

1 *	.0	.0	.0	.0
2 *	.0	.0	.0	.0
3 *	.1	.0	.0	.0
4 *	.4	.0	.1	.1
5 *	.1	.0	.0	.0
6 *	.1	.0	.0	.0
7 *	.0	.7	.7	.2
8 *	.0	.1	.0	.3
9 *	.0	.0	.0	.0
10 *	.0	.0	.0	.0
11 *	.0	.0	.0	.0
12 *	.0	.0	.0	.0
13 *	.0	.1	.0	.1
14 *	.1	.5	.5	.3

15 * .0 .4 .4 .3
 16 * .0 .0 .0 .0
 17 * .2 .0 .0 .0
 18 * .1 .0 .0 .0
 19 * .1 .0 .0 .0
 20 * .0 .0 .0 .0
 21 * .1 .0 .0 .0
 22 * .0 .0 .0 .0
 23 * .0 .0 .0 .0
 24 * .0 .0 .0 .0
 25 * .0 .0 .0 .0
 26 * .1 .0 .0 .0
 27 * .0 .0 .0 .0
 28 * .3 .0 .0 .0
 29 * .0 .0 .0 .0
 30 * .0 .0 .0 .0
 31 * .0 .0 .0 .0
 32 * .0 .0 .0 .0
 33 * .0 .0 .0 .0
 34 * .0 .0 .0 .0
 35 * .0 .0 .0 .0
 36 * .0 .0 .0 .0

JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:43:54.29

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 EB 5th Phil Appr	* 269695.0	284787.0	269838.0	284789.0	*	143.	89.	AG	1280.	11.5	.0	44.0		
2. 2 EB 5th EB Queue	* 269805.0	284789.0	263736.1	284712.2	*	6069.	269.	AG	202.	100.0	.0	24.0	8.89	308.3
3. 3 EB 5th Bake Appr	* 269838.0	284789.0	270093.0	284793.0	*	255.	89.	AG	1270.	11.5	.0	44.0		
4. 4 EB 5th Bake LT	* 270093.0	284793.0	270194.0	284795.0	*	101.	89.	AG	1250.	11.5	.0	44.0		
5. 5 EB 5th EB Rt	* 270093.0	284776.0	270189.0	284778.0	*	96.	89.	AG	20.	11.5	.0	44.0		
6. 6 EB 5th Main Appr	* 270194.0	284795.0	270550.0	284799.0	*	356.	89.	AG	1340.	11.5	.0	44.0		
7. 7 EB 5th EB Queue	* 270491.0	284798.0	264201.6	284738.7	*	6290.	269.	AG	183.	100.0	.0	24.0	8.48	319.5
8. 8 EB 5th Main Dep	* 270550.0	284799.0	270695.0	284801.0	*	145.	89.	AG	1270.	11.5	.0	44.0		
9. 9 NB Phil 5th Appr	* 269851.0	284462.0	269847.0	284786.0	*	324.	359.	AG	460.	11.5	.0	44.0		
10. 10 NB PhilNB Queue	* 269848.0	284750.0	269872.3	282852.6	*	1898.	179.	AG	235.	100.0	.0	24.0	4.04	96.4
11. 11 NB Phil5th Dep	* 269847.0	284786.0	269841.0	285143.0	*	357.	359.	AG	670.	11.5	.0	44.0		
12. 12 SB Phil5th Appr	* 269823.0	285126.0	269830.0	284793.0	*	333.	179.	AG	130.	11.5	.0	44.0		
13. 13 SB PhilSB Queue	* 269829.0	284819.0	269825.0	285138.8	*	320.	359.	AG	235.	100.0	.0	24.0	1.67	16.2
14. 14 SB PhilPhil Dep	* 269830.0	284793.0	269835.0	284461.0	*	332.	179.	AG	110.	11.5	.0	44.0		
15. 15 NB Park5th Appr	* 270203.0	284576.0	270200.0	284791.0	*	215.	359.	AG	30.	11.5	.0	32.0		
16. 16 NB ParkNB Queue	* 270201.0	284761.0	270201.4	284737.6	*	23.	179.	AG	98.	100.0	.0	12.0	.94	1.2
17. 17 NB Bake5th Dep	* 270200.0	284791.0	270194.0	285216.0	*	425.	359.	AG	50.	11.5	.0	32.0		
18. 18 SB Bake5th Appr	* 270180.0	285216.0	270189.0	284778.0	*	438.	179.	AG	100.	11.5	.0	32.0		
19. 19 SB BakeSB Queue	* 270188.0	284828.0	270174.7	285595.0	*	767.	359.	AG	98.	100.0	.0	12.0	3.13	39.0
20. 20 SB BakeBake Dep	* 270189.0	284778.0	270192.0	284577.0	*	201.	179.	AG	70.	11.5	.0	32.0		
21. 21 NB MainMain Appr	* 270564.0	284513.0	270559.0	284795.0	*	282.	359.	AG	160.	11.5	.0	32.0		
22. 22 NB MainNB Queue	* 270560.0	284768.0	270575.4	283584.7	*	1183.	179.	AG	124.	100.0	.0	12.0	2.96	60.1
23. 23 NB MainMain Dep	* 270559.0	284795.0	270556.0	285029.0	*	234.	359.	AG	330.	11.5	.0	32.0		
24. 24 SB MainMain Appr	* 270535.0	285030.0	270539.0	284802.0	*	228.	179.	AG	250.	11.5	.0	.4		
25. 25 SB MainSB Queue	* 270538.0	284828.0	270526.3	285743.7	*	916.	359.	AG	248.	100.0	.0	24.0	2.84	46.5
26. 26 SB MainMain Dep	* 270539.0	284802.0	270543.0	284513.0	*	289.	179.	AG	150.	11.5	.0	44.0		

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	EM	FAC	TYPE	RATE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
2. 2 EB 5th EB Queue	* 60	31	2.0	1280	175	73.00	1	3
7. 7 EB 5th EB Queue	* 60	28	2.0	1340	171	73.00	1	3
10. 10 NB PhilNB Queue	* 60	36	2.0	460	173	73.00	1	3
13. 13 SB PhilSB Queue	* 60	36	2.0	130	119	73.00	1	3
16. 16 NB ParkNB Queue	* 40	20	2.0	30	80	73.00	1	3
19. 19 SB BakeSB Queue	* 40	20	2.0	100	80	73.00	1	3
22. 22 NB MainNB Queue	* 60	38	2.0	160	183	73.00	1	3
25. 25 SB MainSB Queue	* 60	38	2.0	250	147	73.00	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 EB 82	* 269739.0	284764.0			5.0 *
2. R2 SW Corner	* 269811.0	284765.0			5.0 *
3. R3 SB 82	* 269812.0	284693.0			5.0 *
4. R4 SB 164	* 269813.0	284611.0			5.0 *
5. R5 NB 164	* 269868.0	284612.0			5.0 *
6. R6 NB 82	* 269867.0	284694.0			5.0 *
7. R7 SE Corner	* 269866.0	284766.0			5.0 *
8. R8 EB 82	* 269938.0	284768.0			5.0 *
9. R9 EB 164	* 270018.0	284770.0			5.0 *

10. R10 EB 82	*	270099.0	284760.0	5.0	*
11. R10 SW Corner	*	270171.0	284761.0	5.0	*
12. R12 SE Corner	*	270217.0	284772.0	5.0	*
13. R13 EB 82r	*	270289.0	284773.0	5.0	*
14. R14 EB 164	*	270368.0	284774.0	5.0	*
15. R15 EB 82	*	270447.0	284775.0	5.0	*
16. R16 SW Corner	*	270519.0	284776.0	5.0	*
17. R17 SB 82	*	270520.0	284704.0	5.0	*
18. R18 SB 164	*	270521.0	284622.0	5.0	*
19. R19 NB 164	*	270583.0	284618.0	5.0	*
20. R20 NB 82	*	270581.0	284700.0	5.0	*
21. R21 SE Corner	*	270580.0	284773.0	5.0	*
22. R22 SB 82	*	270652.0	284773.0	5.0	*
23. R23 WB 82	*	270652.0	284829.0	5.0	*
24. R24 NE Corner	*	270580.0	284829.0	5.0	*
25. R25 NB 82	*	270579.0	284901.0	5.0	*
26. R26 NB 164	*	270577.0	284983.0	5.0	*
27. R27 SB 164	*	270525.0	284975.0	5.0	*
28. R28 SB 82	*	270527.0	284893.0	5.0	*
29. R29 NW Corner	*	270518.0	284821.0	5.0	*
30. R30 WB 82	*	270446.0	284821.0	5.0	*
31. R31 WB 164	*	270368.0	284820.0	5.0	*
32. R32 WB 82	*	270288.0	284819.0	5.0	*
33. R33 NE Corner	*	270216.0	284818.0	5.0	*
34. R34 NB 82	*	270215.0	284890.0	5.0	*
35. R35 NB 164	*	270214.0	284972.0	5.0	*
36. R36 SB 164	*	270168.0	284972.0	5.0	*
37. R37 SB 82	*	270169.0	284890.0	5.0	*

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JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 11:43:54.29

RUN: W 5th Street & Bakewell

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT)			*
		X	Y	Z	
38. R38 NW Corner	*	270170.0	284818.0	5.0	*
39. R39 WB 82	*	270098.0	284817.0	5.0	*
40. R40 WB 164	*	270017.0	284815.0	5.0	*
41. R41 WB 82	*	269937.0	284814.0	5.0	*
42. R42 NE Corner	*	269865.0	284813.0	5.0	*
43. R43 NB 82	*	269864.0	284885.0	5.0	*
44. R44 NB 164	*	269863.0	284967.0	5.0	*
45. R45 SB 164	*	269809.0	284966.0	5.0	*
46. R46 SB 82	*	269810.0	284884.0	5.0	*
47. R47 NW Corner	*	269811.0	284812.0	5.0	*
48. R48 WB 82	*	269738.0	284810.0	5.0	*

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	*	1.7	1.9	.9	.9	1.2	1.3	1.7	1.0	1.0	.9	1.0	1.2	1.0	1.1	1.2	1.2	.8	.5	.6	.8
5.	*	1.7	2.0	1.2	1.0	1.0	1.0	1.5	1.0	1.0	.9	1.1	1.1	1.1	1.1	1.3	1.4	.9	.7	.4	.5
10.	*	1.9	2.0	1.2	1.1	.7	.8	1.4	1.0	1.0	.9	1.1	1.1	1.1	1.2	1.3	1.4	.9	.7	.3	.4
15.	*	1.9	2.0	1.0	1.0	.4	.8	1.2	1.0	1.1	.9	1.3	1.1	1.1	1.2	1.4	1.3	.7	.5	.2	.3
20.	*	2.0	1.8	1.1	1.2	.4	.5	1.1	1.0	1.1	1.0	1.0	1.1	1.2	1.2	1.4	1.1	.7	.5	.1	.2
25.	*	2.0	1.5	1.1	1.0	.3	.4	1.0	1.1	1.1	1.0	1.1	1.1	1.2	1.2	1.4	1.0	.5	.5	.1	.2
30.	*	2.0	1.4	1.1	1.1	.2	.4	1.0	1.1	1.2	1.0	1.1	1.1	1.2	1.2	1.4	1.0	.5	.4	.1	.2
35.	*	2.0	1.5	1.1	1.3	.4	.5	1.1	1.2	1.3	1.0	.9	1.3	1.3	1.4	1.3	.9	.4	.4	.1	.2
40.	*	2.0	1.5	1.2	1.3	.4	.5	1.1	1.4	1.3	1.1	1.1	1.3	1.4	1.4	1.4	.9	.5	.4	.0	.2
45.	*	2.3	1.6	1.2	1.2	.4	.5	1.3	1.4	1.4	1.2	1.1	1.3	1.4	1.4	1.4	.8	.5	.4	.0	.1
50.	*	2.2	1.5	1.2	1.1	.4	.5	1.3	1.4	1.5	1.3	1.1	1.3	1.4	1.4	1.3	.8	.5	.4	.0	.1
55.	*	2.3	1.5	1.3	1.1	.4	.6	1.3	1.4	1.6	1.1	1.1	1.5	1.6	1.5	1.3	.9	.5	.3	.0	.1
60.	*	2.1	1.6	1.2	1.1	.4	.6	1.4	1.5	1.6	1.1	1.2	1.5	1.5	1.5	1.3	.9	.4	.3	.0	.1
65.	*	2.2	1.8	1.2	1.0	.3	.8	1.5	1.5	1.7	1.2	1.2	1.6	1.5	1.4	1.2	.8	.4	.3	.0	.0
70.	*	2.2	1.7	1.2	.8	.2	.6	1.5	1.7	1.6	1.3	1.2	1.6	1.6	1.5	1.2	.8	.4	.3	.0	.0
75.	*	1.9	1.7	1.1	.8	.2	.6	1.7	1.7	1.6	1.2	1.1	1.6	1.6	1.4	1.0	.8	.3	.3	.0	.0
80.	*	1.8	1.7	1.0	.8	.2	.3	1.7	1.6	1.7	1.1	1.1	1.5	1.6	1.3	1.0	.8	.3	.3	.0	.0
85.	*	1.7	1.5	.8	.6	.0	.2	1.4	1.4	1.4	.9	.9	1.3	1.3	1.0	.8	.7	.3	.3	.0	.0
90.	*	1.5	1.2	.8	.6	.0	.2	1.2	1.2	1.3	.6	.7	1.1	1.0	.8	.7	.7	.3	.3	.0	.0
95.	*	1.2	1.0	.6	.6	.0	.0	.8	.9	.8	.5	.5	.8	.7	.7	.5	.6	.3	.3	.0	.0
100.	*	.7	.7	.6	.6	.0	.0	.6	.6	.6	.2	.3	.5	.4	.6	.4	.5	.3	.3	.0	.0
105.	*	.6	.5	.6	.6	.0	.0	.3	.3	.4	.2	.2	.3	.4	.4	.4	.4	.3	.3	.0	.0
110.	*	.5	.5	.6	.6	.0	.0	.2	.2	.2	.0	.1	.2	.2	.2	.2	.4	.3	.3	.0	.0
115.	*	.4	.4	.6	.6	.0	.0	.1	.1	.1	.0	.1	.2	.2	.2	.3	.3	.3	.3	.0	.0
120.	*	.4	.5	.6	.6	.0	.0	.1	.1	.1	.0	.2	.2	.2	.2	.3	.3	.3	.3	.0	.0
125.	*	.4	.6	.7	.7	.0	.0	.1	.1	.1	.0	.2	.2	.2	.2	.3	.3	.3	.3	.0	.0
130.	*	.4	.8	.8	.8	.0	.0	.0	.1	.1	.0	.2	.2	.2	.2	.3	.3	.3	.3	.0	.0
135.	*	.4	.8	.9	.9	.0	.0	.0	.1	.1	.0	.2	.1	.2	.2	.3	.3	.3	.3	.0	.0
140.	*	.4	.9	.9	.9	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.3	.3	.3	.0	.0

145. * .4 .9 .9 .9 .0 .0 .0 .0 .0 .0 .1 .1 .1 .1 .1 .4 .3 .3 .0 .0
 150. * .4 .9 1.0 1.0 .0 .0 .0 .0 .0 .0 .1 .1 .1 .1 .1 .5 .4 .4 .0 .0
 155. * .4 1.0 1.0 1.0 .2 .2 .2 .0 .0 .0 .0 .1 .1 .1 .1 .5 .4 .4 .0 .0
 160. * .4 1.0 1.0 1.0 .3 .3 .3 .0 .0 .0 .0 .1 .1 .1 .1 .4 .4 .4 .0 .1
 165. * .4 1.1 1.1 1.0 .4 .4 .4 .0 .0 .0 .0 .1 .1 .1 .1 .4 .4 .4 .1 .1
 170. * .3 1.0 .9 .9 .7 .8 .8 .1 .0 .0 .0 .0 .0 .1 .1 .4 .4 .4 .2 .2
 175. * .3 .9 .9 .9 1.0 1.0 1.0 .2 .1 .0 .0 .0 .0 .1 .3 .3 .3 .3 .3
 180. * .2 .7 .7 .6 1.3 1.4 1.3 .3 .1 .1 .0 .0 .0 .1 .3 .3 .3 .3 .5
 185. * .1 .5 .4 .4 1.4 1.5 1.4 .3 .2 .1 .1 .2 .0 .0 .2 .2 .1 .5 .5
 190. * .1 .2 .2 .2 1.6 1.6 1.5 .4 .2 .2 .1 .2 .1 .0 .0 .1 .1 .1 .5 .5
 195. * .0 .1 .1 .1 1.6 1.6 1.4 .5 .3 .2 .1 .2 .1 .1 .1 .0 .0 .0 .5 .5
 200. * .0 .0 .0 .0 1.5 1.5 1.3 .5 .3 .2 .2 .2 .1 .1 .1 .1 .1 .1 .5 .5
 205. * .0 .0 .0 .0 1.4 1.4 1.2 .5 .2 .2 .2 .3 .1 .1 .1 .1 .1 .1 .6 .7

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

210. * .0 .0 .0 .0 1.3 1.3 1.0 .5 .2 .2 .2 .3 .1 .1 .1 .1 .1 .6 .7
 215. * .0 .0 .0 .0 1.2 1.2 .9 .4 .2 .2 .1 .3 .1 .1 .1 .1 .1 .6 .7
 220. * .0 .0 .0 .0 1.1 1.1 .8 .4 .3 .2 .1 .3 .1 .1 .1 .1 .1 .5 .6
 225. * .0 .0 .0 .0 1.1 1.1 .7 .5 .4 .2 .1 .3 .2 .2 .2 .2 .1 .5 .5
 230. * .0 .0 .0 .0 1.0 1.0 .6 .5 .4 .2 .1 .2 .2 .2 .2 .2 .1 .5 .5
 235. * .0 .1 .0 .0 1.0 1.0 .5 .5 .4 .2 .1 .2 .2 .2 .2 .1 .1 .5 .5
 240. * .0 .1 .0 .0 1.0 1.0 .4 .5 .4 .2 .1 .2 .2 .2 .2 .1 .1 .5 .5
 245. * .1 .1 .0 .0 1.0 1.0 .4 .4 .4 .1 .1 .2 .2 .2 .2 .1 .1 .5 .5
 250. * .3 .3 .0 .0 1.0 1.0 .6 .6 .6 .2 .2 .4 .3 .3 .4 .4 .1 .5 .5
 255. * .5 .6 .0 .0 .9 .9 .9 1.0 .6 .4 .4 .6 .8 .6 .6 .7 .1 .5 .5
 260. * .8 .9 .2 .0 1.0 1.2 1.2 1.1 1.1 .7 .7 1.1 1.0 1.0 1.0 1.0 .3 .1 .5 .7
 265. * 1.3 1.4 .4 .2 1.2 1.4 1.6 1.5 1.5 1.1 1.0 1.4 1.4 1.5 1.4 1.4 .4 .3 .7 .8
 270. * 1.6 1.8 .5 .3 1.3 1.5 2.1 2.0 1.9 1.3 1.3 1.6 1.5 1.6 1.7 1.7 .5 .4 .7 .8
 275. * 1.9 2.1 .6 .4 1.4 1.6 2.2 2.1 1.9 1.4 1.4 1.7 1.8 1.8 1.9 1.9 .7 .5 .8 1.0
 280. * 2.0 2.3 .7 .4 1.4 1.6 2.3 2.0 2.0 1.5 1.4 1.9 1.8 2.0 2.0 1.8 .6 .3 .7 .9
 285. * 1.9 2.2 .7 .4 1.4 1.6 2.3 2.1 2.0 1.5 1.4 1.8 1.9 1.9 1.8 1.7 .7 .4 .7 1.0
 290. * 1.9 2.1 .6 .4 1.3 1.6 2.0 1.8 1.9 1.3 1.4 1.6 1.7 1.7 1.7 1.5 .6 .5 .8 .9
 295. * 1.9 2.1 .6 .4 1.4 1.7 2.0 1.7 1.7 1.3 1.3 1.5 1.5 1.5 1.3 .6 .4 .7 .9
 300. * 1.7 1.9 .7 .4 1.4 1.7 1.8 1.8 1.7 1.2 1.2 1.6 1.6 1.6 1.4 1.1 .5 .4 .7 .8
 305. * 1.7 1.9 .7 .4 1.4 1.8 1.7 1.5 1.5 1.2 1.1 1.4 1.5 1.5 1.5 1.1 .5 .3 .7 .8
 310. * 1.8 1.8 .6 .4 1.6 1.6 1.6 1.5 1.5 1.2 1.1 1.3 1.3 1.3 1.3 .9 .4 .3 .7 .8
 315. * 1.6 1.8 .7 .4 1.6 1.6 1.7 1.6 1.5 1.1 1.0 1.3 1.3 1.3 1.3 .8 .4 .3 .7 .7
 320. * 1.6 1.5 .7 .5 1.6 1.6 1.6 1.4 1.4 .9 .9 1.3 1.3 1.3 1.3 .8 .4 .3 .7 .7
 325. * 1.6 1.5 .6 .5 1.6 1.6 1.6 1.4 1.4 1.0 .8 1.3 1.2 1.2 1.2 .7 .4 .2 .7 .8
 330. * 1.6 1.5 .6 .4 1.6 1.7 1.7 1.4 1.2 .9 .8 1.1 1.1 1.1 1.1 .6 .4 .2 .9 .7
 335. * 1.6 1.5 .6 .4 1.7 1.8 2.0 1.4 1.1 .8 .8 1.2 1.1 1.1 1.0 .6 .4 .2 .7 .8
 340. * 1.6 1.5 .7 .3 1.8 1.7 1.9 1.3 1.1 .8 .8 1.3 1.1 1.1 1.0 .6 .4 .3 .7 .8
 345. * 1.6 1.5 .7 .4 1.9 1.6 1.9 1.3 1.0 .8 .9 1.2 1.1 1.1 1.0 .8 .5 .3 .9 1.0
 350. * 1.6 1.6 .9 .4 1.7 1.6 1.9 1.2 1.0 .8 .9 1.2 1.1 1.0 1.1 .9 .6 .4 .9 1.0
 355. * 1.6 1.7 .9 .7 1.6 1.5 1.8 1.1 1.0 .9 1.0 1.2 1.1 1.0 1.1 1.1 .6 .6 .8 .8
 360. * 1.7 1.9 .9 .9 1.2 1.3 1.7 1.0 1.0 .9 1.0 1.2 1.0 1.1 1.2 1.2 .8 .5 .6 .8

MAX * 2.3 2.3 1.3 1.3 1.9 1.8 2.3 2.1 2.0 1.5 1.4 1.9 1.9 2.0 2.0 1.9 .9 .7 .9 1.0
 DEGR. * 45 280 55 35 345 335 280 275 280 280 275 280 285 280 280 275 5 5 330 275

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

0. * 1.0 .6 .1 .5 .5 .4 1.7 1.8 .9 .2 .1 .0 .2 .2 .2 .4 .4 .4 .1 .0
 5. * .9 .6 .1 .4 .4 .3 1.8 2.0 1.2 .3 .1 .0 .1 .1 .1 .4 .4 .4 .1 .0
 10. * .8 .4 .0 .2 .2 1.8 2.0 1.3 .3 .2 .1 .1 .1 .1 .5 .5 .5 .1 .0
 15. * .5 .4 .0 .1 .1 .1 1.8 1.9 1.3 .4 .2 .1 .1 .1 .0 .5 .5 .5 .1 .1
 20. * .4 .4 .0 .0 .0 .0 1.6 1.8 1.2 .4 .2 .2 .1 .1 .1 .6 .6 .5 .1 .1
 25. * .5 .4 .0 .0 .0 .0 1.6 1.6 1.1 .4 .2 .2 .1 .1 .1 .5 .5 .5 .2 .1
 30. * .5 .4 .0 .0 .0 .0 1.5 1.5 1.0 .4 .2 .2 .1 .1 .1 .5 .5 .5 .2 .2
 35. * .5 .4 .0 .0 .0 .0 1.4 1.4 1.0 .4 .2 .2 .1 .1 .1 .5 .5 .5 .2 .2
 40. * .5 .4 .0 .0 .0 .0 1.3 1.3 .9 .3 .2 .2 .1 .1 .1 .5 .4 .3 .2 .2
 45. * .5 .4 .0 .0 .0 .0 1.2 1.2 .8 .4 .3 .3 .2 .1 .1 .4 .4 .3 .2 .2
 50. * .5 .4 .0 .0 .0 .0 1.2 1.2 .8 .4 .3 .3 .2 .1 .1 .4 .4 .3 .2 .2
 55. * .6 .4 .0 .0 .0 .0 1.1 1.1 .7 .4 .3 .3 .2 .1 .1 .4 .4 .3 .2 .3
 60. * .6 .3 .0 .0 .0 .0 1.1 1.1 .6 .4 .3 .3 .2 .1 .1 .4 .4 .2 .3 .3
 65. * .6 .3 .0 .0 .0 .0 1.0 1.0 .7 .4 .3 .3 .2 .1 .1 .4 .4 .3 .3 .3
 70. * .5 .3 .0 .0 .0 .0 1.0 1.0 .7 .3 .3 .3 .4 .1 .1 .4 .4 .4 .5 .4
 75. * .5 .2 .0 .1 .0 .0 1.0 1.0 .6 .5 .5 .4 .5 .1 .1 .4 .4 .5 .5 .6
 80. * .5 .2 .0 .1 .0 .0 1.0 1.0 .6 .5 .6 .7 .7 .1 .1 .4 .3 .7 .8 .8
 85. * .4 .2 .1 .2 .0 .0 1.1 1.0 .8 .6 .8 1.0 .9 .1 .1 .4 .3 .9 1.0 1.1
 90. * .3 .1 .1 .2 .0 .0 1.1 1.0 .7 .8 1.0 1.2 1.3 .1 .1 .3 .4 1.2 1.2 1.3
 95. * .2 .1 .1 .3 .0 .0 1.1 1.0 .9 .9 1.2 1.3 1.5 .2 .1 .4 .5 1.4 1.3 1.5
 100. * .1 .0 .2 .4 .0 .0 1.0 1.0 .8 1.0 1.2 1.5 1.4 .3 .1 .4 .6 1.5 1.5 1.6
 105. * .1 .0 .2 .5 .0 .0 1.0 1.0 .8 1.0 1.3 1.5 1.5 .3 .1 .4 .6 1.5 1.5 1.6

70. * .3 .3 .1 .1 1.2 1.2 1.0 .6
75. * .6 .5 .1 .1 1.1 1.1 1.2 .9
80. * .9 .8 .1 .1 1.2 1.2 1.3 1.2
85. * 1.1 1.2 .2 .1 1.2 1.3 1.5 1.4
90. * 1.3 1.3 .3 .1 1.2 1.4 1.7 1.8
95. * 1.5 1.5 .3 .1 1.2 1.5 2.0 2.2
100. * 1.6 1.7 .4 .2 1.3 1.4 1.8 2.3
105. * 1.7 1.6 .5 .2 1.3 1.5 1.8 2.1
110. * 1.7 1.5 .6 .2 1.2 1.6 1.7 2.3
115. * 1.5 1.5 .6 .3 1.5 1.6 1.7 2.3
120. * 1.3 1.3 .5 .3 1.4 1.6 1.7 2.3
125. * 1.3 1.3 .5 .3 1.4 1.6 1.5 2.2
130. * 1.3 1.3 .5 .3 1.5 1.6 1.6 2.3
135. * 1.2 1.2 .4 .3 1.5 1.6 1.5 2.4
140. * 1.1 1.1 .4 .3 1.6 1.6 1.6 2.1
145. * 1.1 1.1 .5 .4 1.7 1.7 1.6 2.1
150. * 1.1 1.1 .5 .4 1.7 1.7 1.6 2.1
155. * 1.1 1.3 .5 .3 1.7 1.8 1.8 2.1
160. * 1.1 1.4 .6 .4 1.7 1.9 2.0 2.2
165. * 1.0 1.5 .7 .5 1.9 1.8 2.0 2.1
170. * 1.1 1.7 1.0 .7 1.9 1.8 2.1 2.0
175. * 1.2 1.9 1.1 1.0 1.8 1.7 2.0 2.0
180. * 1.3 2.2 1.3 1.3 1.4 1.4 1.8 1.9
185. * 1.3 2.2 1.5 1.5 1.2 1.1 1.8 1.8
190. * 1.4 2.1 1.3 1.4 .7 .9 1.5 1.8
195. * 1.5 2.0 1.3 1.3 .5 .8 1.5 1.7
200. * 1.5 1.8 1.4 1.3 .4 .6 1.5 1.7
205. * 1.6 1.8 1.4 1.4 .4 .6 1.5 1.7

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

210. * 1.5 1.6 1.4 1.4 .5 .6 1.6 1.7
215. * 1.5 1.6 1.2 1.5 .5 .7 1.6 1.7
220. * 1.5 1.6 1.4 1.4 .4 .7 1.7 1.9
225. * 1.5 1.6 1.4 1.4 .4 .7 1.9 1.9
230. * 1.6 1.7 1.6 1.2 .4 .7 1.9 1.9
235. * 1.6 1.7 1.6 1.2 .4 .7 2.0 2.0
240. * 1.7 1.9 1.5 1.2 .4 .7 2.1 2.0
245. * 1.8 2.1 1.5 1.2 .4 .6 2.2 2.2
250. * 2.0 2.4 1.5 1.2 .4 .6 2.4 2.2
255. * 2.0 2.5 1.5 1.2 .4 .7 2.4 2.3
260. * 2.1 2.6 1.5 1.2 .4 .7 2.3 2.3
265. * 2.2 2.6 1.4 1.2 .4 .6 2.3 2.1
270. * 2.0 2.2 1.3 1.1 .3 .5 2.0 1.8
275. * 1.6 1.9 1.2 1.0 .2 .4 1.5 1.4
280. * 1.2 1.6 1.0 .8 .0 .2 1.0 .9
285. * .8 1.1 .8 .8 .0 .0 .5 .5
290. * .6 1.0 .8 .8 .0 .0 .3 .3
295. * .4 .7 .8 .8 .0 .0 .1 .2
300. * .5 .8 .8 .8 .0 .0 .1 .1
305. * .4 .8 .8 .8 .0 .0 .1 .1
310. * .4 .8 .9 .9 .0 .0 .0 .1
315. * .4 .9 .9 .9 .0 .0 .0 .1
320. * .4 .9 .9 .9 .0 .0 .0 .0
325. * .4 1.1 1.1 1.0 .0 .0 .0 .0
330. * .4 1.1 1.1 1.0 .0 .0 .0 .0
335. * .3 1.2 1.1 1.0 .1 .1 .1 .0
340. * .3 1.2 1.1 .9 .1 .1 .1 .0
345. * .2 1.2 1.0 .9 .2 .2 .2 .0
350. * .2 1.0 .9 .8 .3 .6 .6 .0
355. * .1 .8 .8 .7 .7 .8 .8 .0
360. * .0 .7 .7 .5 .8 .9 1.1 .1

MAX * 2.2 2.6 1.6 1.5 1.9 1.9 2.4 2.4
DEGR. * 265 260 230 185 165 160 250 135

THE HIGHEST CONCENTRATION IS 2.60 PPM AT 260 DEGREES FROM REC42.
THE 2ND HIGHEST CONCENTRATION IS 2.40 PPM AT 250 DEGREES FROM REC47.
THE 3RD HIGHEST CONCENTRATION IS 2.40 PPM AT 135 DEGREES FROM REC48.

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

DATE: 08/31/2010 TIME: 11:43:54.29

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)

* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

LINK # * 45 280 55 35 345 335 280 275 280 275 280 285 280 280 275 5 5 330 275

1 * .6 .6 .0 .0 .1 .1 .4 .2 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0
2 * .6 .9 .0 .0 .1 .1 .7 .5 .3 .2 .3 .2 .1 .1 .1 .2 .0 .0
3 * .0 .0 .2 .1 .0 .1 .2 .5 .7 .5 .3 .2 .1 .1 .1 .0 .0 .0
4 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .4 .2 .1 .0 .0 .0 .0
5 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
6 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2 .6 .7 .8 .8 .2 .1 .1
7 * .6 .8 .3 .2 .1 .2 .8 .8 .8 .6 .6 .8 .8 .9 .9 .8 .0 .1 .3

8 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
9 *	.0	.0	.2	.2	.3	.2	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.5	.6	1.0	.8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.3	.0	.0	.0	.2	.2	.0	.0	.1	.1	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
14 *	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.4	.3
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5	.3	.1	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0

1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 11:43:54.29

RUN: W 5th Street & Bakewell

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
REC38 REC39 REC40

LINK # * 280 270 260 265 245 210 170 5 265 260 255 255 260 240 250 145 145 265 260 255

1 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
2 *	.1	.2	.1	.2	.0	.0	.0	.2	.1	.1	.1	.2	.0	.2	.0	.0	.3	.2	.2	.2	.2
3 *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.2	.2	.1	.0	.0	.3	.7	.7	.7	.7
4 *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.4	.1	.0	.0	.0	.4	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.6	.3	.3	.5	.2	.1	.1	.8	.8	.7	.6	.2	.0	.0	.1	.2	.0	.0	.0	.0	.0
7 *	.5	.4	.4	.5	.3	.1	.0	.8	.8	.8	.8	.9	.3	.2	.2	.2	.8	.9	.9	.9	.9
8 *	.2	.3	.4	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.1	.1	.1	.1	.1
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0
14 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.3	.3	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.1	.2	.5	.6	1.5	1.9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 11:43:54.29

RUN: W 5th Street & Bakewell

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

LINK # * 265 260 230 185 165 160 250 135

1 *	.2	.4	.2	.1	.0	.1	.6	.6
2 *	.5	.7	.3	.0	.0	.0	.9	.7
3 *	.4	.2	.0	.1	.1	.1	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.9	.9	.3	.1	.1	.2	.9	.7
8 *	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.1	.1	.1	.0	.1
10 *	.0	.0	.0	.4	.3	.3	.0	.3
11 *	.1	.3	.3	.4	.2	.2	.0	.0
12 *	.0	.0	.0	.0	.1	.1	.0	.0
13 *	.1	.1	.5	.3	1.0	.8	.0	.0
14 *	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0

25 * .0 .0 .0 .0 .0 .0 .0 .0
 26 * .0 .0 .0 .0 .0 .0 .0 .0

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 12:02:35.16

RUN: W 5th Street & Bakewell

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	X2	Y2	* (FT) (DEG)	LENGTH BRG	TYPE	VPH	EF	H	W	V/C	QUEUE
							(G/MI)	(FT)	(VEH)					
1. 1 EB 5th Phil Appr	* 269695.0	284787.0	269838.0	284789.0	*		143.	89. AG	10701.	1.5	.0	44.0		
2. 2 EB 5th EB Queue	* 269805.0	284789.0	264562.6	284722.7	*		5243.	269. AG	248.	100.0	.0	24.0	****	266.3
3. 3 EB 5th Bake Appr	* 269838.0	284789.0	270093.0	284793.0	*		255.	89. AG	1060.	11.5	.0	44.0		
4. 4 EB 5th Bake LT	* 270093.0	284793.0	270194.0	284795.0	*		101.	89. AG	1050.	11.5	.0	44.0		
5. 5 EB 5th EB Rt	* 270093.0	284776.0	270189.0	284778.0	*		96.	89. AG	10.	11.5	.0	44.0		
6. 6 EB 5th Main Appr	* 270194.0	284795.0	270550.0	284799.0	*		356.	89. AG	990.	11.5	.0	44.0		
7. 7 EB 5th EB Queue	* 270491.0	284798.0	270396.5	284797.1	*		94.	270. AG	216.	100.0	.0	24.0	.76	4.8
8. 8 EB 5th Main Dep	* 270550.0	284799.0	270695.0	284801.0	*		145.	89. AG	810.	11.5	.0	44.0		
9. 9 NB Phil 5th Appr	* 269851.0	284462.0	269847.0	284786.0	*		324.	359. AG	250.	11.5	.0	44.0		
10. 10 NB PhilNB Queue	* 269848.0	284750.0	269862.6	283611.0	*		1139.	179. AG	307.	100.0	.0	24.0	5.00	57.9
11. 11 NB Phil5th Dep	* 269847.0	284786.0	269841.0	285143.0	*		357.	359. AG	260.	11.5	.0	44.0		
12. 12 SB Phil5th Appr	* 269823.0	285126.0	269830.0	284793.0	*		333.	179. AG	1180.	11.5	.0	44.0		
13. 13 SB PhilSB Queue	* 269829.0	284819.0	269749.7	291089.6	*		6271.	359. AG	307.	100.0	.0	24.0	****	318.6
14. 14 SB PhilPhil Dep	* 269830.0	284793.0	269835.0	284461.0	*		332.	179. AG	1010.	11.5	.0	44.0		
15. 15 NB Park5th Appr	* 270203.0	284576.0	270200.0	284791.0	*		215.	359. AG	70.	11.5	.0	32.0		
16. 16 NB ParkNB Queue	* 270201.0	284761.0	270207.8	284318.6	*		442.	179. AG	98.	100.0	.0	12.0	2.19	22.5
17. 17 NB Bake5th Dep	* 270200.0	284791.0	270194.0	285216.0	*		425.	359. AG	120.	11.5	.0	32.0		
18. 18 SB Bake5th Appr	* 270180.0	285216.0	270189.0	284778.0	*		438.	179. AG	80.	11.5	.0	32.0		
19. 19 SB BakeSB Queue	* 270188.0	284828.0	270178.4	285378.6	*		551.	359. AG	98.	100.0	.0	12.0	2.50	28.0
20. 20 SB BakeBake Dep	* 270189.0	284778.0	270192.0	284577.0	*		201.	179. AG	40.	11.5	.0	32.0		
21. 21 NB MainMain Appr	* 270564.0	284513.0	270559.0	284795.0	*		282.	359. AG	200.	11.5	.0	32.0		
22. 22 NB MainNB Queue	* 270560.0	284768.0	270578.6	283335.2	*		1433.	179. AG	108.	100.0	.0	12.0	2.86	72.8
23. 23 NB MainMain Dep	* 270559.0	284795.0	270556.0	285029.0	*		234.	359. AG	310.	11.5	.0	32.0		
24. 24 SB MainMain Appr	* 270535.0	285030.0	270539.0	284802.0	*		228.	179. AG	330.	11.5	.0	44.0		
25. 25 SB MainSB Queue	* 270538.0	284828.0	270522.3	286049.6	*		1222.	359. AG	215.	100.0	.0	24.0	3.00	62.1
26. 26 SB MainMain Dep	* 270539.0	284802.0	270543.0	284513.0	*		289.	179. AG	130.	11.5	.0	.4		

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 12:02:35.16

RUN: W 5th Street & Bakewell

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* LENGTH (SEC)	CYCLE (SEC)	RED (SEC)	CLEARANCE (VPH)	APPROACH (VPH)	SATURATION (gm/hr)	IDLE	SIGNAL	ARRIVAL
2. 2 EB 5th EB Queue	* 60	38	2.0	1070	173	73.00	1	3	
7. 7 EB 5th EB Queue	* 60	33	2.0	990	1696	73.30	1	3	
10. 10 NB PhilNB Queue	* 60	47	2.0	250	173	73.00	1	3	
13. 13 SB PhilSB Queue	* 60	47	2.0	1180	179	73.00	1	3	
16. 16 NB ParkNB Queue	* 40	20	2.0	70	80	73.00	1	3	
19. 19 SB BakeSB Queue	* 40	20	2.0	80	80	73.00	1	3	
22. 22 NB MainNB Queue	* 60	33	2.0	200	183	73.00	1	3	
25. 25 SB MainSB Queue	* 60	33	2.0	330	146	73.00	1	3	

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	*
1. R1 EB 82	* 269739.0	284764.0	5.0	*
2. R2 SW Corner	* 269811.0	284765.0	5.0	*
3. R3 SB 82	* 269812.0	284693.0	5.0	*
4. R4 SB 164	* 269813.0	284611.0	5.0	*
5. R5 NB 164	* 269868.0	284612.0	5.0	*
6. R6 NB 82	* 269867.0	284694.0	5.0	*
7. R7 SE Corner	* 269866.0	284766.0	5.0	*
8. R8 EB 82	* 269938.0	284768.0	5.0	*
9. R9 EB 164	* 270018.0	284770.0	5.0	*
10. R10 EB 82	* 270099.0	284760.0	5.0	*
11. R10 SW Corner	* 270171.0	284761.0	5.0	*
12. R12 SE Corner	* 270217.0	284772.0	5.0	*
13. R13 EB 82r	* 270289.0	284773.0	5.0	*
14. R14 EB 164	* 270368.0	284774.0	5.0	*
15. R15 EB 82	* 270447.0	284775.0	5.0	*
16. R16 SW Corner	* 270519.0	284776.0	5.0	*
17. R17 SB 82	* 270520.0	284704.0	5.0	*
18. R18 SB 164	* 270521.0	284622.0	5.0	*
19. R19 NB 164	* 270583.0	284618.0	5.0	*
20. R20 NB 82	* 270581.0	284700.0	5.0	*
21. R21 SE Corner	* 270580.0	284773.0	5.0	*
22. R22 SB 82	* 270652.0	284773.0	5.0	*
23. R23 WB 82	* 270652.0	284829.0	5.0	*
24. R24 NE Corner	* 270580.0	284829.0	5.0	*
25. R25 NB 82	* 270579.0	284901.0	5.0	*
26. R26 NB 164	* 270577.0	284983.0	5.0	*
27. R27 SB 164	* 270525.0	284975.0	5.0	*
28. R28 SB 82	* 270527.0	284893.0	5.0	*
29. R29 NW Corner	* 270518.0	284821.0	5.0	*

30. R30 WB 82 * 270446.0 284821.0 5.0 *
 31. R31 WB 164 * 270368.0 284820.0 5.0 *
 32. R32 WB 82 * 270288.0 284819.0 5.0 *
 33. R33 NE Corner * 270216.0 284818.0 5.0 *
 34. R34 NB 82 * 270215.0 284890.0 5.0 *
 35. R35 NB 164 * 270214.0 284972.0 5.0 *
 36. R36 SB 164 * 270168.0 284972.0 5.0 *
 37. R37 SB 82 * 270169.0 284890.0 5.0 *

1

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 12:02:35.16

RUN: W 5th Street & Bakewell

RECEPTOR LOCATIONS

 RECEPTOR * COORDINATES (FT) *
 * X Y Z *
 -----*
 38. R38 NW Corner * 270170.0 284818.0 5.0 *
 39. R39 WB 82 * 270098.0 284817.0 5.0 *
 40. R40 WB 164 * 270017.0 284815.0 5.0 *
 41. R41 WB 82 * 269937.0 284814.0 5.0 *
 42. R42 NE Corner * 269865.0 284813.0 5.0 *
 43. R43 NB 82 * 269864.0 284885.0 5.0 *
 44. R44 NB 164 * 269863.0 284967.0 5.0 *
 45. R45 SB 164 * 269809.0 284966.0 5.0 *
 46. R46 SB 82 * 269810.0 284884.0 5.0 *
 47. R47 NW Corner * 269811.0 284812.0 5.0 *
 48. R48 WB 82 * 269738.0 284810.0 5.0 *

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to
 the maximum concentration, only the first
 angle, of the angles with same maximum
 concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

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 0. * 1.7 2.7 1.8 1.7 1.6 1.7 1.6 .8 .6 .5 .6 .8 .5 .6 1.2 1.2 .6 .4 .6 .6
 5. * 1.8 2.6 2.0 2.0 1.3 1.1 1.3 .6 .5 .6 .5 .5 .5 1.3 1.3 .7 .5 .4 .4
 10. * 1.9 2.5 1.8 1.8 1.0 .8 .9 .5 .5 .4 .5 .6 .5 .6 1.3 1.3 .7 .5 .3 .3
 15. * 2.0 2.3 1.7 1.7 .5 .5 .6 .4 .4 .4 .7 .5 .5 .6 1.4 1.2 .7 .4 .2 .2
 20. * 1.9 2.1 1.5 1.7 .3 .3 .5 .4 .5 .5 .6 .5 .6 .6 1.3 1.1 .5 .5 .1 .1
 25. * 1.9 1.9 1.4 1.6 .2 .2 .4 .5 .6 .5 .5 .5 .6 .7 1.3 1.0 .4 .5 .1 .1
 30. * 1.9 1.6 1.3 1.6 .2 .3 .5 .5 .6 .5 .5 .5 .6 .7 1.4 .9 .3 .4 .1 .1
 35. * 1.9 1.5 1.4 1.5 .2 .3 .5 .6 .6 .6 .5 .5 .6 .7 1.4 .8 .2 .4 .0 .1
 40. * 2.0 1.4 1.4 1.5 .2 .3 .6 .7 .7 .6 .5 .5 .6 .8 1.4 .7 .3 .4 .0 .1
 45. * 1.9 1.5 1.5 1.5 .2 .3 .6 .7 .7 .6 .4 .5 .6 .8 1.3 .7 .4 .3 .0 .1
 50. * 1.9 1.3 1.4 1.4 .2 .3 .6 .7 .7 .6 .5 .6 .6 1.0 1.4 .6 .4 .3 .0 .1
 55. * 1.9 1.2 1.5 1.4 .2 .3 .6 .7 .8 .6 .5 .6 .6 1.1 1.3 .6 .4 .3 .0 .1
 60. * 2.0 1.2 1.5 1.4 .2 .3 .7 .7 .8 .6 .5 .6 .7 1.0 1.1 .5 .4 .3 .0 .0
 65. * 1.7 1.2 1.5 1.4 .2 .2 .7 .7 .7 .5 .6 .7 .8 1.1 1.1 .4 .4 .3 .0 .0
 70. * 1.7 1.3 1.4 1.3 .1 .3 .7 .8 .9 .6 .5 .8 .8 1.2 1.1 .5 .3 .3 .0 .0
 75. * 1.6 1.2 1.4 1.3 .1 .2 .8 .9 .8 .6 .6 .8 .9 1.2 .8 .5 .3 .3 .0 .0
 80. * 1.2 1.2 1.4 1.2 .0 .1 .8 .7 .8 .6 .7 .8 .9 1.2 .7 .5 .3 .3 .0 .0
 85. * 1.2 1.2 1.3 1.2 .0 .1 .7 .7 .4 .5 .6 .7 1.0 .6 .4 .3 .3 .0 .0
 90. * 1.1 1.2 1.2 1.2 .0 .0 .5 .6 .5 .4 .4 .6 .6 .8 .5 .3 .3 .3 .0 .0
 95. * 1.1 1.1 1.2 1.2 .0 .0 .4 .5 .4 .3 .4 .4 .6 .3 .5 .3 .3 .0 .0
 100. * .7 1.0 1.2 1.2 .0 .0 .2 .3 .4 .2 .2 .3 .3 .4 .4 .3 .3 .0 .0
 105. * .6 .8 1.2 1.2 .0 .0 .1 .1 .1 .1 .2 .2 .2 .3 .2 .4 .3 .3 .0 .0
 110. * .6 .9 1.2 1.2 .0 .0 .1 .1 .2 .1 .2 .1 .2 .2 .2 .2 .3 .3 .0 .0
 115. * .6 .9 1.2 1.2 .0 .0 .1 .1 .2 .1 .2 .1 .2 .2 .2 .2 .3 .3 .0 .0
 120. * .6 .9 1.2 1.2 .0 .0 .1 .1 .2 .1 .2 .1 .2 .2 .2 .2 .3 .3 .0 .0
 125. * .6 1.0 1.2 1.2 .0 .0 .0 .1 .2 .1 .2 .0 .1 .1 .1 .3 .3 .3 .0 .0
 130. * .6 1.2 1.3 1.3 .0 .0 .0 .1 .1 .1 .2 .1 .1 .1 .1 .3 .3 .3 .0 .0
 135. * .6 1.3 1.4 1.4 .0 .0 .0 .1 .1 .2 .1 .1 .1 .1 .1 .3 .3 .3 .0 .0
 140. * .6 1.3 1.4 1.4 .0 .0 .0 .1 .1 .2 .1 .1 .1 .1 .1 .3 .3 .3 .0 .0
 145. * .6 1.4 1.4 1.4 .0 .0 .0 .1 .1 .3 .1 .1 .1 .1 .1 .3 .3 .3 .0 .0
 150. * .6 1.5 1.6 1.6 .1 .1 .0 .0 .1 .1 .2 .1 .1 .1 .1 .3 .3 .2 .0 .0
 155. * .6 1.6 1.6 1.6 .1 .1 .0 .0 .1 .2 .1 .1 .1 .1 .1 .3 .3 .2 .0 .0
 160. * .5 1.8 1.6 1.6 .2 .2 .3 .0 .0 .1 .3 .0 .1 .1 .1 .3 .3 .2 .0 .0
 165. * .5 1.8 1.7 1.6 .5 .5 .6 .0 .0 .1 .2 .1 .1 .1 .1 .4 .3 .3 .1 .1
 170. * .5 1.7 1.6 1.6 .9 .9 .9 .1 .0 .1 .2 .2 .0 .1 .1 .2 .2 .2 .2 .2
 175. * .3 1.5 1.5 1.3 1.2 1.2 1.3 .2 .1 .0 .2 .2 .0 .0 .1 .2 .2 .2 .2 .3
 180. * .2 1.2 1.1 1.1 1.5 1.6 1.7 .3 .1 .0 .1 .3 .0 .0 .1 .2 .2 .2 .4 .4
 185. * .1 .9 .8 .8 1.8 2.0 1.9 .4 .2 .1 .1 .3 .1 .0 .0 .1 .1 .1 .5 .5
 190. * .0 .6 .6 .6 2.0 2.1 2.1 .6 .2 .1 .2 .5 .1 .0 .0 .1 .1 .1 .5 .5
 195. * .0 .3 .3 .3 2.0 2.2 2.0 .6 .3 .2 .1 .5 .2 .0 .0 .0 .0 .0 .5 .5
 200. * .0 .3 .3 .2 2.0 2.1 1.9 .6 .3 .2 .2 .5 .2 .1 .0 .0 .0 .0 .5 .5
 205. * .0 .1 .1 .1 1.9 1.9 1.7 .6 .3 .2 .2 .5 .2 .2 .1 .0 .0 .0 .4 .5

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

210.	*	.0	.1	.1	.1	1.9	1.9	1.5	.7	.4	.2	.2	.5	.2	.2	.1	.1	.1	.0	.4	.4
215.	*	.0	.1	.1	.1	1.8	1.8	1.3	.7	.4	.2	.2	.5	.2	.2	.1	.1	.1	.1	.5	.5
220.	*	.0	.1	.1	.1	1.7	1.7	1.2	.6	.4	.2	.2	.4	.2	.2	.2	.1	.1	.1	.5	.5
225.	*	.0	.1	.1	.1	1.7	1.7	1.1	.6	.4	.3	.2	.4	.2	.2	.2	.1	.1	.1	.5	.5
230.	*	.0	.2	.1	.0	1.5	1.5	.9	.6	.5	.3	.2	.4	.2	.2	.2	.1	.1	.1	.5	.5
235.	*	.1	.1	.0	.0	1.5	1.5	.8	.6	.5	.3	.3	.3	.2	.2	.2	.1	.1	.1	.5	.5
240.	*	.1	.1	.0	.0	1.4	1.4	.7	.6	.4	.3	.3	.4	.2	.3	.3	.2	.1	.1	.5	.5
245.	*	.2	.2	.0	.0	1.4	1.4	.7	.6	.4	.3	.3	.3	.3	.3	.2	.2	.1	.1	.5	.5
250.	*	.2	.2	.0	.0	1.4	1.4	.8	.6	.5	.3	.2	.4	.4	.3	.2	.2	.1	.1	.4	.5
255.	*	.4	.5	.1	.0	1.4	1.5	.9	.8	.7	.5	.4	.5	.5	.4	.4	.5	.1	.1	.5	.5
260.	*	.6	.7	.1	.1	1.5	1.5	1.2	1.0	.9	.5	.5	.6	.8	.4	.5	.6	.2	.2	.5	.6
265.	*	.9	1.0	.2	.1	1.5	1.6	1.5	1.2	1.1	.8	.6	.8	.7	.8	.9	.9	.3	.2	.5	.6
270.	*	1.1	1.5	.3	.2	1.6	1.7	1.7	1.3	1.3	1.0	.8	.9	.9	.8	.9	1.0	.3	.3	.6	.7
275.	*	1.4	1.6	.4	.3	1.7	1.8	1.9	1.5	1.3	1.0	.8	1.0	.9	1.0	1.1	1.3	.3	.3	.6	.7
280.	*	1.4	1.7	.4	.3	1.7	1.8	1.9	1.4	1.2	1.0	1.0	1.0	.9	1.0	1.0	1.3	.4	.3	.6	.6
285.	*	1.5	1.7	.4	.3	1.7	1.9	1.8	1.4	1.1	.9	.7	.9	.9	.9	1.1	1.3	.3	.1	.4	.8
290.	*	1.4	1.7	.4	.3	1.7	1.9	1.7	1.2	1.1	.7	.8	.9	.9	.6	1.1	1.2	.2	.2	.7	.8
295.	*	1.4	1.6	.5	.3	1.7	1.9	1.4	1.0	1.0	.7	.7	.8	.8	.6	1.1	1.2	.4	.2	.6	.8
300.	*	1.4	1.6	.5	.2	1.6	2.0	1.4	1.1	.9	.7	.7	.9	.7	1.2	1.1	.4	.2	.6	.8	
305.	*	1.4	1.4	.4	.2	1.7	2.0	1.4	1.0	.8	.7	.8	.8	.7	1.3	1.0	.4	.2	.6	.8	
310.	*	1.3	1.4	.5	.3	1.9	2.0	1.4	1.0	.8	.7	.8	.7	.7	1.3	.9	.5	.2	.7	.8	
315.	*	1.3	1.3	.6	.3	2.0	2.1	1.4	1.0	.9	.7	.7	.6	.6	1.3	.8	.5	.2	.7	.8	
320.	*	1.3	1.2	.6	.4	2.0	1.9	1.4	1.1	.9	.6	.6	.8	.6	1.3	.7	.5	.3	.7	.8	
325.	*	1.2	1.2	.6	.4	2.1	2.1	1.4	1.1	.8	.6	.6	.7	.7	1.3	.6	.5	.3	.7	.8	
330.	*	1.2	1.2	.6	.4	2.2	2.1	1.7	1.1	.8	.6	.5	.7	.7	1.1	.6	.5	.3	.8	.8	
335.	*	1.2	1.3	.7	.4	2.2	2.3	1.8	1.0	.8	.6	.5	.7	.7	1.1	.7	.5	.3	.8	.7	
340.	*	1.2	1.3	.7	.6	2.4	2.2	1.8	1.0	.7	.6	.5	.8	.7	1.1	.6	.5	.4	.9	1.0	
345.	*	1.3	1.6	1.0	.8	2.4	2.3	1.9	1.0	.7	.6	.6	.9	.7	1.1	.8	.6	.4	.8	1.2	
350.	*	1.4	2.0	1.4	1.1	2.4	2.2	2.0	1.0	.7	.6	.6	.9	.7	.5	1.2	1.0	.7	.5	.8	1.1
355.	*	1.6	2.2	1.6	1.3	2.2	1.9	1.9	.9	.7	.5	.7	.9	.6	.5	1.2	1.2	.9	.6	.8	1.0
360.	*	1.7	2.7	1.8	1.7	1.6	1.7	1.6	.8	.6	.5	.6	.8	.5	.6	1.2	1.2	.6	.4	.6	.6

MAX	*	2.0	2.7	2.0	2.0	2.4	2.3	2.1	1.5	1.3	1.0	1.0	1.0	.9	1.2	1.4	1.3	.9	.6	.9	1.2
DEGR.	*	15	0	5	5	340	335	190	275	270	270	280	280	285	70	30	275	355	355	340	345

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

0.	*	.8	.4	.1	.5	.5	.4	1.6	1.8	1.0	.2	.2	.1	.4	.4	.3	.4	.4	.4	.2	.2
5.	*	.7	.4	.1	.4	.4	.3	1.7	2.0	1.2	.3	.1	.1	.2	.2	.1	.4	.4	.4	.2	.1
10.	*	.5	.3	.0	.2	.2	.2	1.7	2.0	1.3	.3	.2	.1	.2	.2	.1	.4	.4	.5	.1	.1
15.	*	.4	.3	.0	.1	.1	.1	1.7	1.9	1.3	.3	.2	.1	.1	.1	.1	.6	.6	.7	.1	.0
20.	*	.3	.3	.0	.0	.0	.0	1.6	1.7	1.3	.3	.2	.1	.1	.1	.1	.5	.5	.2	.1	
25.	*	.3	.3	.0	.0	.0	.0	1.6	1.6	1.2	.3	.2	.2	.1	.1	.1	.4	.5	.5	.2	.2
30.	*	.3	.3	.0	.0	.0	.0	1.5	1.5	1.1	.3	.2	.2	.1	.1	.1	.4	.4	.4	.2	.2
35.	*	.3	.3	.0	.0	.0	.0	1.4	1.4	1.1	.4	.2	.2	.1	.1	.1	.4	.4	.4	.2	.2
40.	*	.3	.3	.0	.0	.0	.0	1.2	1.3	1.0	.4	.2	.2	.1	.1	.1	.4	.4	.3	.2	.2
45.	*	.3	.3	.0	.0	.0	.0	1.2	1.2	.9	.4	.2	.2	.1	.1	.1	.4	.4	.3	.2	.2
50.	*	.3	.2	.0	.0	.0	.0	1.1	1.1	.8	.4	.2	.1	.1	.1	.1	.4	.4	.3	.2	.2
55.	*	.4	.2	.0	.0	.0	.0	1.1	1.1	.7	.4	.2	.1	.1	.1	.1	.4	.4	.3	.2	.2
60.	*	.4	.2	.0	.0	.0	.0	1.0	1.0	.7	.4	.3	.2	.2	.1	.1	.4	.4	.2	.2	.2
65.	*	.4	.2	.0	.0	.0	.0	1.0	1.0	.6	.4	.3	.2	.2	.1	.1	.4	.4	.2	.3	.3
70.	*	.3	.2	.0	.0	.0	.0	1.0	1.0	.6	.4	.3	.2	.2	.1	.1	.4	.4	.3	.3	.3
75.	*	.3	.2	.0	.0	.0	.0	1.0	1.0	.7	.4	.4	.3	.3	.1	.1	.4	.4	.3	.4	.4
80.	*	.3	.1	.0	.1	.0	.0	1.0	1.0	.6	.6	.4	.5	.5	.1	.1	.4	.3	.4	.5	.5
85.	*	.2	.1	.0	.1	.0	.0	1.0	1.0	.7	.4	.7	.6	.6	.1	.1	.4	.3	.6	.5	.5
90.	*	.2	.1	.1	.1	.0	.0	1.0	1.0	.7	.6	.9	.8	.7	.1	.1	.3	.3	.6	.6	.5
95.	*	.1	.0	.1	.2	.0	.0	1.0	1.0	.7	.7	1.1	.7	.7	.2	.1	.4	.4	.6	.7	.6
100.	*	.1	.0	.1	.2	.0	.0	1.0	1.0	.7	.7	1.0	.8	.7	.3	.1	.4	.6	.8	.6	.7
105.	*	.1	.0	.1	.3	.0	.0	1.0	1.0	.7	.7	1.1	.8	.7	.2	.1	.4	.5	.8	.6	.7
110.	*	.0	.0	.2	.3	.0	.0	1.0	1.0	.7	.9	1.0	.7	.7	.2	.1	.5	.5	.6	.7	.6
115.	*	.0	.0	.2	.3	.0	.0	1.0	1.1	.7	1.0	1.1	.6	.6	.3	.2	.4	.6	.6	.6	.6
120.	*	.0	.0	.2	.3	.0	.0	1.0	1.2	.6	1.1	1.1	.7	.5	.3	.2	.5	.6	.5	.6	.7
125.	*	.0	.0	.2	.3	.1	.0	1.1	1.2	.6	1.1	1.0	.6	.5	.3	.2	.5	.5	.5	.6	.7
130.	*	.0	.0	.2	.3	.1	.0	1.1	1.2	.5	1.2	.9	.6	.6	.2	.2	.5	.5	.5	.6	.6
135.	*	.0	.0	.2	.3	.1	.0	1.2	1.3	.6	1.1	.8	.5	.5	.3	.2	.4	.5	.5	.5	.6
140.	*	.0	.0	.3	.3	.1	.0	1.5	1.4	.6	1.1	.7	.5	.5	.3	.2	.4	.5	.6	.5	.5
145.	*	.0	.0	.3	.3	.1	.0	1.5	1.5	.8	1.1	.6	.5	.5	.3	.2	.5	.6	.6	.5	.5
150.	*	.0	.0	.3	.3	.1	.1	1.6	1.5	.8	1.1	.6	.5	.5	.3	.2	.5	.5	.6	.5	.5
155.	*	.0	.0	.3	.3	.1	.1	1.6	1.6	.8	1.1	.6	.5	.5	.3	.2	.5	.4	.6	.5	.5
160.	*	.0	.0	.3	.3	.1	.1	1.8	1.8	.8	1.1	.5	.5	.4	.3	.2	.5	.5	.6	.5	.4
165.	*	.1	.0	.3	.4	.2	.1	1.8	1.8	.8	1.1	.5	.5	.5	.3	.1	.6	.5	.6	.4	.4
170.	*	.2	.0	.3	.4	.2	.3	1.7	1.8	.7	1.1	.5	.4	.5	.3	.2	.5	.4	.6	.4	.4
175.	*	.4	.1	.4	.5	.4	.4	1.7	1.5	.7	1.1	.4	.4	.6	.2	.3	.4	.3	.6	.4	.5
180.	*	.4	.1	.4	.7	.4	.4	1.5	1.4	.6	1.1	.4	.4	.6	.2	.4	.4	.3	.5	.4	.5
185.	*	.5	.1	.4	.7	.4	.6	1.4	1.3	.5	1.0	.4	.5	.6	.4	.5	.4	.4	.5	.5	.6
190.	*	.5	.1	.4	.7	.6	.8	1.2	1.1	.5	1.0	.4	.5	.7	.6	.6	.3	.3	.6	.5	.6
195.	*	.5	.1	.4	.7	.6	.8	.8	.9	.4	1.0	.4	.6	.7	.6	.5	.2	.3	.5	.6	.7
200.	*	.5	.1	.4	.7	.7	.9	.6	.7	.4	1.0	.6	.6	.6	.6	.5	.3	.4	.6	.5	.7
205.	*	.5	.1	.4	.6	.5	1.0	.6	.9	.5	1.1	.6	.6	.7	.5	.6	.4	.3	.6	.6	.8

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40

210.	*	.5	.1	.4	.6	.8	1.1	.6	.8	.6	1.1	.6	.6	.7	.6	.6	.3	.4	.6	.6	.8
215.	*	.5	.2	.5	.6	.8	1.1	.5	.8	.6	1.1	.6	.6	.7	.6	.7	.3	.4	.6	.6	.8
220.	*	.5	.2	.5	.6	1.0	1.0	.4	.7	.7	1.2	.6	.6	.7	.6	.6	.4	.4	.6	.8	.9
225.	*	.5	.2	.5	.6	1.0	1.0	.4	.7	.9	1.2	.6	.6	.7	.7	.6	.3	.5	.7	.8	.9
230.	*	.4	.2	.5	.6	1.0	1.0	.3	.6	.9	1.3	.7	.7	.8	.6	.3	.4	.8	.8	.8	.8
235.	*	.4	.2	.6	.7	1.0	.9	.3	.5	1.0	1.3	.7	.7	.8	.7	.6	.4	.4	.9	.9	.8
240.	*	.4	.2	.5	.8	1.0	.8	.3	.5	1.1	1.1	.7	.7	.8	.6	.5	.4	.4	.9	.9	.9
245.	*	.4	.2	.6	.9	1.0	.8	.2	.5	1.2	1.1	.6	.7	.8	.6	.5	.3	.5	.8	.9	1.0
250.	*	.5	.2	.7	1.1	1.0	.8	.2	.3	1.2	1.1	.6	.9	1.0	.5	.6	.4	.4	.9	.9	1.1
255.	*	.5	.4	.8	1.2	.9	.7	.1	.3	1.3	1.1	.9	.8	1.0	.6	.6	.4	.5	1.0	1.1	1.2
260.	*	.7	.6	.8	1.2	.9	.9	.3	.3	1.3	1.2	1.0	.9	.9	.7	.7	.5	.7	1.2	1.1	1.2
265.	*	.9	.8	.8	1.1	1.0	.9	.3	.3	1.2	.9	.9	.8	1.0	.9	.7	.4	.5	1.1	1.1	1.3
270.	*	1.0	.7	.7	1.1	.9	.8	.3	.3	1.1	.9	.9	.9	1.0	.7	.7	.5	.5	1.1	1.1	1.2
275.	*	1.1	.7	.6	1.1	.8	.8	.2	.2	.9	.6	.8	.8	.9	.7	.5	.4	.4	.9	.9	1.0
280.	*	1.0	.8	.6	.9	.8	.7	.1	.2	.6	.4	.4	.8	.8	.5	.4	.3	.4	.6	.6	.8
285.	*	1.0	.9	.4	.8	.7	.7	.1	.1	.4	.4	.4	.5	.6	.4	.4	.3	.3	.5	.5	.5
290.	*	.9	.7	.3	.7	.7	.7	.1	.2	.2	.2	.3	.4	.3	.4	.3	.3	.3	.4	.4	.5
295.	*	.8	.7	.3	.7	.7	.7	.2	.2	.2	.2	.3	.4	.3	.4	.3	.2	.3	.4	.4	.4
300.	*	.8	.6	.3	.7	.7	.7	.2	.2	.2	.3	.3	.2	.5	.5	.5	.2	.3	.3	.3	.4
305.	*	.8	.6	.4	.7	.8	.8	.2	.2	.1	.2	.2	.2	.5	.5	.5	.2	.2	.3	.3	.3
310.	*	.9	.6	.3	.8	.8	.8	.2	.2	.1	.2	.2	.2	.5	.5	.5	.2	.2	.2	.3	.4
315.	*	1.0	.8	.4	.8	.8	.8	.2	.3	.1	.2	.2	.2	.5	.5	.5	.2	.2	.2	.3	.4
320.	*	.8	.9	.4	.8	.8	.8	.2	.4	.1	.2	.2	.2	.5	.5	.5	.2	.2	.2	.2	.4
325.	*	.9	.7	.4	.8	.8	.8	.4	.4	.1	.1	.2	.3	.5	.5	.5	.2	.2	.2	.2	.4
330.	*	1.1	.7	.4	1.0	.9	.8	.4	.5	.1	.1	.2	.3	.6	.5	.5	.2	.2	.2	.2	.4
335.	*	1.0	.7	.4	1.0	1.0	.8	.5	.6	.2	.1	.3	.3	.6	.6	.6	.2	.2	.2	.2	.3
340.	*	1.1	.7	.4	1.0	1.0	.8	.7	.7	.3	.1	.2	.3	.6	.6	.6	.2	.2	.2	.3	.3
345.	*	1.2	.7	.4	1.0	.9	.8	.9	1.0	.5	.1	.2	.3	.6	.6	.6	.3	.3	.3	.3	.3
350.	*	1.2	.7	.4	.9	.8	.8	1.2	1.4	.6	.2	.1	.3	.6	.5	.5	.3	.3	.3	.3	.3
355.	*	1.1	.6	.3	.8	.7	.7	1.5	1.7	.9	.2	.1	.1	.5	.5	.5	.4	.4	.4	.2	.3
360.	*	.8	.4	.1	.5	.5	.4	1.6	1.8	1.0	.2	.2	.1	.4	.4	.3	.4	.4	.4	.2	.2

MAX * 1.2 .9 .8 1.2 1.0 1.1 1.8 2.0 1.3 1.3 1.1 .9 1.0 .9 .7 .6 .7 1.2 1.1 1.3
 DEGR. * 345 285 255 255 220 210 160 5 255 230 95 250 250 265 215 15 260 260 255 265

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

0.	*	.4	1.2	1.1	1.0	2.1	2.3	2.3	.4
5.	*	.2	.9	.8	.8	2.5	2.6	2.6	.6
10.	*	.1	.6	.6	.5	2.5	2.6	2.6	.7
15.	*	.0	.3	.3	.3	2.5	2.6	2.5	.7
20.	*	.0	.1	.1	.1	2.4	2.4	2.4	.7
25.	*	.0	.0	.0	.0	2.3	2.3	2.1	.7
30.	*	.1	.1	.0	.0	2.2	2.2	2.0	.7
35.	*	.2	.1	.1	.1	2.0	2.1	1.9	.6
40.	*	.2	.1	.1	.1	2.0	2.0	1.8	.8
45.	*	.2	.1	.1	.1	1.9	1.9	1.6	.8
50.	*	.2	.1	.1	.1	1.8	1.8	1.5	.8
55.	*	.2	.1	.1	.1	1.8	1.8	1.5	.8
60.	*	.3	.2	.1	.1	1.7	1.7	1.4	.8
65.	*	.2	.2	.1	.1	1.7	1.7	1.3	.7
70.	*	.2	.2	.1	.1	1.7	1.7	1.3	.7
75.	*	.3	.3	.1	.1	1.7	1.7	1.3	.9
80.	*	.4	.4	.1	.1	1.7	1.7	1.3	.9
85.	*	.5	.5	.1	.1	1.7	1.7	1.3	1.1
90.	*	.6	.7	.1	.1	1.7	1.6	1.4	1.3
95.	*	.7	.7	.1	.1	1.6	1.7	1.4	1.4
100.	*	.7	.7	.1	.0	1.6	1.8	1.2	1.5
105.	*	.8	.6	.2	.1	1.7	1.8	1.2	1.6
110.	*	.7	.6	.2	.1	1.7	1.7	1.3	1.7
115.	*	.5	.6	.1	.1	1.6	1.8	1.3	1.7
120.	*	.5	.5	.2	.0	1.7	1.8	1.2	2.0
125.	*	.5	.5	.2	.1	1.8	1.9	1.3	1.9
130.	*	.6	.5	.2	.1	1.8	1.9	1.3	1.9
135.	*	.6	.5	.2	.1	1.9	1.9	1.4	1.9
140.	*	.4	.4	.2	.1	2.0	2.0	1.5	2.0
145.	*	.4	.4	.2	.1	2.2	2.1	1.5	2.0
150.	*	.4	.4	.2	.1	2.3	2.1	1.8	1.9
155.	*	.4	.5	.3	.1	2.3	2.3	2.0	1.8
160.	*	.4	.6	.3	.2	2.5	2.5	2.1	1.8
165.	*	.4	.8	.6	.4	2.7	2.6	2.1	1.7

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37

REC38 REC39 REC40

LINK #	* 345	285	255	255	220	210	160	5	255	230	95	250	250	265	215	15	260	260	255	265	
1 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1
2 *	.0	.1	.1	.1	.0	.0	.0	.1	.0	.0	.1	.3	.0	.0	.3	.3	.2	.5	.5	.5	.5
3 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.3	.6	.5	.5	.5	.5
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.4	.0	.1	.0	.0	.4	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.2	.2	.4	.2	.1	.0	.6	.5	.5	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.0	.1	.1	.2	.1	.1	.0	.5	.6	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
8 *	.3	.3	.3	.1	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.1	.1	.0	.2	.0	.0	.1	.1	.1	.1	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.1	.0	.1
13 *	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.0	.0	.1	.0	.0	.1
14 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.4	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.1	.0	.0	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.1	.0	.0	.1	.1	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.6	.1	.0	.1	.4	.5	1.3	1.7	.0	.0	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

LINK #	* 265	260	225	190	165	5	5	120
1 *	.2	.5	.2	.1	.1	.0	.0	.7
2 *	.6	.8	.3	.1	.0	.0	.0	.8
3 *	.4	.2	.0	.1	.1	.0	.0	.1
4 *	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.0	.0	.0	.0	.0	.0	.0	.0
8 *	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.3	.3	.0	.0	.2
11 *	.0	.1	.1	.2	.1	.1	.1	.0
12 *	.1	.3	.4	.3	.7	.8	.8	.0
13 *	.1	.1	.7	.5	1.3	1.7	1.7	.0
14 *	.1	.0	.0	.1	.1	.0	.0	.2
15 *	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0

1

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	* X2	Y2	* (FT) (DEG)	* LENGTH (G/M)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 EB 5th Phil Appr	* 269695.0	284787.0	269838.0	284789.0	* 143.	89. AG	9801.	1.5	.0	44.0				
2. 2 EB 5th EB Queue	* 269805.0	284789.0	265181.1	284730.5	* 4624.	269. AG	228.	100.0	.0	24.0	8.03	234.9		

3. 3 EB 5th Bake Appr	* 269838.0	284789.0	270093.0	284793.0	*	255.	89. AG	1070.	11.5	.0	44.0
4. 4 EB 5th Bake LT	* 270093.0	284793.0	270194.0	284795.0	*	101.	89. AG	1040.	11.5	.0	44.0
5. 5 EB 5th EB Rt	* 270093.0	284776.0	270189.0	284778.0	*	96.	89. AG	30.	11.5	.0	44.0
6. 6 EB 5th Main Appr	* 270194.0	284795.0	270550.0	284799.0	*	356.	89. AG	1340.	11.5	.0	44.0
7. 7 EB 5th EB Queue	* 270491.0	284798.0	263751.5	284734.4	*	6740.	269. AG	255.100.0	.0	24.0	**** 342.4
8. 8 EB 5th Main Dep	* 270550.0	284799.0	270695.0	284801.0	*	145.	89. AG	1070.	11.5	.0	44.0
9. 9 NB Phil 5th Appr	* 269851.0	284462.0	269847.0	284786.0	*	324.	359. AG	660.	11.5	.0	44.0
10. 10 NB PhilNB Queue	* 269848.0	284750.0	269883.7	281964.0	*	2786.	179. AG	202.100.0	.0	24.0	4.58 141.5
11. 11 NB Phil5th Dep	* 269847.0	284786.0	269841.0	285143.0	*	357.	359. AG	180.	11.5	.0	44.0
12. 12 SB Phil5th Appr	* 269823.0	285126.0	269830.0	284793.0	*	333.	179. AG	290.	11.5	.0	44.0
13. 13 SB PhilSB Queue	* 269829.0	284819.0	269815.2	285912.0	*	1093.	359. AG	202.100.0	.0	24.0	3.09 55.5
14. 14 SB PhilPhil Dep	* 269830.0	284793.0	269835.0	284461.0	*	332.	179. AG	180.	11.5	.0	44.0
15. 15 NB Park5th Appr	* 270203.0	284576.0	270200.0	284791.0	*	215.	359. AG	30.	11.5	.0	32.0
16. 16 NB ParkNB Queue	* 270201.0	284761.0	270201.4	284737.6	*	23.	179. AG	98.100.0	.0	12.0	.94 1.2
17. 17 NB Bake5th Dep	* 270200.0	284791.0	270194.0	285216.0	*	425.	359. AG	200.	11.5	.0	32.0
18. 18 SB Bake5th Appr	* 270180.0	285216.0	270189.0	284778.0	*	438.	179. AG	150.	11.5	.0	32.0
19. 19 SB BakeSB Queue	* 270188.0	284828.0	270165.3	286136.0	*	1308.	359. AG	98.100.0	.0	12.0	4.69 66.5
20. 20 SB BakeBake Dep	* 270189.0	284778.0	270192.0	284577.0	*	201.	179. AG	70.	11.5	.0	32.0
21. 21 NB MainMain Appr	* 270564.0	284513.0	270559.0	284795.0	*	282.	359. AG	140.	11.5	.0	32.0
22. 22 NB MainNB Queue	* 270560.0	284768.0	270560.4	284738.2	*	30.	179. AG	128.100.0	.0	12.0	.27 1.5
23. 23 NB MainMain Dep	* 270559.0	284795.0	270556.0	285029.0	*	234.	359. AG	430.	11.5	.0	32.0
24. 24 SB MainMain Appr	* 270535.0	285030.0	270539.0	284802.0	*	228.	179. AG	150.	11.5	.0	44.0
25. 25 SB MainSB Queue	* 270538.0	284828.0	270537.8	284844.0	*	16.	359. AG	256.100.0	.0	24.0	.17 .8
26. 26 SB MainMain Dep	* 270539.0	284802.0	270543.0	284513.0	*	289.	179. AG	130.	11.5	.0	44.0

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:07:59.62

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
2. 2 EB 5th EB Queue	* 60	35	2.0	980	176	73.00	1	3
7. 7 EB 5th EB Queue	* 60	39	2.0	1340	170	73.00	1	3
10. 10 NB PhilNB Queue	* 60	31	2.0	660	173	73.00	1	3
13. 13 SB PhilSB Queue	* 60	31	2.0	290	114	73.00	1	3
16. 16 NB ParkNB Queue	* 40	20	2.0	30	80	73.00	1	3
19. 19 SB BakeSB Queue	* 40	20	2.0	150	80	73.00	1	3
22. 22 NB MainNB Queue	* 60	39	2.0	140	1863	73.30	1	3
25. 25 SB MainSB Queue	* 60	39	2.0	150	1535	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* Z
	* X Y	
1. R1 EB 82	* 269739.0 284764.0	5.0 *
2. R2 SW Corner	* 269811.0 284765.0	5.0 *
3. R3 SB 82	* 269812.0 284693.0	5.0 *
4. R4 SB 164	* 269813.0 284611.0	5.0 *
5. R5 NB 164	* 269868.0 284612.0	5.0 *
6. R6 NB 82	* 269867.0 284694.0	5.0 *
7. R7 SE Corner	* 269866.0 284766.0	5.0 *
8. R8 EB 82	* 269938.0 284768.0	5.0 *
9. R9 EB 164	* 270018.0 284770.0	5.0 *
10. R10 EB 82	* 270099.0 284760.0	5.0 *
11. R10 SW Corner	* 270171.0 284761.0	5.0 *
12. R12 SE Corner	* 270217.0 284772.0	5.0 *
13. R13 EB 82r	* 270289.0 284773.0	5.0 *
14. R14 EB 164	* 270368.0 284774.0	5.0 *
15. R15 EB 82	* 270447.0 284775.0	5.0 *
16. R16 SW Corner	* 270519.0 284776.0	5.0 *
17. R17 SB 82	* 270520.0 284704.0	5.0 *
18. R18 SB 164	* 270521.0 284622.0	5.0 *
19. R19 NB 164	* 270583.0 284618.0	5.0 *
20. R20 NB 82	* 270581.0 284700.0	5.0 *
21. R21 SE Corner	* 270580.0 284773.0	5.0 *
22. R22 SB 82	* 270652.0 284773.0	5.0 *
23. R23 WB 82	* 270652.0 284829.0	5.0 *
24. R24 NE Corner	* 270580.0 284829.0	5.0 *
25. R25 NB 82	* 270579.0 284901.0	5.0 *
26. R26 NB 164	* 270577.0 284983.0	5.0 *
27. R27 SB 164	* 270525.0 284975.0	5.0 *
28. R28 SB 82	* 270527.0 284893.0	5.0 *
29. R29 NW Corner	* 270518.0 284821.0	5.0 *
30. R30 WB 82	* 270446.0 284821.0	5.0 *
31. R31 WB 164	* 270368.0 284820.0	5.0 *
32. R32 WB 82	* 270288.0 284819.0	5.0 *
33. R33 NE Corner	* 270216.0 284818.0	5.0 *
34. R34 NB 82	* 270215.0 284890.0	5.0 *
35. R35 NB 164	* 270214.0 284972.0	5.0 *
36. R36 SB 164	* 270168.0 284972.0	5.0 *
37. R37 SB 82	* 270169.0 284890.0	5.0 *

1

JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:07:59.62

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* Z
	* X Y	
38. R38 NW Corner	* 270170.0 284818.0	5.0 *

39. R39 WB 82 * 270098.0 284817.0 5.0 *
 40. R40 WB 164 * 270017.0 284815.0 5.0 *
 41. R41 WB 82 * 269937.0 284814.0 5.0 *
 42. R42 NE Corner * 269865.0 284813.0 5.0 *
 43. R43 NB 82 * 269864.0 284885.0 5.0 *
 44. R44 NB 164 * 269863.0 284967.0 5.0 *
 45. R45 SB 164 * 269809.0 284966.0 5.0 *
 46. R46 SB 82 * 269810.0 284884.0 5.0 *
 47. R47 NW Corner * 269811.0 284812.0 5.0 *
 48. R48 WB 82 * 269738.0 284810.0 5.0 *

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	*	2.0	2.0	1.2	1.0	1.3	1.3	1.8	1.2	1.1	1.0	1.3	1.5	1.3	1.2	1.2	.8	.3	.2	.1	.4	
5.	*	2.0	2.2	1.3	1.1	1.1	1.0	1.6	1.2	1.2	1.1	1.3	1.4	1.2	1.2	1.2	.8	.4	.2	.1	.3	
10.	*	2.1	2.1	1.3	1.2	.8	1.0	1.4	1.1	1.2	1.0	1.3	1.4	1.2	1.2	1.2	.8	.5	.3	.1	.2	
15.	*	2.1	2.0	1.2	1.1	.7	.7	1.3	1.2	1.2	1.0	1.4	1.2	1.2	1.2	1.2	.8	.4	.2	.1	.2	
20.	*	2.1	1.8	1.1	1.1	.6	.6	1.1	1.2	1.2	1.0	1.3	1.2	1.2	1.2	1.2	.8	.5	.2	.1	.2	
25.	*	2.2	1.8	1.1	1.1	.5	.7	1.2	1.2	1.2	1.0	1.3	1.2	1.2	1.2	1.2	.8	.5	.2	.1	.2	
30.	*	2.3	1.7	1.1	1.1	.5	.7	1.2	1.2	1.2	1.0	1.3	1.3	1.3	1.3	1.3	.8	.3	.2	.1	.2	
35.	*	2.3	1.6	1.1	1.1	.4	.6	1.2	1.2	1.3	1.1	1.0	1.4	1.3	1.4	1.4	.8	.4	.2	.0	.2	
40.	*	2.3	1.7	1.2	1.1	.3	.5	1.3	1.4	1.4	1.1	1.1	1.4	1.4	1.4	1.5	.8	.4	.2	.0	.1	
45.	*	2.4	1.6	1.2	1.1	.3	.5	1.3	1.4	1.4	1.2	1.1	1.4	1.4	1.4	1.4	.7	.4	.2	.0	.1	
50.	*	2.3	1.5	1.2	1.1	.3	.5	1.3	1.4	1.5	1.3	1.2	1.5	1.5	1.5	1.5	.7	.4	.1	.0	.1	
55.	*	2.3	1.6	1.3	1.1	.3	.6	1.3	1.5	1.6	1.2	1.2	1.6	1.6	1.6	1.6	1.5	.7	.3	.1	.0	.1
60.	*	2.3	1.7	1.3	1.1	.3	.6	1.5	1.5	1.7	1.2	1.3	1.6	1.6	1.6	1.6	1.5	.8	.3	.1	.0	.0
65.	*	2.3	1.8	1.3	1.0	.3	.6	1.5	1.6	1.7	1.2	1.3	1.8	1.6	1.6	1.6	1.3	.7	.1	.0	.0	.0
70.	*	2.4	1.8	1.3	1.0	.3	.5	1.6	1.8	1.8	1.4	1.2	1.8	1.7	1.6	1.1	.8	.1	.0	.0	.0	.0
75.	*	2.1	2.0	1.2	.9	.2	.5	1.7	1.8	1.7	1.3	1.2	1.7	1.7	1.5	1.1	.8	.0	.0	.0	.0	.0
80.	*	2.1	1.9	1.2	.9	.2	.3	1.7	1.6	1.7	1.1	1.2	1.6	1.7	1.4	1.0	.8	.1	.1	.0	.0	.0
85.	*	1.8	1.8	1.0	.8	.0	.3	1.5	1.5	1.6	.9	1.0	1.4	1.4	1.2	.8	.6	.1	.1	.0	.0	.0
90.	*	1.7	1.4	.9	.7	.0	.2	1.1	1.3	1.3	.7	.8	1.1	1.2	.9	.6	.7	.1	.1	.0	.0	.0
95.	*	1.3	1.4	.8	.7	.0	.1	.9	1.0	.9	.6	.5	.9	.7	.7	.4	.6	.1	.1	.0	.0	.0
100.	*	.8	1.0	.7	.7	.0	.0	.6	.6	.7	.3	.3	.5	.5	.4	.3	.4	.1	.1	.0	.0	.0
105.	*	.7	.8	.7	.7	.0	.0	.4	.3	.4	.2	.3	.3	.3	.2	.4	.0	.0	.0	.0	.0	.0
110.	*	.5	.7	.7	.7	.0	.0	.2	.2	.2	.0	.1	.2	.2	.1	.1	.3	.0	.0	.0	.0	.0
115.	*	.4	.5	.7	.7	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.2	.1	.0	.0	.0	.0	.0
120.	*	.4	.6	.8	.8	.0	.0	.1	.1	.1	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0
125.	*	.3	.6	.8	.8	.0	.0	.0	.0	.1	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0
130.	*	.3	.7	.8	.8	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0
135.	*	.3	.7	.8	.8	.0	.0	.0	.0	.0	.1	.0	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0
140.	*	.4	.8	.8	.8	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0
145.	*	.4	.9	.9	.8	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0
150.	*	.4	1.0	1.0	.9	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
155.	*	.4	1.0	1.0	.9	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
160.	*	.4	1.0	1.0	.9	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
165.	*	.3	1.1	1.0	1.0	.5	.5	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
170.	*	.3	1.0	1.0	.9	.7	.7	.8	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
175.	*	.3	.9	.9	.8	1.0	1.0	1.0	.2	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
180.	*	.2	.7	.7	.7	1.2	1.3	1.3	.3	.1	.1	.1	.0	.0	.0	.1	.1	.1	.0	.0	.1	.1
185.	*	.1	.6	.6	.4	1.5	1.5	1.5	.3	.2	.1	.1	.2	.1	.0	.0	.1	.0	.0	.0	.1	.1
190.	*	.1	.4	.3	.2	1.5	1.6	1.5	.5	.2	.2	.1	.2	.1	.1	.0	.0	.0	.0	.1	.1	.1
195.	*	.0	.1	.1	.1	1.6	1.6	1.5	.5	.2	.2	.1	.2	.1	.1	.1	.1	.1	.1	.1	.1	.1
200.	*	.0	.0	.0	.0	1.5	1.5	1.3	.4	.2	.2	.1	.2	.1	.1	.1	.1	.1	.1	.1	.2	.2
205.	*	.0	.0	.0	.0	1.5	1.5	1.2	.4	.2	.2	.1	.3	.1	.1	.1	.1	.1	.1	.2	.2	.2

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

210.	*	.0	.0	.0	.0	1.4	1.4	1.1	.4	.2	.2	.1	.3	.1	.1	.1	.1	.1	.1	.2	.2
215.	*	.0	.0	.0	.0	1.2	1.3	1.1	.4	.3	.2	.1	.3	.1	.1	.1	.1	.1	.1	.2	.2
220.	*	.0	.0	.0	.0	1.2	1.2	.9	.4	.3	.1	.1	.3	.1	.1	.1	.1	.1	.1	.2	.2
225.	*	.0	.0	.0	.0	1.2	1.2	.8	.4	.3	.1	.1	.3	.2	.2	.2	.2	.1	.1	.2	.2
230.	*	.0	.0	.0	.0	1.1	1.1	.7	.4	.4	.1	.1	.2	.2	.2	.2	.2	.1	.1	.2	.2
235.	*	.0	.1	.0	.0	1.1	1.1	.7	.4	.4	.2	.1	.2	.2	.2	.2	.2	.1	.1	.2	.2
240.	*	.0	.1	.0	.0	1.1	1.1	.6	.4	.4	.2	.1	.2	.2	.2	.2	.2	.1	.1	.2	.2
245.	*	.1	.2	.0	.0	1.1	1.1	.6	.5	.5	.2	.1	.3	.3	.3	.3	.3	.1	.1	.2	.2
250.	*	.3	.3	.0	.0	1.1	1.1	.8	.6	.5	.3	.2	.4	.3	.3	.4	.4	.1	.1	.2	.2
255.	*	.5	.6	.0	.0	1.0	1.0	1.0	.9	.8	.6	.5	.7	.7	.7	.7	.8	.2	.1	.2	.2
260.	*	.9	1.0	.2	.2	1.2	1.2	1.6	1.3	1.4	.8	.8	1.1	1.1	1.1	1.1	1.0	.3	.2	.3	.4
265.	*	1.6	1.7	.4	.2	1.3	1.5	2.1	1.8	1.9	1.3	1.0	1.5	1.5	1.6	1.6	1.5	.4	.3	.4	.4
270.	*	2.0	2.2	.6	.4	1.5	1.7	2.4	2.2	2.1	1.6	1.5	1.8	1.8	1.9	1.9	1.9	.6	.4	.5	.6
275.	*	2.3	2.5	.8	.5	1.6	1.9	2.8	2.3	2.1	1.6	1.6	2.1	2.0	2.1	2.2	2.1	.7	.5	.6	.8
280.	*	2.3	2.7	.8	.6	1.6	1.8	2.8	2.4	2.3	1.8	1.7	2.2	2.2	2.3	2.2	2.0	.7	.5	.5	.7
285.	*	2.3	2.6	.8	.6	1.6	1.8	2.6	2.2	2.1	1.7	1.5	1.9	2.2	2.3	2.2	2.0	.8	.4	.5	.8
290.	*	2.3	2.5	.8	.5	1.5	1.9	2.3	1.9	2.0	1.5	1.5	1.9	2.0	1.9	2.0	1.8	.7	.5	.6	.8
295.	*	2.2	2.4	.8	.5	1.6	2.0	2.0	1.8	1.8	1.3	1.4	1.7	1.8	1.8	1.8	1.6	.7	.5	.6	.8

300. * 2.1 2.3 .8 .4 1.5 1.9 2.0 1.7 1.6 1.2 1.2 1.7 1.9 1.9 1.8 1.4 .7 .5 .5 .7
 305. * 2.0 2.2 .8 .4 1.5 2.0 1.9 1.6 1.6 1.2 1.2 1.6 1.7 1.8 1.8 1.3 .7 .4 .5 .7
 310. * 2.1 2.1 .7 .4 1.6 1.9 1.9 1.5 1.6 1.2 1.3 1.6 1.7 1.7 1.7 1.1 .6 .4 .5 .6
 315. * 2.0 2.1 .8 .4 1.7 1.8 1.8 1.5 1.5 1.2 1.2 1.5 1.6 1.6 1.7 1.0 .6 .4 .6 .7
 320. * 1.9 1.8 .8 .5 1.7 1.8 1.7 1.5 1.5 1.0 1.1 1.8 1.6 1.6 1.6 .9 .6 .4 .5 .6
 325. * 1.9 1.8 .8 .5 1.8 1.9 1.8 1.4 1.4 1.0 1.1 1.7 1.5 1.5 1.5 .8 .7 .5 .4 .5
 330. * 1.9 1.7 .8 .5 1.8 1.8 1.9 1.4 1.3 1.1 1.0 1.6 1.5 1.5 1.4 .7 .6 .4 .3 .5
 335. * 1.8 1.8 .8 .5 1.9 1.9 2.0 1.4 1.3 1.1 1.0 1.7 1.4 1.3 1.3 .6 .5 .4 .3 .4
 340. * 1.8 1.7 .8 .6 1.9 1.9 1.9 1.4 1.3 1.0 1.0 1.7 1.3 1.3 1.3 .5 .4 .3 .3 .5
 345. * 1.8 1.8 .9 .5 1.9 1.7 2.0 1.4 1.3 1.0 1.1 1.6 1.3 1.3 1.2 .5 .3 .2 .2 .5
 350. * 1.9 2.0 1.0 .7 1.8 1.7 2.0 1.3 1.2 1.1 1.0 1.6 1.3 1.3 1.2 .5 .3 .2 .3 .5
 355. * 1.9 2.0 1.1 .9 1.7 1.5 1.9 1.3 1.2 1.0 1.2 1.6 1.3 1.2 1.2 .6 .3 .3 .3 .3
 360. * 2.0 2.0 1.2 1.0 1.3 1.3 1.8 1.2 1.1 1.0 1.3 1.5 1.3 1.2 1.2 .8 .3 .2 .1 .4

MAX * 2.4 2.7 1.3 1.2 1.9 2.0 2.8 2.4 2.3 1.8 1.7 2.2 2.2 2.3 2.2 2.1 .8 .5 .6 .8
 DEGR. * 70 280 5 10 335 295 275 280 280 280 280 280 285 280 275 275 285 275 275 275

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

0. * .5 .4 .0 .1 .1 .1 .1 .2 .1 .0 .0 .1 .3 .3 .3 .4 .4 .5 .1 .0
 5. * .5 .4 .0 .1 .1 .0 .1 .2 .3 .0 .0 .0 .3 .2 .2 .6 .6 .6 .1 .1
 10. * .5 .4 .0 .1 .0 .0 .1 .2 .3 .0 .0 .0 .2 .2 .2 .6 .6 .6 .1 .1
 15. * .4 .4 .0 .0 .0 .0 .1 .2 .4 .0 .0 .0 .0 .0 .0 .6 .6 .6 .1 .1
 20. * .4 .4 .0 .0 .0 .0 .2 .2 .4 .0 .0 .0 .0 .0 .0 .6 .6 .6 .1 .1
 25. * .4 .4 .0 .0 .0 .0 .2 .3 .5 .0 .0 .0 .0 .0 .0 .5 .5 .5 .1 .1
 30. * .4 .4 .0 .0 .0 .0 .2 .3 .5 .0 .0 .0 .0 .0 .0 .5 .5 .5 .1 .1
 35. * .4 .4 .0 .0 .0 .0 .2 .3 .5 .0 .0 .0 .0 .0 .0 .5 .5 .5 .1 .1
 40. * .4 .4 .0 .0 .0 .0 .2 .3 .6 .1 .0 .0 .0 .0 .0 .5 .5 .4 .1 .1
 45. * .4 .3 .0 .0 .0 .0 .2 .3 .6 .2 .1 .1 .1 .0 .0 .5 .5 .4 .1 .1
 50. * .5 .3 .0 .0 .0 .0 .2 .2 .6 .2 .1 .1 .1 .0 .0 .5 .5 .4 .1 .1
 55. * .5 .3 .0 .0 .0 .0 .2 .2 .6 .2 .1 .1 .1 .0 .0 .5 .5 .4 .1 .1
 60. * .5 .3 .0 .0 .0 .0 .2 .2 .6 .2 .1 .1 .1 .0 .0 .5 .5 .3 .1 .1
 65. * .5 .3 .0 .0 .0 .0 .2 .2 .7 .2 .1 .1 .1 .0 .0 .5 .5 .4 .2 .3
 70. * .5 .2 .0 .0 .0 .0 .2 .2 .8 .3 .1 .3 .3 .0 .0 .5 .5 .5 .4 .3
 75. * .4 .2 .0 .0 .0 .0 .2 .2 .7 .5 .3 .3 .5 .0 .0 .5 .5 .7 .5 .5
 80. * .4 .2 .0 .1 .0 .0 .2 .2 .7 .5 .5 .6 .7 .0 .0 .5 .4 .9 .8 .8
 85. * .3 .1 .1 .1 .0 .0 .2 .2 .8 .6 .7 .9 .9 .0 .0 .5 .4 .1 .2 .9 .1 .1
 90. * .2 .1 .1 .2 .0 .0 .2 .2 .8 .7 1.0 1.2 1.3 .0 .0 .4 .5 1.4 1.3 1.4
 95. * .2 .1 .1 .3 .0 .0 .2 .2 .9 .9 1.2 1.5 1.6 .2 .0 .5 .6 1.7 1.5 1.6
 100. * .1 .0 .2 .3 .0 .0 .2 .2 .9 1.0 1.4 1.7 1.7 .2 .0 .5 .7 1.9 1.7 1.8
 105. * .1 .0 .2 .4 .0 .0 .2 .2 .9 1.0 1.5 1.7 1.8 .4 .0 .5 .9 2.0 1.7 1.8
 110. * .1 .0 .2 .4 .0 .0 .2 .3 .8 1.1 1.5 1.7 1.8 .4 .1 .7 1.0 2.0 1.7 1.7
 115. * .0 .0 .2 .4 .0 .0 .2 .3 .7 1.2 1.6 1.7 1.8 .5 .2 .7 1.0 1.9 1.6 1.8
 120. * .0 .0 .3 .4 .1 .0 .2 .3 .8 1.3 1.6 1.6 1.7 .5 .2 .7 1.0 1.7 1.6 1.6
 125. * .0 .0 .3 .4 .1 .0 .2 .3 .7 1.2 1.6 1.6 1.6 .5 .2 .8 1.1 1.6 1.5 1.6
 130. * .0 .0 .3 .4 .1 .0 .2 .4 .6 1.3 1.5 1.5 1.5 .5 .3 .8 1.0 1.6 1.4 1.4
 135. * .0 .0 .3 .4 .1 .0 .4 .4 .8 1.3 1.4 1.4 1.4 .5 .3 .9 1.0 1.5 1.2 1.4
 140. * .0 .0 .3 .4 .1 .0 .4 .4 .7 1.3 1.4 1.4 1.4 .5 .3 .8 1.0 1.4 1.2 1.2
 145. * .0 .0 .4 .4 .2 .1 .4 .5 .7 1.2 1.3 1.3 1.4 .5 .3 .8 1.0 1.4 1.2 1.2
 150. * .0 .0 .4 .4 .2 .1 .4 .4 .7 1.2 1.3 1.3 1.3 .5 .3 .8 1.0 1.3 1.2 1.2
 155. * .0 .0 .4 .4 .2 .1 .4 .5 .7 1.2 1.2 1.2 1.2 .5 .3 .8 .9 1.3 1.1 1.2
 160. * .0 .0 .4 .4 .2 .1 .3 .5 .7 1.2 1.2 1.2 1.2 .5 .3 .8 .9 1.2 1.1 1.2
 165. * .0 .0 .4 .4 .2 .2 .3 .5 .6 1.2 1.2 1.2 1.2 .5 .3 .8 .8 1.1 1.0 1.2
 170. * .0 .0 .4 .4 .2 .2 .4 .5 .6 1.2 1.2 1.2 1.2 .5 .4 .9 .7 1.1 1.0 1.1
 175. * .0 .0 .4 .4 .3 .2 .3 .5 .6 1.2 1.2 1.2 1.2 .6 .5 .7 .7 1.1 1.1 1.3
 180. * .1 .0 .4 .4 .2 .3 .3 .4 .7 1.2 1.2 1.2 1.2 .6 .5 .7 .7 1.2 1.2 1.3
 185. * .1 .0 .4 .7 .3 .4 .3 .4 .5 1.2 1.2 1.3 1.3 .8 .7 .6 .6 1.2 1.2 1.4
 190. * .2 .0 .4 .7 .4 .4 .3 .5 .5 1.3 1.3 1.4 .8 .8 .5 .6 1.2 1.3 1.4
 195. * .2 .0 .4 .8 .6 .4 .4 .6 .6 1.3 1.3 1.3 1.5 .8 .8 .4 .6 1.2 1.3 1.4
 200. * .3 .1 .5 .6 .6 .5 .4 .4 .6 1.3 1.3 1.3 1.5 .9 .8 .5 .6 1.2 1.2 1.4
 205. * .4 .1 .5 .7 .6 .5 .4 .5 .7 1.3 1.3 1.3 1.4 .8 .8 .5 .5 1.2 1.3 1.4

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

210. * .4 .1 .5 .6 .7 .6 .5 .5 .7 1.4 1.4 1.4 1.5 .9 .8 .4 .6 1.3 1.4 1.5
 215. * .4 .1 .5 .7 .7 .7 .4 .6 .9 1.4 1.4 1.4 1.6 .9 .9 .4 .6 1.3 1.4 1.5
 220. * .4 .1 .5 .7 .8 .7 .5 .6 .9 1.5 1.5 1.5 1.6 .9 .8 .4 .6 1.3 1.4 1.6
 225. * .5 .1 .5 .7 .8 .6 .4 .6 1.0 1.5 1.5 1.6 1.6 1.0 .8 .4 .6 1.3 1.5 1.7
 230. * .5 .1 .5 .8 .8 .6 .4 .7 1.1 1.6 1.6 1.6 1.7 1.1 .8 .4 .6 1.5 1.6 1.7
 235. * .4 .1 .6 1.0 .8 .6 .4 .7 1.3 1.7 1.7 1.6 1.7 1.1 .8 .5 .7 1.6 1.7 1.7
 240. * .4 .1 .7 1.1 .8 .6 .5 .7 1.4 1.8 1.8 1.9 1.1 .8 .5 .7 1.7 1.8 1.8
 245. * .4 .1 .8 1.2 .9 .6 .4 .7 1.7 1.8 1.8 1.8 1.9 1.0 .8 .6 .8 1.7 1.7 2.0
 250. * .6 .2 .9 1.5 .9 .7 .4 .8 1.8 2.0 1.9 2.1 2.1 .9 .9 .6 .6 1.9 1.9 2.2

220. * 1.7 1.8 1.3 1.2 .4 .8 2.0 2.2
 225. * 1.7 1.7 1.3 1.2 .4 .8 2.2 2.2
 230. * 1.7 1.8 1.5 1.1 .4 .8 2.2 2.3
 235. * 1.8 2.0 1.5 1.1 .4 .8 2.4 2.4
 240. * 1.9 2.0 1.5 1.2 .5 .8 2.5 2.4
 245. * 2.0 2.3 1.6 1.2 .5 .8 2.6 2.6
 250. * 2.3 2.6 1.6 1.3 .6 .8 2.8 2.7
 255. * 2.4 2.8 1.6 1.3 .6 .9 2.9 2.7
 260. * 2.3 3.0 1.5 1.3 .6 .9 2.9 2.8
 265. * 2.4 2.8 1.4 1.1 .5 .8 2.7 2.6
 270. * 2.1 2.4 1.2 1.0 .4 .6 2.3 2.2
 275. * 1.6 2.1 1.1 .8 .2 .4 1.7 1.7
 280. * 1.2 1.6 .9 .8 .1 .2 1.1 1.1
 285. * .8 1.1 .7 .7 .0 .0 .6 .6
 290. * .5 .8 .7 .7 .0 .0 .3 .4
 295. * .4 .7 .7 .7 .0 .0 .2 .2
 300. * .2 .6 .7 .7 .0 .0 .1 .1
 305. * .2 .6 .7 .7 .0 .0 .1 .1
 310. * .2 .7 .7 .7 .0 .0 .0 .1
 315. * .2 .7 .7 .7 .0 .0 .0 .1
 320. * .3 .7 .7 .7 .0 .0 .0 .0
 325. * .3 .7 .7 .7 .0 .0 .0 .0
 330. * .3 .8 .8 .8 .0 .0 .0 .0
 335. * .3 .8 .8 .8 .1 .1 .1 .0
 340. * .3 .8 .8 .8 .2 .2 .2 .0
 345. * .3 .8 .8 .8 .4 .4 .4 .0
 350. * .2 .8 .8 .8 .6 .6 .6 .1
 355. * .2 .7 .7 .6 .8 .8 .9 .1
 360. * .1 .6 .5 .5 1.0 1.1 1.1 .2

MAX * 2.4 3.0 1.6 1.4 1.7 1.8 2.9 2.8
 DEGR. * 255 260 245 190 160 155 255 260

THE HIGHEST CONCENTRATION IS 3.00 PPM AT 260 DEGREES FROM REC42.
 THE 2ND HIGHEST CONCENTRATION IS 2.90 PPM AT 255 DEGREES FROM REC47.
 THE 3RD HIGHEST CONCENTRATION IS 2.80 PPM AT 260 DEGREES FROM REC48.

1

JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:07:59.62

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

LINK #	* 70	280	5	10	335	295	275	280	280	280	280	280	285	280	275	275	275
1 *	.6	.6	.2	.1	.1	.1	.4	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0
2 *	.5	1.0	.1	.0	.1	.4	.8	.5	.3	.3	.2	.2	.1	.1	.2	.2	.2
3 *	.2	.0	.0	.1	.0	.0	.2	.5	.6	.4	.3	.2	.1	.1	.1	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3	.1	.1	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.6	.7	.7	.8	.2	.0
7 *	1.0	1.1	.3	.2	.2	.4	1.0	1.1	1.2	.9	.9	1.2	1.2	1.2	1.2	1.1	.5
8 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.1	.2	.4	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.3	.9	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.1	.0	.4	.2	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0
14 *	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:07:59.62

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

LINK #	* 275	270	265	265	245	215	210	250	265	255	260	255	260	265	215	135	125	255	255	255	
1 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
2 *	.2	.2	.2	.2	.0	.0	.0	.1	.2	.1	.2	.3	.0	.0	.0	.1	.2	.2	.0	.0	.0
3 *	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.1	.1	.0	.0	.3	.6	.6	.0	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.3	.0	.1	.0	.0	.4	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.5	.3	.3	.5	.2	.1	.2	.2	.8	.8	.7	.6	.2	.0	.0	.2	.3	.0	.0	.0	.0

```

7 * .8 .6 .6 .7 .4 .2 .2 .4 1.1 1.2 1.2 1.2 1.2 .4 .2 .2 .3 1.2 1.2 1.2
8 * .1 .2 .2 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
9 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
10 * .0 .0 .0 .0 .1 .1 .1 .1 .0 .1 .0 .1 .0 .0 .1 .0 .0 .1 .1 .1
11 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
12 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
13 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0
14 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
15 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
16 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
17 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .1 .1 .1 .1 .0 .0 .0
18 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .1 .1 .1 .0 .0 .0 .0
19 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2 .2 .3 .3 .0 .0 .0 .0
20 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
21 * .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
22 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
23 * .0 .0 .1 .2 .2 .2 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
24 * .0 .0 .0 .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
25 * .0 .0 .0 .2 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
26 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

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JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 11:07:59.62

RUN: W 5th Street & Bakewell

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48
LINK # * 255 260 245 190 160 155 255 260

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1 * .2 .4 .1 .1 .0 .1 .6 .3
2 * .4 .8 .4 .1 .0 .0 1.0 1.1
3 * .5 .2 .0 .1 .1 .1 .0 .0
4 * .0 .0 .0 .0 .0 .0 .0 .0
5 * .0 .0 .0 .0 .0 .0 .0 .0
6 * .0 .0 .0 .0 .0 .0 .0 .0
7 * 1.2 1.3 .4 .2 .2 .3 1.3 1.4
8 * .0 .0 .0 .0 .0 .0 .0 .0
9 * .1 .0 .0 .1 .1 .1 .0 .0
10 * .0 .0 .0 .3 .1 .2 .0 .0
11 * .0 .1 .1 .1 .1 .1 .0 .0
12 * .0 .1 .1 .1 .2 .2 .0 .0
13 * .0 .1 .5 .3 .9 .7 .0 .0
14 * .0 .0 .0 .0 .0 .0 .0 .0
15 * .0 .0 .0 .0 .0 .0 .0 .0
16 * .0 .0 .0 .0 .0 .0 .0 .0
17 * .0 .0 .0 .0 .0 .0 .0 .0
18 * .0 .0 .0 .0 .0 .0 .0 .0
19 * .0 .0 .0 .0 .0 .0 .0 .0
20 * .0 .0 .0 .0 .0 .0 .0 .0
21 * .0 .0 .0 .0 .0 .0 .0 .0
22 * .0 .0 .0 .0 .0 .0 .0 .0
23 * .0 .0 .0 .0 .0 .0 .0 .0
24 * .0 .0 .0 .0 .0 .0 .0 .0
25 * .0 .0 .0 .0 .0 .0 .0 .0
26 * .0 .0 .0 .0 .0 .0 .0 .0

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1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 11:27:13.00

RUN: W 5th Street & Bakewell

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	* Y2	(FT)	(DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH	EF	H	W	V/C	QUEUE
1. 1 EB 5th Phil Appr	* 269695.0	284787.0	269838.0	284789.0	*		143.	89.	AG	7701.	1.5	.0	44.0		
2. 2 EB 5th EB Queue	* 269805.0	284789.0	269247.3	284782.0	*		558.	269.	AG	288.	100.0	.0	24.0	1.11	28.3
3. 3 EB 5th Bake Appr	* 269838.0	284789.0	270093.0	284793.0	*		255.	89.	AG	720.	11.5	.0	44.0		
4. 4 EB 5th Bake LT	* 270093.0	284793.0	270194.0	284795.0	*		101.	89.	AG	710.	11.5	.0	44.0		
5. 5 EB 5th EB Rt	* 270093.0	284776.0	270189.0	284778.0	*		96.	89.	AG	10.	11.5	.0	44.0		
6. 6 EB 5th Main Appr	* 270194.0	284795.0	270550.0	284799.0	*		356.	89.	AG	960.	11.5	.0	44.0		
7. 7 EB 5th EB Queue	* 270491.0	284798.0	270409.6	284797.2	*		81.	269.	AG	203.	100.0	.0	24.0	.66	4.1
8. 8 EB 5th Main Dep	* 270550.0	284799.0	270695.0	284801.0	*		145.	89.	AG	720.	11.5	.0	44.0		
9. 9 NB Phil 5th Appr	* 269851.0	284462.0	269847.0	284786.0	*		324.	359.	AG	410.	11.5	.0	44.0		
10. 10 NB PhilNB Queue	* 269848.0	284750.0	269848.3	284724.2	*		26.	179.	AG	151.	100.0	.0	24.0	.22	1.3
11. 11 NB Phil5th Dep	* 269847.0	284786.0	269841.0	285143.0	*		357.	359.	AG	320.	11.5	.0	44.0		
12. 12 SB Phil5th Appr	* 269823.0	285126.0	269830.0	284793.0	*		333.	179.	AG	1390.	11.5	.0	44.0		
13. 13 SB PhilSB Queue	* 269829.0	284819.0	269780.1	288686.3	*		3868.	359.	AG	151.	100.0	.0	24.0	2.11	196.5
14. 14 SB PhilPhil Dep	* 269830.0	284793.0	269835.0	284461.0	*		332.	179.	AG	1120.	11.5	.0	44.0		
15. 15 NB Park5th Appr	* 270203.0	284576.0	270200.0	284791.0	*		215.	359.	AG	70.	11.5	.0	32.0		
16. 16 NB ParkNB Queue	* 270201.0	284761.0	270201.1	284753.3	*		8.	179.	AG	98.	100.0	.0	12.0	.22	.4
17. 17 NB Bake5th Dep	* 270200.0	284791.0	270194.0	285216.0	*		425.	359.	AG	140.	11.5	.0	32.0		
18. 18 SB Bake5th Appr	* 270180.0	285216.0	270189.0	284778.0	*		438.	179.	AG	140.	11.5	.0	32.0		
19. 19 SB BakeSB Queue	* 270188.0	284828.0	270187.8	284843.3	*		15.	359.	AG	98.	100.0	.0	12.0	.44	.8
20. 20 SB BakeBake Dep	* 270189.0	284778.0	270192.0	284577.0	*		201.	179.	AG	70.	11.5	.0	32.0		
21. 21 NB MainMain Appr	* 270564.0	284513.0	270559.0	284795.0	*		282.	359.	AG	170.	11.5	.0	32.0		
22. 22 NB MainNB Queue	* 270560.0	284768.0	270560.4	284734.6	*		33.	179.	AG	118.	100.0	.0	12.0	.27	1.7

23. 23 NB MainMain Dep * 270559.0 284795.0 270556.0 285029.0 * 234. 359. AG 470. 11.5 .0 44.0
 24. 24 SB MainMain Appr * 270535.0 285030.0 270539.0 284802.0 * 228. 179. AG 180. 11.5 .0 44.0
 25. 25 SB MainSB Queue * 270538.0 284828.0 270537.8 284845.7 * 18. 359. AG 236. 100.0 .0 24.0 .18 .9
 26. 26 SB MainMain Dep * 270539.0 284802.0 270543.0 284513.0 * 289. 179. AG 120. 11.5 .0 44.0

1

JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:27:13.00

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE (SEC)	APPROACH (VPH)	SATURATION (VPH)	IDLE (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
2. 2 EB 5th EB Queue	* 60	44	2.0	770	1743	73.30	1 3	
7. 7 EB 5th EB Queue	* 60	31	2.0	960	1743	73.30	1 3	
10. 10 NB PhilNB Queue	* 60	23	2.0	410	1731	73.30	1 3	
13. 13 SB PhilSB Queue	* 60	23	2.0	1390	600	73.30	1 3	
16. 16 NB ParkNB Queue	* 40	20	2.0	70	800	73.30	1 3	
19. 19 SB BakeSB Queue	* 40	20	2.0	140	800	73.30	1 3	
22. 22 NB MainNB Queue	* 60	36	2.0	170	1866	73.30	1 3	
25. 25 SB MainSB Queue	* 60	36	2.0	180	1483	73.30	1 3	

RECEPTOR LOCATIONS

RECEPTOR	* X	COORDINATES (FT) Y	Z	* 5.0 *
1. R1 EB 82	* 269739.0	284764.0		5.0 *
2. R2 SW Corner	* 269811.0	284765.0		5.0 *
3. R3 SB 82	* 269812.0	284693.0		5.0 *
4. R4 SB 164	* 269813.0	284611.0		5.0 *
5. R5 NB 164	* 269868.0	284612.0		5.0 *
6. R6 NB 82	* 269867.0	284694.0		5.0 *
7. R7 SE Corner	* 269866.0	284766.0		5.0 *
8. R8 EB 82	* 269938.0	284768.0		5.0 *
9. R9 EB 164	* 270018.0	284770.0		5.0 *
10. R10 EB 82	* 270099.0	284760.0		5.0 *
11. R10 SW Corner	* 270171.0	284761.0		5.0 *
12. R12 SE Corner	* 270217.0	284772.0		5.0 *
13. R13 EB 82r	* 270289.0	284773.0		5.0 *
14. R14 EB 164	* 270368.0	284774.0		5.0 *
15. R15 EB 82	* 270447.0	284775.0		5.0 *
16. R16 SW Corner	* 270519.0	284776.0		5.0 *
17. R17 SB 82	* 270520.0	284704.0		5.0 *
18. R18 SB 164	* 270521.0	284622.0		5.0 *
19. R19 NB 164	* 270583.0	284618.0		5.0 *
20. R20 NB 82	* 270581.0	284700.0		5.0 *
21. R21 SE Corner	* 270580.0	284773.0		5.0 *
22. R22 SB 82	* 270652.0	284773.0		5.0 *
23. R23 WB 82	* 270652.0	284829.0		5.0 *
24. R24 NE Corner	* 270580.0	284829.0		5.0 *
25. R25 NB 82	* 270579.0	284901.0		5.0 *
26. R26 NB 164	* 270577.0	284983.0		5.0 *
27. R27 SB 164	* 270525.0	284975.0		5.0 *
28. R28 SB 82	* 270527.0	284893.0		5.0 *
29. R29 NW Corner	* 270518.0	284821.0		5.0 *
30. R30 WB 82	* 270446.0	284821.0		5.0 *
31. R31 WB 164	* 270368.0	284820.0		5.0 *
32. R32 WB 82	* 270288.0	284819.0		5.0 *
33. R33 NE Corner	* 270216.0	284818.0		5.0 *
34. R34 NB 82	* 270215.0	284890.0		5.0 *
35. R35 NB 164	* 270214.0	284972.0		5.0 *
36. R36 SB 164	* 270168.0	284972.0		5.0 *
37. R37 SB 82	* 270169.0	284890.0		5.0 *

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 11:27:13.00

RECEPTOR LOCATIONS

RECEPTOR	* X	COORDINATES (FT) Y	Z	* 5.0 *
38. R38 NW Corner	* 270170.0	284818.0		5.0 *
39. R39 WB 82	* 270098.0	284817.0		5.0 *
40. R40 WB 164	* 270017.0	284815.0		5.0 *
41. R41 WB 82	* 269937.0	284814.0		5.0 *
42. R42 NE Corner	* 269865.0	284813.0		5.0 *
43. R43 NB 82	* 269864.0	284885.0		5.0 *
44. R44 NB 164	* 269863.0	284967.0		5.0 *
45. R45 SB 164	* 269809.0	284966.0		5.0 *
46. R46 SB 82	* 269810.0	284884.0		5.0 *
47. R47 NW Corner	* 269811.0	284812.0		5.0 *
48. R48 WB 82	* 269738.0	284810.0		5.0 *

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

0.	*	1.5	2.1	1.5	1.4	1.0	1.1	1.2	.5	.4	.4	.3	.5	.4	.4	1.0	.7	.2	.2	.3	.3
5.	*	1.6	2.1	1.5	1.4	.7	.8	1.0	.4	.4	.2	.3	.4	.4	.4	1.0	.7	.3	.3	.1	.2
10.	*	1.6	2.0	1.5	1.2	.5	.4	.8	.3	.3	.2	.4	.4	.4	1.0	.7	.3	.3	.1	.1	.1
15.	*	1.7	1.8	1.6	1.1	.3	.4	.6	.3	.3	.2	.5	.4	.4	.9	.7	.4	.1	.1	.1	.1
20.	*	1.7	1.6	1.4	1.1	.2	.2	.3	.3	.3	.2	.5	.4	.3	.3	.9	.8	.5	.2	.1	.1
25.	*	1.7	1.4	1.1	.9	.2	.1	.3	.3	.3	.2	.4	.4	.4	1.1	.8	.5	.2	.1	.1	.1
30.	*	1.8	1.4	1.0	.9	.1	.1	.3	.3	.3	.2	.3	.4	.4	1.1	.7	.4	.2	.0	.1	.1
35.	*	1.8	1.3	.9	.9	.1	.1	.3	.3	.3	.2	.3	.4	.4	1.1	.6	.3	.3	.0	.1	.1
40.	*	1.9	1.3	.8	.8	.1	.1	.3	.3	.3	.3	.3	.4	.4	.5	1.1	.6	.3	.3	.0	.1
45.	*	1.8	1.1	.8	.7	.1	.1	.3	.3	.3	.3	.3	.4	.4	.5	1.1	.5	.3	.1	.0	.1
50.	*	1.8	1.2	.8	.7	.0	.1	.3	.3	.3	.3	.4	.5	.5	.7	1.2	.5	.3	.1	.0	.1
55.	*	1.6	1.1	.8	.7	.0	.1	.4	.4	.3	.4	.4	.5	.5	.7	1.2	.6	.2	.1	.0	.0
60.	*	1.7	1.1	.7	.5	.0	.1	.4	.4	.4	.3	.4	.5	.6	.8	1.2	.6	.2	.0	.0	.0
65.	*	1.7	1.0	.7	.5	.1	.1	.4	.4	.4	.3	.4	.5	.6	.8	1.2	.5	.1	.0	.0	.0
70.	*	1.4	1.0	.6	.6	.1	.2	.4	.4	.5	.4	.4	.7	.7	.9	.9	.5	.0	.0	.0	.0
75.	*	1.2	1.0	.7	.6	.1	.1	.4	.5	.5	.4	.5	.7	.7	1.0	.7	.4	.0	.0	.0	.0
80.	*	1.1	1.1	.6	.5	.0	.1	.5	.6	.5	.3	.5	.7	.6	.9	.7	.4	.0	.0	.0	.0
85.	*	.9	1.0	.7	.6	.0	.1	.4	.5	.4	.3	.4	.6	.6	.8	.6	.4	.0	.0	.0	.0
90.	*	.8	1.0	.6	.6	.0	.0	.4	.5	.4	.3	.4	.5	.7	.5	.3	.0	.0	.0	.0	.0
95.	*	.7	1.0	.5	.6	.0	.0	.3	.3	.4	.1	.3	.4	.4	.4	.3	.3	.0	.0	.0	.0
100.	*	.6	.8	.5	.5	.0	.0	.2	.2	.3	.1	.2	.2	.3	.3	.3	.3	.0	.0	.0	.0
105.	*	.5	.7	.5	.5	.0	.0	.1	.1	.0	.2	.2	.2	.1	.1	.3	.0	.0	.0	.0	.0
110.	*	.5	.6	.5	.5	.0	.0	.1	.1	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
115.	*	.4	.7	.5	.5	.0	.0	.1	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0
120.	*	.3	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1	.0	.0	.0	.0
125.	*	.3	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
130.	*	.3	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
135.	*	.3	.8	.6	.6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.1	.0	.0	.0
140.	*	.3	.9	.8	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.1	.0	.0	.0
145.	*	.3	.9	.8	.8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.1	.0	.0	.0
150.	*	.3	.9	.8	.8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0
155.	*	.3	1.0	.9	.7	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
160.	*	.2	.9	.9	.8	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0
165.	*	.1	.9	.8	.7	.1	.1	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
170.	*	.1	.8	.8	.7	.2	.2	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
175.	*	.0	.8	.8	.7	.3	.3	.5	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
180.	*	.0	.7	.7	.5	.4	.4	.6	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1
185.	*	.0	.6	.5	.4	.4	.6	.7	.9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
190.	*	.0	.4	.4	.3	.5	.7	.9	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
195.	*	.0	.3	.3	.2	.6	.7	1.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
200.	*	.0	.2	.2	.2	.6	.7	1.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
205.	*	.0	.1	.1	.1	.6	.7	1.1	.3	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1

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JOB: Brent Spence Bridge

PAGE 5
RUN: W 5th Street & Bakewell

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

210.	*	.0	.1	.1	.1	.6	.6	1.0	.3	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1
215.	*	.0	.1	.1	.1	.6	.6	.9	.3	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1
220.	*	.0	.1	.1	.1	.6	.6	.9	.3	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1
225.	*	.0	.1	.1	.1	.6	.6	.9	.3	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1
230.	*	.0	.1	.1	.1	.6	.6	.8	.3	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.1	.1
235.	*	.0	.0	.0	.0	.6	.6	.8	.3	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1
240.	*	.0	.0	.0	.0	.6	.6	.7	.4	.1	.1	.1	.2	.0	.1	.1	.1	.0	.0	.1	.1
245.	*	.0	.2	.0	.0	.6	.6	.7	.5	.2	.1	.1	.2	.2	.1	.1	.1	.0	.0	.1	.1
250.	*	.2	.2	.0	.0	.5	.5	.9	.6	.3	.1	.1	.2	.1	.1	.1	.1	.0	.0	.1	.1
255.	*	.3	.3	.0	.0	.5	.5	.8	.8	.3	.2	.2	.3	.3	.1	.2	.3	.0	.0	.1	.1
260.	*	.5	.6	.0	.0	.5	.5	1.0	.9	.6	.3	.3	.4	.4	.3	.4	.5	.0	.0	.1	.1
265.	*	.7	.8	.1	.0	.6	.7	1.4	1.0	.8	.4	.4	.5	.5	.4	.4	.7	.1	.0	.1	.2
270.	*	1.0	1.1	.1	.0	.6	.8	1.7	1.0	.8	.6	.5	.6	.6	.6	.5	.9	.1	.1	.2	.2
275.	*	1.2	1.4	.2	.1	.7	.8	1.7	1.2	1.0	.6	.5	.6	.6	.8	.7	.9	.2	.1	.2	.3
280.	*	1.3	1.5	.3	.1	.6	.8	1.7	1.1	.9	.7	.6	.6	.8	.7	.8	1.1	.2	.1	.2	.3
285.	*	1.4	1.7	.4	.1	.7	.9	1.8	.9	.9	.6	.7	.8	.8	.7	.9	1.1	.2	.1	.2	.3
290.	*	1.4	1.6	.4	.2	.7	1.0	1.5	.9	.7	.6	.6	.7	.7	.9	1.1	.1	.1	.1	.3	.3
295.	*	1.4	1.6	.4	.2	.8	1.1	1.4	.8	.7	.5	.5	.6	.7	.7	1.0	.9	.2	.1	.2	.4
300.	*	1.4	1.5	.5	.2	.9	1.1	1.3	.8	.6	.5	.5	.6	.7	.6	1.0	1.0	.3	.1	.2	.4
305.	*	1.3	1.4	.6	.4	.9	1.2	1.2	.7	.6	.5	.5	.6	.5	.6	1.1	.9	.4	.1	.2	.4
310.	*	1.4	1.4	.6	.4	.9	1.2	1.3	.8	.6	.5	.4	.6	.5	.6	1.1	.9	.4	.2	.3	.5
315.	*	1.3	1.2	.6	.4	.9	1.2	1.3	.8	.5	.4	.4	.5	.5	1.1	.7	.5	.2	.4	.6	.6
320.	*	1.3	1.2	.6	.3	.9	1.2	1.0	.8	.5	.4	.3	.6	.5	.5	1.1	.7	.5	.2	.4	.6
325.	*	1.3	1.2	.7	.4	.9	1.2	1.2	.8	.5	.4	.3	.6	.5	.5	1.1	.6	.5	.3	.4	.5
330.	*	1.2	1.1	.6	.4	.9	1.2	1.3	.8	.5	.3	.3	.7	.5	.5	1.1	.6	.5	.3	.4	.4
335.	*	1.2	1.2	.6	.4	1.1	1.2	1.4	.8	.6	.4	.3	.7	.5	.5	1.1	.5	.5	.3	.4	.5
340.	*	1.2	1.3	.9	.5	1.0	1.6	1.5	.8	.5	.4	.3	.6	.4	.5	1.1	.5	.4	.3	.3	.6
345.	*	1.2	1.3	.9	.8	1.2	1.5	1.5	.6	.5	.3	.3	.7	.4	.5	1.1	.5	.4	.3	.2	.5
350.	*	1.3	1.6	1.1	1.0	1.1	1.4	1.6	.6	.5	.3	.3	.7	.5	.5	1.0	.4	.3	.2	.2	.4
355.	*	1.3	1.9	1.4	1.1	.9	1.3	1.5	.6	.4	.3	.4	.6	.4	.4	1.0	.6	.2	.2	.3	.4
360.	*	1.5	2.1	1.5	1.4	1.0	1.1	1.2	.5	.4	.4	.3	.5	.4	.4	1.0	.7	.2	.2	.3	.3

MAX * 1.9 2.1 1.6 1.4 1.2 1.6 1.8 1.2 1.0 .7 .7 .8 .8 1.0 1.2 1.1 .5 .3 .4 .6
DEGR. * 40 0 15 0 345 340 285 275 275 280 285 285 280 75 50 280 20 5 315 315

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JOB: Brent Spence Bridge

PAGE 6
RUN: W 5th Street & Bakewell

355. * .5 .3 .0 .2 .2 .1 .1 .2 .1 .0 .0 .0 .2 .2 .2 .2 .2 .1 .1
 360. * .5 .3 .0 .2 .2 .1 .1 .2 .2 .0 .0 .0 .1 .1 .1 .1 .1 .1 .1

 MAX * .9 .6 .7 1.1 .7 .6 .4 .6 1.1 1.0 .9 .8 .8 .5 .5 .4 .4 .7 .8 1.0
 DEGR * 270 275 260 260 220 200 140 160 245 115 95 255 250 260 255 250 110 90 260 260

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JOB: Brent Spence Bridge

PAGE 8
 RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to
 the maximum concentration, only the first
 angle, of the angles with same maximum
 concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

 0. * .2 .9 .8 .8 1.6 1.6 1.7 .2
 5. * .1 .7 .5 .5 1.7 1.8 1.8 .3
 10. * .0 .4 .4 .4 1.7 1.8 1.8 .4
 15. * .0 .3 .2 .2 1.8 1.8 1.8 .5
 20. * .0 .1 .1 .1 1.7 1.8 1.7 .5
 25. * .0 .0 .0 .0 1.6 1.6 1.6 .4
 30. * .0 .0 .0 .0 1.6 1.6 1.5 .6
 35. * .0 .0 .0 .0 1.4 1.4 1.4 .6
 40. * .0 .0 .0 .0 1.4 1.4 1.3 .6
 45. * .0 .0 .0 .0 1.3 1.3 1.2 .6
 50. * .0 .0 .0 .0 1.2 1.2 1.1 .6
 55. * .0 .0 .0 .0 1.2 1.2 1.1 .5
 60. * .0 .0 .0 .0 1.2 1.2 1.0 .5
 65. * .0 .1 .0 .0 1.2 1.1 1.0 .5
 70. * .1 .1 .0 .0 1.1 1.1 .9 .4
 75. * .1 .1 .0 .0 1.1 1.1 1.0 .5
 80. * .3 .2 .0 .0 1.1 1.1 1.0 .7
 85. * .3 .3 .0 .0 1.1 1.1 1.2 .9
 90. * .5 .4 .0 .0 1.1 1.2 1.2 1.0
 95. * .5 .5 .1 .0 1.1 1.2 1.1 1.2
 100. * .6 .5 .1 .0 1.1 1.2 1.1 1.2
 105. * .5 .4 .2 .1 1.2 1.3 1.1 1.4
 110. * .4 .4 .2 .1 1.2 1.2 1.2 1.6
 115. * .4 .4 .1 .1 1.2 1.2 1.1 1.6
 120. * .4 .4 .1 .0 1.2 1.3 1.2 1.7
 125. * .3 .4 .1 .0 1.3 1.3 1.2 1.7
 130. * .3 .3 .1 .1 1.4 1.3 1.3 1.7
 135. * .3 .3 .1 .1 1.4 1.4 1.2 1.6
 140. * .3 .3 .1 .1 1.5 1.5 1.3 1.6
 145. * .3 .3 .1 .1 1.6 1.6 1.4 1.6
 150. * .3 .3 .1 .1 1.6 1.5 1.3 1.6
 155. * .3 .3 .1 .1 1.8 1.6 1.4 1.6
 160. * .3 .3 .2 .2 1.9 1.8 1.5 1.4
 165. * .3 .5 .3 .2 1.7 1.7 1.6 1.3
 170. * .3 .6 .4 .4 1.9 1.8 1.6 1.3
 175. * .3 .8 .6 .5 1.9 1.5 1.5 1.3
 180. * .3 1.0 .6 .8 1.4 1.4 1.5 1.3
 185. * .3 1.1 .7 1.0 1.1 1.2 1.4 1.2
 190. * .4 1.1 1.1 1.2 1.1 1.0 1.2 1.2
 195. * .5 1.1 1.1 1.2 .9 .9 1.1 1.3
 200. * .5 1.1 1.2 1.3 .7 .8 1.1 1.2
 205. * .6 1.1 1.2 1.5 .5 .7 1.2 1.3

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JOB: Brent Spence Bridge

PAGE 9
 RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

 210. * .6 1.1 1.2 1.4 .5 .6 1.1 1.3
 215. * .6 .9 1.4 1.4 .4 .6 1.1 1.3
 220. * .6 1.0 1.5 1.4 .3 .6 1.2 1.4
 225. * .6 1.1 1.4 1.3 .4 .6 1.3 1.4
 230. * .7 1.2 1.4 1.3 .4 .6 1.4 1.4
 235. * .6 1.2 1.4 1.2 .4 .6 1.5 1.5
 240. * .8 1.3 1.3 1.1 .3 .6 1.6 1.4
 245. * .7 1.4 1.3 1.0 .3 .5 1.6 1.5
 250. * .9 1.6 1.3 1.0 .2 .4 1.7 1.6
 255. * 1.0 1.8 1.2 .9 .1 .3 1.7 1.5
 260. * 1.2 1.7 1.1 .9 .1 .3 1.5 1.4
 265. * 1.1 1.8 1.0 .9 .0 .2 1.4 1.2
 270. * 1.0 1.6 .9 .8 .0 .1 1.1 1.0
 275. * .9 1.4 .9 .8 .0 .1 .8 .7
 280. * .8 1.1 .8 .8 .0 .0 .6 .5
 285. * .6 1.0 .8 .8 .0 .0 .3 .3
 290. * .6 .8 .8 .8 .0 .0 .2 .2
 295. * .5 .8 .8 .8 .1 .1 .2 .1
 300. * .5 .9 .9 .8 .1 .1 .1 .0
 305. * .5 .9 .9 .9 .1 .1 .1 .0
 310. * .5 .9 1.0 1.0 .1 .1 .1 .0
 315. * .5 1.0 1.0 1.0 .1 .1 .1 .0

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

LINK #	260	255	220	205	170	160	5	120
1 *	.2	.4	.2	.1	.1	.0	.5	
2 *	.5	.7	.3	.2	.0	.0	.9	
3 *	.3	.1	.0	.0	.1	.0	.0	
4 *	.0	.0	.0	.0	.0	.0	.0	
5 *	.0	.0	.0	.0	.0	.0	.0	
6 *	.0	.0	.0	.0	.0	.0	.0	
7 *	.0	.0	.0	.0	.0	.0	.0	
8 *	.0	.0	.0	.0	.0	.0	.0	
9 *	.0	.0	.0	.1	.1	.0	.1	
10 *	.0	.0	.0	.0	.0	.0	.0	
11 *	.0	.1	.2	.2	.1	.1	.1	.0
12 *	.1	.4	.5	.5	.9	.7	.9	.0
13 *	.0	.0	.3	.4	.6	.5	.8	.0
14 *	.1	.1	.0	.1	.1	.2	.0	.2
15 *	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	X1	Y1	X2	Y2	LINK COORDINATES (FT)	LENGTH	BRG	TYPE	VPH	EF	H	W	V/C	QUEUE
					(FT) (DEG)	(G/MI)	(FT)	(FT)	(VEH)					
1. 1 EB 5th Phil Appr	*		269695.0	284787.0	269838.0 284789.0 *	143.	89.	AG	1130.	11.5	.0	44.0		
2. 2 EB 5th EB Queue	*		269805.0	284789.0	269694.6 284787.6 *	110.	269.	AG	210.	100.0	.0	24.0	.81	5.6
3. 3 EB 5th Bake Appr	*		269838.0	284789.0	270093.0 284793.0 *	255.	89.	AG	1180.	11.5	.0	44.0		
4. 4 EB 5th Bake LT	*		270093.0	284793.0	270194.0 284795.0 *	101.	89.	AG	1160.	11.5	.0	44.0		
5. 5 EB 5th EB Rt	*		270093.0	284776.0	270189.0 284778.0 *	96.	89.	AG	20.	11.5	.0	44.0		
6. 6 EB 5th Main Appr	*		270194.0	284795.0	270550.0 284799.0 *	356.	89.	AG	1430.	11.5	.0	44.0		
7. 7 EB 5th EB Queue	*		270491.0	284798.0	270392.5 284797.1 *	99.	270.	AG	157.	100.0	.0	24.0	.79	5.0
8. 8 EB 5th Main Dep	*		270550.0	284799.0	270695.0 284801.0 *	145.	89.	AG	1180.	11.5	.0	44.0		
9. 9 NB Phil 5th Appr	*		269851.0	284462.0	269847.0 284786.0 *	324.	359.	AG	580.	11.5	.0	44.0		
10. 10 NB PhilNB Queue	*		269848.0	284750.0	269851.5 284474.4 *	276.	179.	AG	216.	100.0	.0	24.0	1.05	14.0
11. 11 NB Phil5th Dep	*		269847.0	284786.0	269841.0 285143.0 *	357.	359.	AG	850.	11.5	.0	44.0		
12. 12 SB Phil5th Appr	*		269823.0	285126.0	269830.0 284793.0 *	333.	179.	AG	170.	11.5	.0	44.0		
13. 13 SB PhilSB Queue	*		269829.0	284819.0	269828.8 284834.3 *	15.	359.	AG	216.	100.0	.0	24.0	.20	.8
14. 14 SB PhilPhil Dep	*		269830.0	284793.0	269835.0 284461.0 *	332.	179.	AG	90.	11.5	.0	44.0		
15. 15 NB Park5th Appr	*		270203.0	284576.0	270200.0 284791.0 *	215.	359.	AG	30.	11.5	.0	32.0		
16. 16 NB ParkNB Queue	*		270201.0	284761.0	270201.1 284757.7 *	3.	179.	AG	98.	100.0	.0	12.0	.09	.2
17. 17 NB Bake5th Dep	*		270200.0	284791.0	270194.0 285216.0 *	425.	359.	AG	50.	11.5	.0	32.0		
18. 18 SB Bake5th Appr	*		270180.0	285216.0	270189.0 284778.0 *	438.	179.	AG	100.	11.5	.0	32.0		
19. 19 SB BakeSB Queue	*		270188.0	284828.0	270187.8 284839.0 *	11.	359.	AG	98.	100.0	.0	12.0	.31	.6
20. 20 SB BakeBake Dep	*		270189.0	284778.0	270192.0 284577.0 *	201.	179.	AG	70.	11.5	.0	32.0		
21. 21 NB MainMain Appr	*		270564.0	284513.0	270559.0 284795.0 *	282.	359.	AG	210.	11.5	.0	32.0		
22. 22 NB MainNB Queue	*		270560.0	284768.0	270560.6 284722.1 *	46.	179.	AG	131.	100.0	.0	12.0	.43	2.3
23. 23 NB MainMain Dep	*		270559.0	284795.0	270556.0 285029.0 *	234.	359.	AG	490.	11.5	.0	32.0		
24. 24 SB MainMain Appr	*		270535.0	285030.0	270539.0 284802.0 *	228.	179.	AG	180.	11.5	.0	44.0		
25. 25 SB MainSB Queue	*		270538.0	284828.0	270537.8 284847.7 *	20.	359.	AG	262.	100.0	.0	24.0	.25	1.0
26. 26 SB MainMain Dep	*		270539.0	284802.0	270543.0 284513.0 *	289.	179.	AG	150.	11.5	.0	44.0		

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
	LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM	FAC	TYPE
	(SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)	RATE	
2. 2 EB 5th EB Queue	*	60	32	2.0	1130	1754	73.30	1 3
7. 7 EB 5th EB Queue	*	60	24	2.0	1430	1706	73.30	1 3
10. 10 NB PhilNB Queue	*	60	33	2.0	580	721	73.30	1 3
13. 13 SB PhilSB Queue	*	60	33	2.0	170	1113	73.30	1 3
16. 16 NB ParkNB Queue	*	40	20	2.0	30	800	73.30	1 3

19. 19 SB BakeSB Queue *	40	20	2.0	100	800	73.30	1	3
22. 22 NB MainNB Queue *	60	40	2.0	210	1845	73.30	1	3
25. 25 SB MainSB Queue *	60	40	2.0	180	1373	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT)			*
	X	Y	Z	
1. R1 EB 82	269739.0	284764.0	5.0	*
2. R2 SW Corner	269811.0	284765.0	5.0	*
3. R3 SB 82	269812.0	284693.0	5.0	*
4. R4 SB 164	269813.0	284611.0	5.0	*
5. R5 NB 164	269868.0	284612.0	5.0	*
6. R6 NB 82	269867.0	284694.0	5.0	*
7. R7 SE Corner	269866.0	284766.0	5.0	*
8. R8 EB 82	269938.0	284768.0	5.0	*
9. R9 EB 164	270018.0	284770.0	5.0	*
10. R10 EB 82	270099.0	284760.0	5.0	*
11. R10 SW Corner	270171.0	284761.0	5.0	*
12. R12 SE Corner	270217.0	284772.0	5.0	*
13. R13 EB 82r	270289.0	284773.0	5.0	*
14. R14 EB 164	270368.0	284774.0	5.0	*
15. R15 EB 82	270447.0	284775.0	5.0	*
16. R16 SW Corner	270519.0	284776.0	5.0	*
17. R17 SB 82	270520.0	284704.0	5.0	*
18. R18 SB 164	270521.0	284622.0	5.0	*
19. R19 NB 164	270583.0	284618.0	5.0	*
20. R20 NB 82	270581.0	284700.0	5.0	*
21. R21 SE Corner	270580.0	284773.0	5.0	*
22. R22 SB 82	270652.0	284773.0	5.0	*
23. R23 WB 82	270652.0	284829.0	5.0	*
24. R24 NE Corner	270580.0	284829.0	5.0	*
25. R25 NB 82	270579.0	284901.0	5.0	*
26. R26 NB 164	270577.0	284983.0	5.0	*
27. R27 SB 164	270525.0	284975.0	5.0	*
28. R28 SB 82	270527.0	284893.0	5.0	*
29. R29 NW Corner	270518.0	284821.0	5.0	*
30. R30 WB 82	270446.0	284821.0	5.0	*
31. R31 WB 164	270368.0	284820.0	5.0	*
32. R32 WB 82	270288.0	284819.0	5.0	*
33. R33 NE Corner	270216.0	284818.0	5.0	*
34. R34 NB 82	270215.0	284890.0	5.0	*
35. R35 NB 164	270214.0	284972.0	5.0	*
36. R36 SB 164	270168.0	284972.0	5.0	*
37. R37 SB 82	270169.0	284890.0	5.0	*

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell
 DATE: 08/31/2010 TIME: 10:44:39.41

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT)			*
	X	Y	Z	
38. R38 NW Corner	270170.0	284818.0	5.0	*
39. R39 WB 82	270098.0	284817.0	5.0	*
40. R40 WB 164	270017.0	284815.0	5.0	*
41. R41 WB 82	269937.0	284814.0	5.0	*
42. R42 NE Corner	269865.0	284813.0	5.0	*
43. R43 NB 82	269864.0	284885.0	5.0	*
44. R44 NB 164	269863.0	284967.0	5.0	*
45. R45 SB 164	269809.0	284966.0	5.0	*
46. R46 SB 82	269810.0	284884.0	5.0	*
47. R47 NW Corner	269811.0	284812.0	5.0	*
48. R48 WB 82	269738.0	284810.0	5.0	*

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JOB: Brent Spence Bridge RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	1.1	1.0	.5	.5	1.0	.8	1.0	.5	.5	.4	.4	.6	.6	.6	1.1	.9	.4	.2	.2	.4
5.	1.0	1.0	.6	.7	.7	.7	.9	.5	.5	.4	.5	.6	.6	.6	1.1	.9	.5	.3	.1	.3
10.	1.1	1.0	.6	.9	.6	.5	.7	.4	.4	.3	.5	.5	.5	.9	.8	.6	.4	.1	.2	
15.	1.1	.9	.6	.9	.3	.5	.7	.4	.4	.3	.5	.5	.5	.9	.9	.5	.4	.1	.2	
20.	1.1	.9	.7	.9	.3	.3	.5	.4	.4	.3	.4	.5	.5	.9	.9	.5	.4	.1	.2	
25.	1.1	1.0	.7	.9	.2	.3	.5	.4	.4	.4	.5	.5	.5	.6	1.0	.9	.5	.3	.1	.2
30.	1.1	.9	.8	.8	.2	.2	.5	.5	.5	.4	.4	.6	.6	.7	1.2	.9	.5	.3	.1	.2
35.	1.2	.9	.8	.8	.1	.2	.5	.5	.5	.4	.5	.6	.6	.7	1.2	.8	.5	.3	.1	.2
40.	1.2	.7	.8	.8	.1	.2	.5	.5	.5	.4	.5	.6	.6	.8	1.2	.8	.6	.3	.0	.2
45.	1.2	.8	.8	.8	.1	.2	.5	.5	.5	.4	.5	.6	.6	.8	1.3	.8	.6	.3	.0	.1
50.	1.2	.9	.8	.8	.1	.2	.6	.6	.5	.5	.5	.7	.7	1.0	1.3	.8	.6	.2	.0	.1

55.	*	1.3	.9	.9	.8	.2	.2	.6	.6	.7	.5	.5	.7	.7	1.0	1.3	.9	.5	.2	.0	.1
60.	*	1.3	.9	.9	.9	.1	.2	.6	.6	.6	.5	.6	.8	.9	1.1	1.4	.9	.4	.2	.0	.1
65.	*	1.2	.8	.9	.8	.1	.2	.6	.6	.7	.6	.6	.8	.9	1.2	1.3	1.0	.4	.2	.0	.0
70.	*	1.2	.9	.9	.8	.1	.3	.7	.8	.8	.6	.7	1.0	.9	1.3	1.1	.9	.4	.2	.0	.0
75.	*	1.1	1.0	.9	.8	.1	.3	.8	.8	.9	.6	.7	1.0	.9	1.3	1.0	.8	.3	.2	.0	.0
80.	*	1.1	1.0	.9	.8	.1	.1	.8	.8	.8	.5	.6	.9	1.0	1.1	.9	.8	.2	.2	.0	.0
85.	*	1.0	.9	.8	.7	.0	.1	.8	.7	.8	.5	.6	.9	.9	1.1	.8	.7	.2	.2	.0	.0
90.	*	.9	.8	.8	.7	.0	.1	.7	.6	.7	.4	.5	.8	.8	.9	.7	.8	.2	.2	.0	.0
95.	*	.8	.8	.7	.7	.0	.0	.5	.5	.6	.3	.2	.6	.7	.6	.5	.7	.2	.2	.0	.0
100.	*	.5	.6	.7	.7	.0	.0	.4	.3	.4	.1	.1	.4	.4	.5	.4	.6	.2	.2	.0	.0
105.	*	.5	.5	.7	.7	.0	.0	.2	.2	.3	.1	.1	.2	.2	.2	.4	.5	.2	.2	.0	.0
110.	*	.4	.5	.7	.7	.0	.0	.1	.1	.1	.0	.0	.2	.2	.1	.2	.5	.2	.2	.0	.0
115.	*	.4	.5	.7	.7	.0	.0	.1	.1	.1	.0	.0	.1	.1	.1	.1	.4	.2	.2	.0	.0
120.	*	.3	.5	.7	.7	.0	.0	.1	.1	.1	.0	.0	.1	.1	.1	.1	.4	.2	.2	.0	.0
125.	*	.3	.6	.7	.7	.0	.0	.1	.1	.1	.0	.0	.1	.1	.1	.1	.4	.2	.2	.0	.0
130.	*	.4	.6	.7	.7	.0	.0	.0	.0	.1	.0	.0	.1	.1	.1	.1	.4	.2	.2	.0	.0
135.	*	.4	.7	.7	.7	.0	.0	.0	.0	.1	.0	.0	.1	.1	.1	.1	.4	.2	.2	.0	.0
140.	*	.4	.7	.7	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.0	.0
145.	*	.3	.7	.8	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.0	.0
150.	*	.3	.9	.9	.7	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.0	.0
155.	*	.3	.9	.9	.8	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.1	.0	.0
160.	*	.2	.9	.8	.7	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.1	.0	.0
165.	*	.1	.8	.8	.6	.3	.4	.4	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0
170.	*	.1	.8	.7	.4	.4	.5	.6	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0
175.	*	.0	.7	.5	.3	.6	.8	.8	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.1
180.	*	.0	.5	.3	.2	.8	.9	1.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1
185.	*	.0	.3	.2	.1	1.0	1.2	1.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.1
190.	*	.0	.1	.1	.0	1.1	1.3	1.3	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
195.	*	.0	.0	.0	.0	1.2	1.4	1.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
200.	*	.0	.0	.0	.0	1.2	1.4	1.2	.3	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
205.	*	.0	.0	.0	.0	1.2	1.3	1.2	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

210.	*	.0	.0	.0	.0	1.2	1.2	1.0	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2
215.	*	.0	.0	.0	.0	1.2	1.2	.9	.4	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2
220.	*	.0	.0	.0	.0	1.1	1.2	.8	.4	.3	.1	.0	.0	.0	.0	.0	.1	.0	.0	.1	.2
225.	*	.0	.0	.0	.0	1.1	1.1	.7	.4	.4	.1	.1	.0	.1	.1	.1	.1	.0	.0	.1	.1
230.	*	.0	.0	.0	.0	1.1	1.1	.7	.5	.4	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1
235.	*	.0	.0	.0	.0	.9	.9	.6	.5	.4	.1	.1	.1	.1	.1	.1	.1	.0	.0	.1	.1
240.	*	.0	.1	.0	.0	.9	.9	.4	.4	.4	.1	.1	.1	.2	.1	.1	.1	.0	.0	.1	.1
245.	*	.0	.1	.0	.0	.9	.9	.4	.4	.4	.1	.1	.1	.2	.2	.1	.1	.0	.0	.1	.1
250.	*	.1	.1	.0	.0	.9	.9	.4	.4	.3	.1	.1	.2	.2	.2	.3	.2	.0	.0	.1	.1
255.	*	.1	.2	.0	.0	.9	.9	.6	.7	.4	.2	.2	.3	.3	.3	.4	.4	.0	.0	.1	.1
260.	*	.1	.3	.0	.0	.9	.9	.6	.6	.7	.2	.2	.5	.5	.5	.5	.5	.0	.0	.1	.1
265.	*	.1	.5	.0	.0	.9	.9	.7	.7	.8	.3	.4	.6	.6	.6	.7	.8	.0	.0	.1	.1
270.	*	.3	.7	.0	.0	.9	.9	1.0	.9	.8	.6	.4	.7	.6	.8	1.0	1.0	.0	.1	.1	.1
275.	*	.3	.8	.0	.0	.9	.9	1.1	1.1	.8	.6	.4	.7	.8	.9	1.1	1.2	.1	.0	.1	.2
280.	*	.5	1.0	.0	.0	.9	.9	1.1	1.1	.9	.6	.5	.8	.9	.9	1.1	1.2	.2	.0	.1	.2
285.	*	.5	1.1	.0	.0	.9	1.0	1.1	.9	1.0	.6	.5	.8	.8	1.0	1.1	1.3	.2	.0	.1	.3
290.	*	.6	1.1	.0	.0	.9	1.1	1.1	.9	.9	.6	.6	.8	.9	.8	1.1	1.2	.2	.1	.2	.4
295.	*	.7	1.2	.1	.0	.9	1.1	1.2	.9	.7	.6	.6	.9	.8	.8	1.2	1.2	.3	.1	.2	.4
300.	*	.8	1.2	.2	.0	.9	1.2	1.1	.8	.7	.6	.6	.7	.8	.7	1.2	1.1	.4	.1	.2	.6
305.	*	.9	1.2	.2	.0	1.1	1.3	1.0	.7	.7	.5	.6	.6	.7	.7	1.2	1.0	.4	.1	.2	.6
310.	*	1.0	1.1	.3	.0	1.2	1.5	1.1	.7	.7	.5	.6	.6	.7	.7	1.2	.9	.4	.1	.4	.6
315.	*	1.0	1.1	.3	.0	1.3	1.5	1.0	.7	.6	.5	.4	.6	.6	.6	1.1	.8	.4	.2	.4	.6
320.	*	1.0	1.0	.4	.1	1.4	1.5	1.1	.7	.6	.5	.4	.6	.6	.6	1.1	.7	.5	.3	.5	.6
325.	*	1.0	1.0	.4	.2	1.4	1.4	1.1	.7	.6	.4	.4	.6	.6	.6	1.1	.7	.4	.3	.5	.6
330.	*	1.0	.9	.4	.2	1.4	1.3	1.1	.7	.6	.4	.4	.5	.5	.6	1.1	.7	.3	.3	.4	.5
335.	*	1.0	.8	.4	.2	1.4	1.4	1.2	.6	.5	.4	.4	.6	.5	.5	1.0	.5	.3	.3	.2	.6
340.	*	1.0	.8	.4	.2	1.6	1.2	1.1	.5	.4	.4	.4	.6	.5	.5	1.0	.5	.3	.2	.2	.7
345.	*	1.0	.7	.4	.2	1.6	1.3	1.1	.5	.4	.4	.4	.5	.5	.5	.9	.5	.3	.2	.3	.7
350.	*	1.0	.7	.5	.3	1.4	1.1	1.1	.5	.5	.4	.4	.5	.5	.5	.9	.6	.3	.2	.5	.5
355.	*	1.0	.9	.4	.5	1.1	1.0	1.0	.6	.5	.3	.4	.6	.6	.6	1.1	.8	.2	.2	.5	.5
360.	*	1.1	1.0	.5	.5	1.0	.8	1.0	.5	.5	.4	.4	.6	.6	.6	1.1	.9	.4	.2	.2	.4
MAX	*	1.3	1.2	.9	.9	1.6	1.5	1.3	1.1	1.0	.6	.7	1.0	1.0	1.3	1.4	1.3	.6	.4	.5	.7
DEGR.	*	55	295	150	10	340	310	190	275	285	65	70	70	80	70	60	285	10	10	320	340

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
 REC38 REC39 REC40

0.	*	.6	.4	.0	.2	.1	.1	.1	.2	.3	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0
5.	*	.5	.4	.0	.1	.1	.0	.1	.2	.3	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0
10.	*	.5	.4	.0	.1	.1	.0	.1	.2	.4	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0
15.	*	.4	.4	.0	.0	.0	.0	.2	.2	.4	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0

20.	*	.4	.4	.0	.0	.0	.0	.2	.3	.5	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0
25.	*	.4	.4	.0	.0	.0	.0	.2	.3	.5	.0	.0	.0	.0	.0	.1	.1	.2	.0	.0
30.	*	.4	.4	.0	.0	.0	.0	.2	.3	.6	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0
35.	*	.5	.4	.0	.0	.0	.0	.2	.3	.6	.1	.0	.0	.0	.1	.1	.2	.0	.0	.0
40.	*	.5	.4	.0	.0	.0	.0	.2	.3	.7	.1	.0	.0	.1	.0	.1	.0	.1	.0	.0
45.	*	.5	.4	.0	.0	.0	.0	.2	.3	.7	.2	.1	.1	.1	.0	.0	.0	.1	.0	.0
50.	*	.5	.4	.0	.0	.0	.0	.2	.3	.7	.2	.1	.1	.1	.0	.0	.0	.1	.0	.0
55.	*	.5	.3	.0	.0	.0	.0	.3	.3	.7	.2	.1	.1	.1	.0	.0	.0	.1	.0	.0
60.	*	.5	.3	.0	.0	.0	.0	.3	.3	.7	.2	.1	.1	.1	.0	.0	.0	.1	.1	.1
65.	*	.5	.3	.0	.0	.0	.0	.2	.3	.7	.3	.1	.1	.1	.0	.0	.0	.2	.1	.1
70.	*	.5	.3	.0	.0	.0	.0	.2	.3	.8	.3	.1	.2	.2	.0	.0	.0	.2	.2	.1
75.	*	.5	.2	.0	.1	.0	.0	.2	.3	.7	.5	.2	.3	.3	.0	.0	.0	.3	.2	.3
80.	*	.4	.2	.0	.1	.0	.0	.2	.3	.8	.5	.5	.5	.4	.0	.0	.0	.4	.4	.4
85.	*	.4	.1	.1	.1	.0	.0	.2	.3	.8	.6	.7	.7	.7	.0	.0	.0	.5	.6	.5
90.	*	.3	.1	.1	.2	.0	.0	.2	.3	.8	.9	.9	.9	.8	.0	.0	.1	.8	.6	.7
95.	*	.2	.1	.1	.3	.0	.0	.2	.3	1.0	.9	1.1	1.0	.9	.1	.0	.1	.9	.7	.8
100.	*	.1	.0	.2	.4	.0	.0	.2	.2	.9	.9	1.1	1.0	1.0	.1	.0	.1	1.0	.8	.8
105.	*	.1	.0	.2	.4	.0	.0	.2	.2	.9	1.0	1.3	1.0	1.0	.3	.0	.0	.3	.9	.8
110.	*	.1	.0	.2	.4	.0	.0	.2	.4	.9	1.0	1.3	.9	.8	.3	.1	.1	.3	.8	.7
115.	*	.0	.0	.3	.5	.0	.0	.3	.4	.9	1.1	1.2	.9	.8	.3	.1	.1	.3	.7	.7
120.	*	.0	.0	.3	.5	.1	.0	.3	.4	.9	1.2	1.1	.9	.8	.4	.1	.1	.3	.7	.6
125.	*	.0	.0	.3	.5	.1	.0	.3	.5	.9	1.1	1.0	.7	.7	.3	.2	.1	.3	.7	.6
130.	*	.0	.0	.3	.5	.1	.0	.3	.5	.8	1.1	1.0	.7	.7	.3	.3	.2	.3	.7	.5
135.	*	.0	.0	.4	.5	.1	.0	.4	.5	.8	1.0	.8	.6	.6	.3	.2	.2	.3	.6	.5
140.	*	.0	.0	.4	.4	.2	.0	.4	.6	.8	1.1	.8	.6	.6	.3	.2	.3	.2	.5	.5
145.	*	.0	.0	.4	.4	.2	.1	.4	.6	.8	1.1	.7	.6	.6	.2	.2	.3	.3	.5	.4
150.	*	.0	.0	.4	.4	.2	.1	.4	.6	.9	1.0	.7	.6	.6	.2	.2	.3	.3	.5	.4
155.	*	.0	.0	.4	.4	.2	.1	.4	.6	.8	.9	.6	.5	.5	.2	.2	.2	.3	.5	.4
160.	*	.0	.0	.4	.4	.2	.1	.4	.6	.8	.9	.5	.5	.5	.2	.1	.2	.3	.4	.4
165.	*	.0	.0	.4	.4	.2	.2	.4	.6	.8	.9	.5	.5	.5	.2	.1	.2	.3	.4	.4
170.	*	.0	.0	.4	.4	.3	.2	.5	.6	.8	.9	.5	.5	.5	.2	.1	.3	.2	.4	.5
175.	*	.1	.0	.4	.6	.3	.2	.5	.7	.7	1.0	.6	.6	.6	.2	.1	.3	.2	.5	.5
180.	*	.2	.0	.4	.6	.3	.3	.4	.5	.7	1.0	.6	.6	.6	.2	.1	.1	.2	.5	.4
185.	*	.2	.0	.4	.7	.4	.4	.2	.4	.6	1.0	.6	.6	.6	.3	.2	.1	.2	.5	.5
190.	*	.2	.0	.4	.7	.5	.4	.3	.4	.5	.9	.5	.5	.5	.2	.2	.1	.2	.4	.4
195.	*	.3	.0	.4	.7	.5	.4	.3	.5	.5	.9	.5	.5	.5	.2	.1	.1	.2	.4	.4
200.	*	.4	.0	.4	.8	.5	.5	.4	.5	.9	.5	.5	.6	.2	.1	.2	.2	.4	.5	.5
205.	*	.4	.0	.4	.8	.6	.6	.3	.3	.5	1.0	.5	.5	.6	.2	.1	.2	.2	.4	.5

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
REC38 REC39 REC40

210.	*	.5	.0	.4	.6	.5	.5	.3	.3	.7	1.1	.6	.6	.5	.2	.1	.2	.2	.5	.5	.7
215.	*	.5	.0	.4	.6	.7	.6	.3	.3	.7	1.1	.6	.6	.2	.3	.2	.3	.2	.3	.5	.6
220.	*	.5	.0	.6	.7	.6	.3	.5	.7	1.1	.6	.6	.6	.3	.2	.2	.3	.6	.6	.8	.8
225.	*	.4	.0	.6	.8	.7	.6	.2	.4	.9	1.1	.6	.6	.8	.3	.2	.2	.3	.6	.6	.8
230.	*	.4	.0	.6	.7	.8	.5	.1	.4	.9	1.2	.7	.7	.7	.3	.2	.2	.3	.7	.7	.9
235.	*	.4	.0	.7	.9	.8	.4	.1	.4	1.0	1.1	.7	.8	.7	.3	.2	.2	.3	.7	.7	.9
240.	*	.3	.1	.6	.9	.6	.4	.1	.4	1.1	1.2	.8	.9	.9	.3	.1	.1	.3	.7	.8	.8
245.	*	.3	.1	.7	1.0	.6	.4	.1	.3	1.2	1.1	.9	.9	.9	.3	.1	.1	.3	.8	.7	.8
250.	*	.4	.1	.7	1.2	.6	.4	.0	.2	1.3	1.2	1.0	.9	.8	.2	.1	.0	.2	.8	.7	1.0
255.	*	.5	.3	.8	1.2	.5	.3	.0	.2	1.3	1.1	1.1	1.0	.9	.1	.0	.1	.1	.8	.7	.9
260.	*	.6	.4	.8	1.3	.4	.3	.0	.2	1.2	1.1	.9	.9	.9	.1	.1	.1	.1	.8	.8	.8
265.	*	.8	.6	.9	1.2	.4	.3	.0	.1	1.2	1.0	.9	.7	.7	.1	.1	.1	.2	.6	.7	.8
270.	*	.9	.6	.8	1.0	.3	.3	.0	.0	1.0	.8	.7	.6	.7	.1	.1	.1	.1	.5	.8	.7
275.	*	1.0	.7	.6	1.0	.3	.3	.0	.0	.6	.6	.6	.5	.4	.1	.1	.1	.1	.4	.4	.6
280.	*	1.0	.8	.4	.8	.3	.3	.0	.0	.5	.3	.3	.4	.3	.1	.0	.1	.1	.3	.3	.3
285.	*	1.1	.8	.4	.7	.3	.2	.0	.0	.3	.2	.2	.2	.4	.1	.0	.1	.1	.3	.2	.3
290.	*	.9	.9	.1	.7	.3	.2	.0	.0	.2	.1	.1	.1	.3	.1	.0	.0	.1	.2	.2	.2
295.	*	.9	.9	.1	.5	.3	.2	.0	.0	.1	.1	.1	.1	.2	.0	.0	.0	.1	.2	.2	.2
300.	*	.8	.8	.1	.5	.3	.2	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.1	.1	.2	.2
305.	*	1.0	.8	.1	.4	.3	.2	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.1	.1	.2	.2
310.	*	.9	.6	.1	.4	.3	.2	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1
315.	*	.8	.6	.1	.4	.3	.2	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1
320.	*	.7	.6	.1	.3	.3	.2	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
325.	*	.7	.5	.1	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
330.	*	.9	.5	.1	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
335.	*	.9	.5	.0	.4	.2	.2	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
340.	*	.8	.4	.0	.4	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
345.	*	.8	.4	.0	.3	.2	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
350.	*	.7	.4	.0	.2	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
355.	*	.6	.4	.0	.2	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
360.	*	.6	.4	.0	.2	.1	.1	.1	.2	.3	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0

MAX * 1.1 .9 .9 1.3 .8 .6 .5 .7 1.3 1.2 1.3 1.0 1.0 .4 .3 .3 .3 1.0 .8 1.0
DEGR. * 285 290 265 260 230 205 170 175 250 120 105 95 100 120 130 140 105 100 240 250

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

0.	*	.0	.5	.5	.4	.2	.3	.4	.0
5.	*	.0	.4	.4	.3	.3	.3	.5	.0
10.	*	.0	.3	.3	.3	.3	.4	.5	.1
15.	*	.0	.2	.2	.2	.4	.4	.7	.1
20.	*	.0	.2	.2	.1	.4	.4	.7	.1
25.	*	.0	.1	.1	.1	.4	.4	.7	.1
30.	*	.0	.1	.1	.1	.4	.4	.7	.1
35.	*	.0	.1	.1	.1	.4	.4	.7	.1
40.	*	.0	.1	.1	.1	.4	.4	.7	.1
45.	*	.0	.1	.1	.0	.4	.4	.8	.1
50.	*	.0	.0	.0	.0	.4	.4	.8	.1
55.	*	.1	.1	.0	.0	.4	.4	.8	.2
60.	*	.1	.1	.0	.0	.4	.4	.8	.2
65.	*	.1	.1	.0	.0	.4	.4	.7	.2
70.	*	.1	.1	.0	.0	.4	.4	.8	.3
75.	*	.3	.2	.0	.0	.4	.4	.8	.5
80.	*	.4	.4	.0	.0	.4	.4	1.0	.6
85.	*	.5	.5	.0	.0	.4	.4	1.0	.9
90.	*	.6	.7	.1	.0	.4	.5	1.1	1.1
95.	*	.7	.8	.1	.0	.4	.5	1.3	1.1
100.	*	.8	.8	.2	.1	.5	.6	1.2	1.3
105.	*	.8	.8	.3	.1	.5	.6	1.1	1.3
110.	*	.8	.7	.3	.1	.5	.7	1.0	1.4
115.	*	.6	.6	.3	.1	.5	.6	1.0	1.4
120.	*	.6	.6	.2	.1	.5	.6	1.1	1.5
125.	*	.6	.6	.2	.1	.5	.6	1.0	1.5
130.	*	.5	.5	.2	.1	.5	.6	1.0	1.5
135.	*	.5	.5	.3	.2	.5	.6	.8	1.5
140.	*	.5	.5	.3	.2	.5	.7	.9	1.5
145.	*	.5	.5	.3	.2	.5	.8	1.0	1.5
150.	*	.5	.6	.3	.2	.5	.9	1.1	1.3
155.	*	.4	.5	.3	.2	.6	.9	1.1	1.3
160.	*	.4	.7	.4	.3	.7	.9	1.0	1.3
165.	*	.4	.8	.6	.4	.7	.9	1.0	1.2
170.	*	.4	1.1	.7	.5	.8	.9	1.1	1.1
175.	*	.5	1.3	.8	.7	.8	.8	1.2	1.1
180.	*	.6	1.4	1.0	.8	.6	.9	1.0	1.1
185.	*	.6	1.5	.9	1.0	.5	.7	.9	1.0
190.	*	.6	1.4	.9	.9	.4	.5	.9	1.0
195.	*	.7	1.3	1.0	1.0	.2	.4	.7	1.0
200.	*	.7	1.1	1.0	.9	.2	.4	.8	1.0
205.	*	.8	1.1	1.1	.8	.2	.4	.8	1.0

1

PAGE 9

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

210.	*	.9	1.2	.9	.8	.2	.4	.9	1.0
215.	*	.9	1.0	.9	.8	.2	.4	1.0	1.0
220.	*	.8	1.1	1.0	.7	.1	.4	1.1	1.0
225.	*	.8	1.0	1.0	.7	.0	.3	1.1	1.0
230.	*	.8	1.1	1.0	.6	.0	.2	1.1	1.0
235.	*	.8	1.1	.8	.5	.0	.2	1.2	1.0
240.	*	1.0	1.1	.6	.4	.0	.2	1.2	.9
245.	*	.9	1.2	.6	.4	.0	.0	1.2	.8
250.	*	.9	1.2	.6	.4	.0	.0	1.2	.7
255.	*	.9	1.2	.4	.4	.0	.0	1.1	.6
260.	*	1.0	1.3	.4	.4	.0	.0	1.0	.5
265.	*	.9	1.3	.4	.4	.0	.0	.8	.4
270.	*	.6	1.1	.4	.4	.0	.0	.6	.3
275.	*	.6	1.1	.4	.4	.0	.0	.5	.2
280.	*	.5	.9	.4	.4	.0	.0	.3	.1
285.	*	.2	.8	.4	.4	.0	.0	.2	.1
290.	*	.2	.6	.4	.4	.0	.0	.1	.1
295.	*	.2	.6	.4	.4	.0	.0	.1	.1
300.	*	.2	.7	.5	.4	.0	.0	.1	.1
305.	*	.2	.7	.5	.5	.0	.0	.0	.0
310.	*	.2	.6	.5	.5	.0	.0	.0	.0
315.	*	.2	.6	.5	.5	.0	.0	.0	.0
320.	*	.2	.6	.5	.5	.0	.0	.0	.0
325.	*	.2	.7	.6	.6	.0	.0	.0	.0
330.	*	.2	.6	.6	.6	.0	.0	.0	.0
335.	*	.1	.6	.6	.6	.0	.0	.0	.0
340.	*	.1	.7	.7	.6	.0	.0	.0	.0
345.	*	.1	.7	.7	.5	.0	.1	.1	.0
350.	*	.1	.7	.7	.5	.2	.2	.2	.0
355.	*	.0	.6	.5	.5	.2	.2	.2	.0
360.	*	.0	.5	.5	.4	.2	.3	.4	.0

MAX * 1.0 1.5 1.1 1.0 .8 .9 1.3 1.5
 DEGR. * 240 185 205 185 170 150 95 120

THE HIGHEST CONCENTRATION IS 1.60 PPM AT 340 DEGREES FROM REC5 .
 THE 2ND HIGHEST CONCENTRATION IS 1.50 PPM AT 120 DEGREES FROM REC48.
 THE 3RD HIGHEST CONCENTRATION IS 1.50 PPM AT 310 DEGREES FROM REC6 .

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PAGE 10

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

DATE: 08/31/2010 TIME: 10:44:39.41

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

LINK #	55	295	150	10	340	310	190	275	285	65	70	70	80	70	60	285	10	10	320	340	
1 *	.5	.5	.0	.1	.1	.2	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2 *	.6	.7	.0	.0	.1	.2	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3 *	.1	.0	.0	.1	.0	.0	.0	.5	.7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0	.2	.6	.9	.8	.8	.7	.9	.2	.1	.2	.1	.0	.0
7 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.4	.4	.4	.0	.0	.1	.0	.0	.0	.0
8 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.1	.0	.1	.0
9 *	.0	.0	.2	.2	.4	.3	.4	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.6	.3	.9	.8	.9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.1	.0	.0	.1	.1	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.1	.1	.0	.1	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.1
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.0

1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 10:44:39.41

RUN: W 5th Street & Bakewell

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37

REC38 REC39 REC40

LINK #	285	290	265	260	230	205	170	175	250	120	105	95	100	120	130	140	105	100	240	250	
1 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
2 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
3 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6	.7
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.6	.2	.3	.6	.3	.1	.1	.2	.9	.7	.8	.8	.9	.3	.2	.2	.2	.7	.0	.0	.0
7 *	.2	.1	.1	.2	.1	.1	.0	.4	.4	.4	.1	.1	.1	.1	.0	.1	.1	.0	.0	.0	.0
8 *	.2	.5	.3	.1	.0	.1	.1	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.1	.1	.2	.2	.3	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.1	.2	.1	.0	.1	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 10:44:39.41

RUN: W 5th Street & Bakewell

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

LINK #	240	185	205	185	170	150	95	120
1 *	.1	.0	.1	.1	.1	.0	.2	.5
2 *	.1	.0	.1	.0	.0	.0	.0	.7
3 *	.6	.5	.1	.1	.1	.2	.5	.1
4 *	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.1	.0	.0

7 * .0 .0 .0 .0 .0 .0 .0 .0
8 * .0 .0 .0 .0 .0 .0 .0 .0
9 * .1 .3 .1 .1 .1 .1 .0 .1
10 * .1 .5 .1 .2 .2 .1 .0 .1
11 * .0 .2 .5 .5 .2 .3 .3 .0
12 * .0 .0 .0 .0 .1 .1 .1 .0
13 * .0 .0 .1 .0 .0 .1 .1 .0
14 * .0 .0 .0 .0 .0 .0 .0 .0
15 * .0 .0 .0 .0 .0 .0 .0 .0
16 * .0 .0 .0 .0 .0 .0 .0 .0
17 * .0 .0 .0 .0 .0 .0 .0 .0
18 * .0 .0 .0 .0 .0 .0 .0 .0
19 * .0 .0 .0 .0 .0 .0 .0 .0
20 * .0 .0 .0 .0 .0 .0 .0 .0
21 * .0 .0 .0 .0 .0 .0 .0 .0
22 * .0 .0 .0 .0 .0 .0 .0 .0
23 * .0 .0 .0 .0 .0 .0 .0 .0
24 * .0 .0 .0 .0 .0 .0 .0 .0
25 * .0 .0 .0 .0 .0 .0 .0 .0
26 * .0 .0 .0 .0 .0 .0 .0 .0

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

PAGE 1

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 10:46:56.72

RUN: W 5th Street & Bakewell

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 EB 5th Phil Appr	* 269695.0	284787.0	269838.0	284789.0	*	143.	89.	AG	8901.	1.5	.0	44.0			
2. 2 EB 5th EB Queue	* 269805.0	284789.0	266020.0	284741.1	*	3785.	269.	AG	163.	100.0	.0	24.0	4.94	192.3	
3. 3 EB 5th Bake Appr	* 269838.0	284789.0	270093.0	284793.0	*	255.	89.	AG	850.	11.5	.0	44.0			
4. 4 EB 5th Bake Appr	* 270093.0	284793.0	270194.0	284795.0	*	101.	89.	AG	840.	11.5	.0	44.0			
5. 5 EB 5th EB Rt	* 270093.0	284776.0	270189.0	284778.0	*	96.	89.	AG	10.	11.5	.0	44.0			
6. 6 EB 5th Main Appr	* 270194.0	284795.0	270550.0	284799.0	*	356.	89.	AG	1080.	11.5	.0	44.0			
7. 7 EB 5th EB Queue	* 270491.0	284798.0	265483.8	284750.8	*	5007.	269.	AG	196.	100.0	.0	24.0	7.50	254.4	
8. 8 EB 5th Main Dep	* 270550.0	284799.0	270695.0	284801.0	*	145.	89.	AG	850.	11.5	.0	44.0			
9. 9 NB Phil 5th Appr	* 269851.0	284462.0	269847.0	284786.0	*	324.	359.	AG	310.	11.5	.0	44.0			
10. 10 NB PhilNB Queue	* 269848.0	284750.0	269859.7	283838.9	*	911.	179.	AG	196.	100.0	.0	24.0	2.09	46.3	
11. 11 NB Phil5th Dep	* 269847.0	284786.0	269841.0	285143.0	*	357.	359.	AG	400.	11.5	.0	44.0			
12. 12 SB Phil5th Appr	* 269823.0	285126.0	269830.0	284793.0	*	333.	179.	AG	850.	11.5	.0	44.0			
13. 13 SB PhilSB Queue	* 269829.0	284819.0	269779.6	288726.3	*	3908.	359.	AG	196.	100.0	.0	24.0	6.85	198.5	
14. 14 SB PhilPhil Dep	* 269830.0	284793.0	269835.0	284461.0	*	332.	179.	AG	580.	11.5	.0	.4			
15. 15 NB Park5th Appr	* 270203.0	284576.0	270200.0	284791.0	*	215.	359.	AG	70.	11.5	.0	32.0			
16. 16 NB ParkNB Queue	* 270201.0	284761.0	270207.8	284318.6	*	442.	179.	AG	98.	100.0	.0	12.0	2.19	22.5	
17. 17 NB Bake5th Dep	* 270200.0	284791.0	270194.0	285216.0	*	425.	359.	AG	70.	11.5	.0	32.0			
18. 18 SB Bake5th Appr	* 270180.0	285216.0	270189.0	284778.0	*	438.	179.	AG	80.	11.5	.0	32.0			
19. 19 SB BakeSB Queue	* 270188.0	284828.0	270178.4	285378.6	*	551.	359.	AG	98.	100.0	.0	12.0	2.50	28.0	
20. 20 SB BakeBake Dep	* 270189.0	284778.0	270192.0	284577.0	*	201.	179.	AG	40.	11.5	.0	.3			
21. 21 NB MainMain Appr	* 270564.0	284513.0	270559.0	284795.0	*	282.	359.	AG	210.	11.5	.0	.3			
22. 22 NB MainNB Queue	* 270560.0	284768.0	270581.3	283128.3	*	1640.	179.	AG	117.	100.0	.0	12.0	3.44	83.3	
23. 23 NB MainMain Dep	* 270559.0	284795.0	270556.0	285029.0	*	234.	359.	AG	540.	11.5	.0	.3			
24. 24 SB MainMain Appr	* 270535.0	285030.0	270539.0	284802.0	*	228.	179.	AG	250.	11.5	.0	.4			
25. 25 SB MainSB Queue	* 270538.0	284828.0	270531.8	285312.8	*	485.	359.	AG	141.	100.0	.0	24.0	1.47	24.6	
26. 26 SB MainMain Dep	* 270539.0	284802.0	270543.0	284513.0	*	289.	179.	AG	150.	11.5	.0	.4			

PAGE 2

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 10:46:56.72

RUN: W 5th Street & Bakewell

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH (SEC)	TIME (SEC)	LOST TIME (SEC)	VOL (VPH)	FLOW RATE (VPH)	EM FAC (gm/hr)	TYPE	RATE	
2. 2 EB 5th EB Queue	* 60	25	2.0	890	175	73.00	1	3
7. 7 EB 5th EB Queue	* 60	30	2.0	1080	168	73.00	1	3
10. 10 NB PhilNB Queue	* 60	30	2.0	310	173	73.00	1	3
13. 13 SB PhilSB Queue	* 60	30	2.0	850	144	73.00	1	3
16. 16 NB ParkNB Queue	* 40	20	2.0	70	80	73.00	1	3
19. 19 SB BakeSB Queue	* 40	20	2.0	80	80	73.00	1	3
22. 22 NB MainNB Queue	* 60	36	2.0	210	186	73.00	1	3
25. 25 SB MainSB Queue	* 100	36	2.0	250	142	73.00	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	X	Y	Z	*
1. R1 EB 82	* 269739.0	284764.0		5.0	*
2. R2 SW Corner	* 269811.0	284765.0		5.0	*
3. R3 SB 82	* 269812.0	284693.0		5.0	*
4. R4 SB 164	* 269813.0	284611.0		5.0	*
5. R5 NB 164	* 269868.0	284612.0		5.0	*
6. R6 NB 82	* 269867.0	284694.0		5.0	*
7. R7 SE Corner	* 269866.0	284766.0		5.0	*
8. R8 EB 82	* 269938.0	284768.0		5.0	*
9. R9 EB 164	* 270018.0	284770.0		5.0	*
10. R10 EB 82	* 270099.0	284760.0		5.0	*
11. R10 SW Corner	* 270171.0	284761.0		5.0	*

12. R12 SE Corner	*	270217.0	284772.0	5.0	*
13. R13 EB 82r	*	270289.0	284773.0	5.0	*
14. R14 EB 164	*	270368.0	284774.0	5.0	*
15. R15 EB 82	*	270447.0	284775.0	5.0	*
16. R16 SW Corner	*	270519.0	284776.0	5.0	*
17. R17 SB 82	*	270520.0	284704.0	5.0	*
18. R18 SB 164	*	270521.0	284622.0	5.0	*
19. R19 NB 164	*	270583.0	284618.0	5.0	*
20. R20 NB 82	*	270581.0	284700.0	5.0	*
21. R21 SE Corner	*	270580.0	284773.0	5.0	*
22. R22 SB 82	*	270652.0	284773.0	5.0	*
23. R23 WB 82	*	270652.0	284829.0	5.0	*
24. R24 NE Corner	*	270580.0	284829.0	5.0	*
25. R25 NB 82	*	270579.0	284901.0	5.0	*
26. R26 NB 164	*	270577.0	284983.0	5.0	*
27. R27 SB 164	*	270525.0	284975.0	5.0	*
28. R28 SB 82	*	270527.0	284893.0	5.0	*
29. R29 NW Corner	*	270518.0	284821.0	5.0	*
30. R30 WB 82	*	270446.0	284821.0	5.0	*
31. R31 WB 164	*	270368.0	284820.0	5.0	*
32. R32 WB 82	*	270288.0	284819.0	5.0	*
33. R33 NE Corner	*	270216.0	284818.0	5.0	*
34. R34 NB 82	*	270215.0	284890.0	5.0	*
35. R35 NB 164	*	270214.0	284972.0	5.0	*
36. R36 SB 164	*	270168.0	284972.0	5.0	*
37. R37 SB 82	*	270169.0	284890.0	5.0	*

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JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 10:46:56.72

RUN: W 5th Street & Bakewell

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT)			*
		X	Y	Z	
38. R38 NW Corner	*	270170.0	284818.0	5.0	*
39. R39 WB 82	*	270098.0	284817.0	5.0	*
40. R40 WB 164	*	270017.0	284815.0	5.0	*
41. R41 WB 82	*	269937.0	284814.0	5.0	*
42. R42 NE Corner	*	269865.0	284813.0	5.0	*
43. R43 NB 82	*	269864.0	284885.0	5.0	*
44. R44 NB 164	*	269863.0	284967.0	5.0	*
45. R45 SB 164	*	269809.0	284966.0	5.0	*
46. R46 SB 82	*	269810.0	284884.0	5.0	*
47. R47 NW Corner	*	269811.0	284812.0	5.0	*
48. R48 WB 82	*	269738.0	284810.0	5.0	*

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JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)	(DEGR)* REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18		
0.	* 1.8	2.3	1.3	1.1	1.4	1.2	1.8	1.0	1.1	.8	1.0	1.2	1.0	1.0	1.1	.8	.4	.3	.3	.4
5.	* 1.9	2.3	1.2	1.2	1.1	1.0	1.5	.9	1.0	.8	.9	1.1	1.0	1.0	1.1	.8	.3	.4	.3	.2
10.	* 1.9	2.1	1.2	1.4	.8	.9	1.2	.9	.9	.8	1.0	1.1	1.0	1.0	1.1	.8	.3	.3	.3	.2
15.	* 1.9	2.1	1.3	1.1	.6	.5	1.0	.8	.9	.8	1.0	1.0	1.0	1.1	1.2	.8	.4	.3	.1	.1
20.	* 1.9	1.8	1.1	1.1	.5	.3	.8	.8	1.0	.9	.9	1.0	1.0	1.1	1.2	.7	.4	.4	.1	.1
25.	* 2.0	1.6	1.1	.9	.3	.3	.8	.9	1.0	.9	.9	1.0	1.1	1.1	1.2	.6	.4	.3	.1	.1
30.	* 2.0	1.5	.8	1.0	.3	.3	.8	.9	1.0	.9	1.0	1.0	1.1	1.1	1.2	.7	.2	.3	.1	.1
35.	* 2.1	1.4	.8	1.0	.3	.3	1.0	1.1	1.0	.9	.9	1.1	1.1	1.1	1.2	.6	.2	.3	.0	.1
40.	* 2.1	1.5	.8	1.0	.3	.3	1.0	1.1	1.1	.9	.9	1.2	1.2	1.2	1.3	.6	.2	.3	.0	.1
45.	* 2.1	1.3	1.0	1.0	.3	.4	1.0	1.1	1.1	.9	1.0	1.2	1.3	1.3	1.3	.5	.3	.2	.0	.1
50.	* 2.0	1.3	1.1	.9	.3	.4	1.0	1.2	1.2	1.0	1.0	1.3	1.3	1.3	1.1	.5	.3	.2	.0	.1
55.	* 1.9	1.3	1.1	.9	.2	.4	1.1	1.2	1.3	1.0	1.0	1.3	1.3	1.3	1.1	.5	.3	.2	.0	.1
60.	* 2.0	1.5	1.0	.8	.3	.4	1.1	1.1	1.4	1.1	1.2	1.4	1.4	1.4	1.1	.5	.3	.2	.0	.0
65.	* 1.9	1.4	1.0	.9	.3	.4	1.2	1.2	1.5	1.2	1.1	1.4	1.4	1.4	1.1	.6	.3	.2	.0	.0
70.	* 1.8	1.3	1.0	.7	.2	.5	1.3	1.4	1.4	1.0	1.1	1.6	1.4	1.3	.9	.5	.2	.2	.0	.0
75.	* 1.8	1.4	.9	.7	.2	.4	1.3	1.4	1.3	1.0	.9	1.4	1.4	1.4	.8	.5	.2	.2	.0	.0
80.	* 1.6	1.4	.8	.6	.1	.3	1.3	1.3	1.2	1.0	1.0	1.2	1.2	1.2	.7	.5	.2	.2	.0	.0
85.	* 1.4	1.3	.7	.5	.0	.2	1.1	1.2	1.2	.7	.8	1.1	1.1	1.0	.6	.5	.2	.2	.0	.0
90.	* 1.3	1.1	.6	.5	.0	.1	.9	1.0	.9	.6	.7	.9	.9	.8	.5	.4	.2	.2	.0	.0
95.	* .9	1.0	.5	.5	.0	.0	.8	.7	.8	.4	.5	.7	.7	.6	.4	.4	.2	.2	.0	.0
100.	* .6	.6	.5	.5	.0	.0	.4	.5	.5	.3	.3	.5	.4	.4	.3	.2	.2	.0	.0	.0
105.	* .3	.5	.5	.5	.0	.0	.2	.2	.2	.2	.3	.3	.3	.4	.2	.3	.2	.2	.0	.0
110.	* .4	.5	.6	.6	.0	.0	.2	.2	.3	.1	.2	.2	.2	.2	.1	.2	.2	.0	.0	.0
115.	* .3	.4	.6	.6	.0	.0	.1	.1	.2	.1	.2	.2	.2	.2	.1	.2	.2	.0	.0	.0
120.	* .3	.5	.6	.6	.0	.0	.0	.0	.1	.1	.2	.2	.2	.2	.2	.2	.2	.0	.0	.0
125.	* .2	.5	.6	.6	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.2	.2	.0	.0	.0
130.	* .3	.6	.7	.7	.0	.0	.0	.1	.1	.1	.3	.1	.1	.1	.1	.2	.2	.0	.0	.0
135.	* .3	.6	.7	.7	.0	.0	.0	.0	.1	.1	.3	.1	.1	.1	.1	.2	.2	.0	.0	.0
140.	* .3	.7	.7	.7	.0	.0	.0	.0	.1	.1	.3	.1	.1	.1	.1	.2	.2	.0	.0	.0
145.	* .3	.7	.7	.7	.0	.0	.0	.0	.1	.1	.3	.1	.1	.1	.1	.2	.2	.0	.0	.0
150.	* .3	.7	.7	.7	.0	.0	.0	.0	.1	.1	.3	.1	.1	.1	.1	.2	.2	.0	.0	.0

155.	*	.3	.8	.8	.8	.1	.1	.1	.0	.0	.1	.3	.1	.1	.1	.1	.3	.3	.3	.0	.0
160.	*	.3	.8	.8	.8	.2	.2	.2	.0	.0	.1	.3	.1	.1	.1	.1	.3	.3	.3	.0	.1
165.	*	.2	.8	.8	.8	.4	.4	.4	.0	.0	.1	.2	.1	.1	.1	.3	.3	.3	.1	.1	
170.	*	.2	.8	.8	.7	.5	.5	.0	.0	.1	.2	.2	.0	.1	.1	.3	.3	.3	.2	.2	
175.	*	.2	.7	.7	.6	.7	.7	.8	.1	.0	.0	.2	.2	.0	.1	.1	.2	.2	.2	.3	.3
180.	*	.1	.6	.5	.4	1.0	1.0	1.0	.2	.1	.0	.1	.3	.0	.0	.1	.2	.2	.2	.3	.4
185.	*	.1	.3	.3	.3	1.1	1.1	1.1	.2	.1	.0	.1	.3	.1	.0	.0	.1	.1	.1	.4	.4
190.	*	.0	.2	.2	.1	1.2	1.2	1.1	.3	.1	.1	.1	.4	.1	.0	.0	.1	.1	.1	.4	.4
195.	*	.0	.1	.1	.1	1.2	1.2	1.2	.3	.2	.1	.1	.4	.1	.0	.0	.0	.0	.0	.4	.4
200.	*	.0	.0	.0	.0	1.2	1.3	1.1	.3	.2	.1	.1	.5	.1	.0	.0	.0	.0	.0	.4	.4
205.	*	.0	.0	.0	.0	1.1	1.2	1.0	.4	.2	.1	.1	.4	.2	.1	.0	.0	.0	.0	.4	.4

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JOB: Brent Spence Bridge

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WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

210.	*	.0	.0	.0	.0	1.1	1.2	.9	.4	.2	.1	.1	.4	.2	.2	.0	.0	.0	.0	.4	.4	
215.	*	.0	.0	.0	.0	1.0	1.0	.8	.4	.2	.1	.1	.4	.2	.2	.1	.0	.0	.0	.3	.3	
220.	*	.0	.0	.0	.0	1.0	1.0	.7	.4	.2	.1	.1	.3	.2	.2	.2	.1	.0	.0	.3	.3	
225.	*	.0	.0	.0	.0	.8	.8	.5	.4	.2	.1	.1	.3	.2	.2	.2	.1	.1	.0	.3	.3	
230.	*	.0	.0	.0	.0	.8	.8	.4	.4	.2	.1	.1	.3	.2	.2	.2	.1	.1	.1	.3	.4	
235.	*	.0	.0	.0	.0	.8	.8	.4	.3	.2	.1	.1	.2	.2	.3	.3	.2	.1	.1	.4	.4	
240.	*	.0	.1	.0	.0	.8	.8	.3	.3	.3	.1	.1	.2	.3	.3	.3	.2	.1	.1	.4	.4	
245.	*	.1	.1	.0	.0	.7	.7	.3	.4	.2	.1	.1	.2	.3	.3	.2	.2	.1	.1	.4	.4	
250.	*	.3	.3	.0	.0	.7	.5	.6	.3	.2	.2	.3	.4	.4	.3	.3	.1	.1	.4	.4		
255.	*	.5	.5	.0	.0	.7	.7	.6	.3	.2	.3	.6	.6	.5	.5	.5	.1	.1	.4	.4		
260.	*	.7	.8	.2	.0	.7	.9	1.0	1.0	1.0	.6	.6	.9	1.1	.8	.9	.8	.3	.1	.4	.5	
265.	*	1.2	1.3	.3	.2	.9	1.0	1.3	1.3	1.4	.8	.8	1.3	1.2	1.1	1.1	1.1	1.1	.4	.3	.6	.6
270.	*	1.5	1.7	.4	.2	.9	1.1	1.7	1.7	1.5	1.2	1.1	1.4	1.5	1.6	1.4	1.4	.4	.4	.6	.7	
275.	*	1.7	1.9	.6	.4	1.1	1.3	2.0	1.7	1.7	1.3	1.2	1.5	1.7	1.7	1.6	1.5	.5	.3	.6	.8	
280.	*	1.8	2.0	.6	.4	1.1	1.3	1.9	1.9	1.9	1.4	1.2	1.7	1.7	1.8	1.6	1.6	.6	.3	.6	.8	
285.	*	1.8	2.0	.6	.4	1.1	1.3	1.9	1.8	1.8	1.3	1.3	1.7	1.8	1.7	1.6	1.6	.5	.3	.6	.8	
290.	*	1.7	1.9	.6	.4	1.1	1.4	1.9	1.6	1.7	1.3	1.2	1.5	1.5	1.5	1.5	1.4	.6	.2	.6	.9	
295.	*	1.7	1.9	.6	.4	1.1	1.4	1.7	1.6	1.5	1.2	1.1	1.5	1.5	1.5	1.5	1.3	.6	.4	.7	.9	
300.	*	1.7	1.9	.6	.4	1.2	1.4	1.6	1.5	1.3	1.1	1.2	1.2	1.4	1.5	1.5	1.2	.6	.4	.7	.9	
305.	*	1.6	1.6	.6	.4	1.2	1.5	1.6	1.5	1.3	1.0	1.1	1.2	1.4	1.4	1.4	1.0	.6	.4	.7	.8	
310.	*	1.5	1.6	.6	.3	1.1	1.5	1.6	1.4	1.4	1.0	.9	1.3	1.4	1.4	1.4	.9	.6	.4	.7	.8	
315.	*	1.5	1.6	.6	.3	1.2	1.5	1.6	1.4	1.3	1.0	.9	1.2	1.3	1.4	1.4	.8	.6	.4	.7	.7	
320.	*	1.5	1.5	.6	.3	1.4	1.4	1.7	1.4	1.3	.9	.9	1.2	1.3	1.3	1.3	.8	.5	.4	.6	.7	
325.	*	1.4	1.4	.6	.4	1.4	1.6	1.7	1.4	1.2	.9	.9	1.2	1.2	1.2	1.2	.6	.5	.4	.6	.7	
330.	*	1.4	1.3	.6	.4	1.4	1.5	1.7	1.4	1.2	.9	.9	1.2	1.2	1.2	1.1	.6	.5	.4	.6	.6	
335.	*	1.4	1.4	.6	.4	1.6	1.5	1.9	1.3	1.1	1.0	.9	1.3	1.2	1.2	1.1	.5	.5	.3	.7	.6	
340.	*	1.4	1.4	.7	.5	1.7	1.8	1.9	1.3	1.1	1.0	.9	1.3	1.2	1.2	1.1	.6	.4	.3	.6	.7	
345.	*	1.4	1.5	.8	.5	1.7	1.8	2.0	1.3	1.1	1.0	1.0	1.3	1.2	1.1	1.1	.6	.5	.4	.6	.7	
350.	*	1.5	1.7	.9	.7	1.7	1.6	2.0	1.2	1.1	.9	1.0	1.3	1.2	1.1	1.1	.6	.4	.4	.5	.5	
355.	*	1.7	2.1	1.2	.9	1.7	1.5	1.9	1.1	1.1	.8	1.0	1.3	1.2	1.0	1.0	.7	.4	.3	.4	.4	
360.	*	1.8	2.3	1.3	1.1	1.4	1.2	1.8	1.0	1.1	.8	1.0	1.2	1.0	1.0	1.1	.8	.4	.3	.3	.4	

MAX	*	2.1	2.3	1.3	1.4	1.7	1.8	2.0	1.9	1.9	1.4	1.3	1.7	1.8	1.8	1.6	1.6	.6	.4	.7	.9	
DEGR.	*	35	0	15	10	340	340	275	280	280	280	280	285	280	285	280	275	280	280	5	295	290

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JOB: Brent Spence Bridge

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MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37
REC38 REC39 REC40

0.	*	.5	.3	.0	.2	.2	.2	.9	1.0	.5	.1	.0	.0	.2	.2	.1	.4	.4	.4	.1	.1
5.	*	.4	.3	.0	.1	.1	.1	.9	1.0	.6	.1	.0	.0	.1	.1	.1	.3	.3	.3	.1	.1
10.	*	.4	.3	.0	.1	.1	.1	1.0	1.0	.6	.1	.0	.0	.1	.1	.1	.4	.4	.5	.1	.0
15.	*	.3	.3	.0	.0	.0	.0	1.0	1.0	.6	.2	.1	.0	.0	.0	.0	.5	.5	.5	.1	.0
20.	*	.3	.3	.0	.0	.0	.0	.9	.9	.6	.2	.1	.0	.0	.0	.0	.4	.3	.3	.1	.1
25.	*	.3	.3	.0	.0	.0	.0	.8	.9	.6	.2	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1
30.	*	.3	.3	.0	.0	.0	.0	.8	.8	.5	.2	.1	.1	.0	.0	.0	.3	.3	.3	.1	.1
35.	*	.3	.3	.0	.0	.0	.0	.7	.8	.5	.2	.1	.1	.1	.0	.0	.3	.3	.3	.1	.1
40.	*	.3	.3	.0	.0	.0	.0	.7	.7	.5	.2	.1	.1	.1	.1	.0	.3	.3	.2	.1	.1
45.	*	.4	.3	.0	.0	.0	.0	.6	.6	.4	.2	.1	.1	.1	.1	.0	.3	.3	.3	.1	.1
50.	*	.4	.3	.0	.0	.0	.0	.6	.6	.4	.2	.1	.1	.1	.1	.1	.3	.4	.3	.2	.1
55.	*	.4	.2	.0	.0	.0	.0	.6	.6	.3	.2	.1	.2	.2	.1	.1	.4	.4	.3	.2	.1
60.	*	.4	.2	.0	.0	.0	.0	.5	.6	.3	.3	.2	.2	.2	.1	.1	.4	.4	.2	.2	.2
65.	*	.4	.2	.0	.0	.0	.0	.5	.5	.3	.3	.2	.2	.2	.1	.1	.4	.4	.2	.2	.2
70.	*	.4	.2	.0	.0	.0	.0	.5	.5	.3	.2	.2	.2	.3	.1	.1	.4	.4	.4	.4	.3
75.	*	.3	.2	.0	.0	.0	.0	.5	.5	.4	.2	.4	.4	.4	.1	.1	.4	.4	.5	.5	.4
80.	*	.3	.1	.0	.1	.0	.0	.5	.5	.3	.4	.4	.6	.6	.1	.1	.4	.3	.5	.6	.6
85.	*	.3	.1	.0	.1	.0	.0	.5	.5	.4	.5	.7	.8	.7	.1	.1	.4	.3	.8	.8	.8
90.	*	.2	.1	.1	.2	.0	.0	.5	.5	.5	.6	.8	.9	1.0	.1	.1	.3	.3	1.0	.9	1.1
95.	*	.1	.0	.1	.2	.0	.0	.5	.5	.5	.6	1.0	1.1	1.2	.3	.1	.4	.4	1.2	1.3	1.3
100.	*	.1	.0	.1	.3	.0	.0	.5	.5	.5	.8	1.2	1.2	1.4	.2	.1	.4	.5	1.3	1.3	1.3
105.	*	.1	.0	.1	.3	.0	.0	.5	.5	.5	.8	1.3	1.3	1.5	.2	.1	.3	.6	1.4	1.4	1.4
110.	*	.0	.0	.2	.3	.0	.0	.5	.6	.6	.9	1.2	1.3	1.4	.4	.0	.5	.6	1.4	1.4	1.4
115.	*	.0	.0	.2	.3	.0	.0	.5	.6	.5	1.1	1.4	1.4	1.4	.4	.2	.5	.7	1.4	1.3	1.3

120.	*	.0	.0	.2	.3	.0	.0	.6	.7	.5	1.0	1.4	1.4	1.4	.4	.2	.5	.8	1.3	1.2	1.4
125.	*	.0	.0	.2	.3	.1	.0	.6	.7	.5	1.1	1.3	1.3	1.3	.5	.2	.5	.8	1.2	1.2	1.2
130.	*	.0	.0	.2	.3	.1	.0	.6	.7	.6	1.1	1.3	1.3	1.3	.6	.2	.5	.8	1.3	1.2	1.2
135.	*	.0	.0	.3	.3	.1	.0	.6	.7	.6	1.2	1.2	1.2	1.3	.6	.3	.6	.9	1.1	1.2	1.2
140.	*	.0	.0	.3	.3	.1	.0	.8	.8	.6	1.2	1.2	1.2	1.2	.5	.4	.7	.8	1.2	1.0	1.1
145.	*	.0	.0	.3	.3	.1	.0	.8	.8	.6	1.1	1.1	1.1	1.1	.5	.4	.7	.8	1.2	1.0	1.0
150.	*	.0	.0	.3	.3	.1	.1	.9	.8	.6	1.1	1.1	1.1	1.1	.5	.4	.7	.8	1.2	1.0	1.0
155.	*	.0	.0	.3	.3	.1	.1	.9	.9	.6	1.1	1.1	1.1	1.1	.5	.4	.7	.7	1.2	1.0	1.0
160.	*	.1	.0	.3	.3	.1	.1	1.1	1.1	.6	1.0	1.1	1.1	1.1	.5	.4	.8	.8	1.1	1.0	.9
165.	*	.1	.0	.3	.4	.2	.2	1.1	1.1	.7	1.0	1.1	1.1	1.1	.5	.4	.8	.7	1.1	1.0	.9
170.	*	.2	.0	.3	.5	.2	.2	1.1	1.1	.7	1.0	1.1	1.0	1.1	.5	.4	.6	.6	1.1	1.0	.9
175.	*	.3	.1	.4	.5	.3	.2	1.1	1.0	.6	1.1	1.1	1.0	1.2	.5	.5	.6	.5	1.1	1.0	.9
180.	*	.4	.1	.4	.6	.3	.4	.9	.9	.6	1.1	1.0	1.0	1.2	.4	.5	.6	.5	1.0	.9	1.0
185.	*	.4	.1	.4	.6	.3	.3	.9	.8	.5	1.0	1.0	1.1	1.2	.4	.5	.5	.4	1.0	.9	1.0
190.	*	.4	.2	.5	.6	.4	.5	.7	.8	.5	1.0	1.0	1.1	1.2	.6	.6	.4	.3	1.0	1.0	1.0
195.	*	.4	.2	.5	.6	.4	.5	.5	.8	.4	1.0	1.0	1.1	1.2	.6	.6	.4	.4	1.0	1.0	1.1
200.	*	.4	.2	.5	.5	.4	.6	.4	.5	.4	1.0	1.1	1.1	1.2	.7	.6	.4	.4	1.0	1.0	1.1
205.	*	.4	.2	.4	.5	.3	.6	.4	.5	.5	1.0	1.1	1.2	1.3	.5	.6	.4	.4	1.0	1.0	1.1

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40

210.	*	.4	.1	.4	.4	.5	.6	.3	.5	.5	1.0	1.2	1.2	1.2	.6	.6	.4	.4	1.0	1.0	1.1
215.	*	.3	.1	.4	.4	.6	.6	.5	.5	.6	1.1	1.2	1.2	1.1	.6	.5	.4	.5	1.0	1.1	1.1
220.	*	.3	.1	.4	.4	.7	.7	.5	.6	.8	1.3	1.3	1.3	1.2	.7	.6	.4	.6	1.1	1.1	1.3
225.	*	.4	.1	.4	.5	.8	.8	.5	.6	.9	1.3	1.4	1.4	1.3	.8	.6	.4	.6	1.2	1.2	1.3
230.	*	.4	.2	.5	.6	.8	.7	.5	.7	.9	1.4	1.4	1.4	1.3	.8	.6	.4	.5	1.2	1.2	1.3
235.	*	.3	.2	.6	.7	.8	.7	.4	.7	1.1	1.4	1.4	1.4	1.2	.8	.6	.4	.5	1.3	1.2	1.2
240.	*	.3	.2	.6	.7	.9	.7	.4	.7	1.2	1.4	1.6	1.5	1.4	.8	.6	.4	.5	1.4	1.3	1.3
245.	*	.3	.2	.6	.8	.9	.6	.3	.6	1.3	1.5	1.5	1.5	1.5	.7	.6	.3	.6	1.4	1.3	1.5
250.	*	.5	.3	.8	.9	.8	.6	.3	.5	1.5	1.6	1.6	1.7	1.6	.7	.6	.4	.5	1.6	1.6	1.7
255.	*	.5	.5	.8	1.1	.8	.6	.3	.5	1.6	1.7	1.8	1.8	1.7	.7	.6	.6	.5	1.6	1.6	1.8
260.	*	.7	.6	.9	1.2	.8	.6	.3	.5	1.6	1.6	1.7	1.6	1.6	.8	.7	.6	.7	1.6	1.6	1.7
265.	*	.9	.8	1.0	1.2	.8	.6	.3	.5	1.5	1.4	1.6	1.7	1.5	.8	.7	.5	.6	1.4	1.6	1.7
270.	*	1.2	.9	.9	1.1	.6	.6	.3	.3	1.3	1.3	1.4	1.4	1.3	.7	.6	.4	.6	1.3	1.4	1.7
275.	*	1.2	.9	.8	.9	.6	.6	.3	.4	1.1	1.0	1.0	1.2	1.2	.7	.5	.4	.5	1.0	1.2	1.3
280.	*	1.2	1.0	.6	.6	.5	.4	.1	.2	.9	.7	.8	.9	1.0	.6	.3	.2	.4	.9	.9	1.0
285.	*	1.1	.8	.4	.5	.4	.4	.1	.1	.5	.5	.4	.5	.6	.3	.3	.1	.2	.7	.6	.6
290.	*	.9	.9	.2	.5	.4	.4	.1	.1	.3	.3	.4	.4	.4	.3	.3	.1	.2	.4	.4	.4
295.	*	.9	.7	.2	.4	.4	.4	.1	.1	.2	.2	.3	.3	.2	.3	.3	.1	.1	.2	.2	.3
300.	*	.7	.7	.3	.4	.4	.4	.1	.2	.2	.3	.3	.3	.2	.3	.3	.1	.1	.2	.2	.3
305.	*	.7	.6	.3	.4	.4	.4	.2	.2	.2	.2	.2	.2	.3	.3	.3	.1	.1	.1	.2	.3
310.	*	.6	.6	.3	.4	.4	.4	.2	.2	.1	.2	.2	.2	.3	.3	.3	.1	.1	.1	.2	.3
315.	*	.6	.6	.3	.4	.4	.4	.2	.2	.1	.2	.2	.2	.3	.3	.3	.1	.1	.1	.1	.3
320.	*	.5	.6	.3	.5	.5	.4	.2	.2	.1	.2	.2	.2	.3	.3	.3	.1	.1	.1	.1	.3
325.	*	.7	.6	.3	.5	.5	.4	.2	.2	.1	.1	.2	.2	.3	.3	.3	.1	.1	.1	.1	.3
330.	*	.7	.6	.3	.6	.6	.5	.2	.3	.1	.1	.2	.2	.4	.3	.3	.1	.1	.1	.1	.2
335.	*	.9	.6	.3	.6	.6	.5	.3	.3	.1	.1	.2	.2	.4	.4	.4	.1	.1	.1	.2	.2
340.	*	.8	.6	.2	.6	.6	.5	.4	.4	.2	.1	.1	.2	.4	.4	.4	.1	.1	.1	.2	.2
345.	*	.8	.5	.2	.6	.4	.4	.5	.6	.2	.1	.1	.2	.4	.4	.4	.2	.2	.2	.2	.2
350.	*	.7	.4	.1	.4	.3	.3	.6	.7	.2	.1	.1	.2	.4	.3	.3	.2	.2	.2	.1	.2
355.	*	.6	.4	.1	.3	.2	.2	.7	.8	.4	.0	.0	.1	.3	.3	.3	.3	.3	.1	.2	.2
360.	*	.5	.3	.0	.2	.2	.2	.9	1.0	.5	.1	.0	.0	.2	.2	.1	.4	.4	.4	.1	.1

MAX * 1.2 1.0 1.0 1.2 .9 .8 1.1 1.1 1.6 1.7 1.8 1.8 1.7 .8 .7 .8 .9 1.6 1.6 1.8
 DEGR. * 270 280 265 260 240 225 160 160 255 255 255 255 255 225 260 160 135 250 250 255

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

0.	*	.2	.9	.8	.8	1.5	1.5	1.5	.3
5.	*	.1	.7	.7	.7	1.7	1.7	1.7	.3
10.	*	.1	.4	.4	.3	1.7	1.8	1.8	.5
15.	*	.0	.2	.2	.2	1.7	1.9	1.8	.5
20.	*	.0	.1	.1	.1	1.7	1.7	1.6	.4
25.	*	.0	.1	.1	.0	1.6	1.6	1.5	.5
30.	*	.0	.0	.0	.0	1.6	1.6	1.5	.6
35.	*	.1	.0	.0	.0	1.5	1.5	1.4	.6
40.	*	.1	.0	.0	.0	1.3	1.3	1.1	.6
45.	*	.1	.0	.0	.0	1.2	1.2	1.1	.6
50.	*	.1	.0	.0	.0	1.2	1.2	1.0	.7
55.	*	.1	.0	.0	.0	1.2	1.2	1.0	.5
60.	*	.1	.0	.0	.0	1.1	1.1	.9	.5
65.	*	.1	.1	.0	.0	1.0	1.0	.9	.6
70.	*	.2	.2	.0	.0	1.0	1.0	.9	.6
75.	*	.3	.3	.0	.0	1.0	1.0	.9	.9

80. * .6 .6 .0 .0 1.0 1.0 1.3 1.1
 85. * .9 .9 .1 .0 1.0 1.1 1.4 1.5
 90. * 1.1 1.1 .2 .0 1.0 1.2 1.7 1.7
 95. * 1.4 1.3 .3 .0 1.1 1.3 1.8 2.0
 100. * 1.4 1.5 .3 .2 1.2 1.4 2.0 2.1
 105. * 1.5 1.4 .5 .2 1.2 1.5 1.9 2.1
 110. * 1.3 1.4 .5 .2 1.3 1.4 1.8 2.1
 115. * 1.2 1.3 .4 .3 1.3 1.4 1.8 2.2
 120. * 1.2 1.2 .4 .2 1.5 1.5 1.8 2.1
 125. * 1.1 1.2 .4 .2 1.5 1.7 1.7 2.0
 130. * 1.2 1.1 .4 .3 1.5 1.7 1.8 2.0
 135. * 1.2 1.1 .4 .3 1.5 1.6 1.7 2.0
 140. * 1.0 1.1 .4 .3 1.7 1.6 1.6 2.0
 145. * .9 .9 .3 .3 1.8 1.6 1.7 2.0
 150. * .9 .9 .3 .3 1.8 1.7 1.8 1.8
 155. * .9 1.0 .3 .4 2.0 1.8 1.8 1.8
 160. * .9 1.0 .5 .4 1.9 1.8 1.9 1.8
 165. * .9 1.3 .5 .5 1.9 1.9 1.9 1.8
 170. * .9 1.4 .6 .6 1.8 1.7 1.9 1.7
 175. * 1.0 1.6 .8 .9 1.8 1.7 2.1 1.8
 180. * 1.1 1.7 1.1 1.0 1.6 1.4 2.0 1.7
 185. * 1.1 1.7 1.2 1.2 1.3 1.2 1.6 1.7
 190. * 1.2 1.8 1.2 1.2 1.0 .9 1.5 1.5
 195. * 1.2 1.7 1.2 1.4 .8 .9 1.4 1.5
 200. * 1.3 1.5 1.2 1.4 .7 .7 1.4 1.5
 205. * 1.3 1.5 1.2 1.4 .5 .7 1.3 1.5

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48

210. * 1.3 1.5 1.3 1.4 .5 .7 1.5 1.5
 215. * 1.3 1.4 1.4 1.4 .5 .7 1.5 1.6
 220. * 1.4 1.6 1.6 1.4 .4 .8 1.6 1.6
 225. * 1.4 1.4 1.6 1.4 .4 .7 1.7 1.7
 230. * 1.4 1.5 1.6 1.3 .4 .6 1.7 1.8
 235. * 1.3 1.6 1.6 1.3 .4 .6 1.9 1.8
 240. * 1.5 1.7 1.5 1.3 .4 .6 2.0 2.0
 245. * 1.5 2.2 1.6 1.3 .4 .6 2.1 2.0
 250. * 1.6 2.3 1.6 1.3 .4 .6 2.2 2.1
 255. * 2.0 2.4 1.6 1.3 .4 .7 2.2 2.1
 260. * 1.9 2.5 1.5 1.3 .4 .6 2.3 2.1
 265. * 2.1 2.5 1.4 1.2 .3 .5 2.0 2.0
 270. * 1.9 2.3 1.3 1.1 .2 .4 1.8 1.6
 275. * 1.5 2.0 1.2 1.1 .2 .3 1.3 1.3
 280. * 1.1 1.5 1.1 .9 .0 .2 .9 .8
 285. * .8 1.2 .9 .9 .0 .0 .5 .5
 290. * .6 1.1 .9 .9 .0 .0 .3 .3
 295. * .4 .8 .9 .9 .0 .0 .1 .2
 300. * .4 .9 .9 .9 .0 .0 .1 .1
 305. * .4 .9 1.0 1.0 .0 .0 .0 .0
 310. * .4 .9 1.0 1.0 .1 .1 .0 .0
 315. * .4 1.0 1.0 1.0 .1 .1 .1 .0
 320. * .4 1.0 1.0 1.0 .1 .1 .1 .0
 325. * .5 1.0 1.0 1.0 .1 .1 .1 .0
 330. * .5 1.2 1.1 1.1 .1 .1 .1 .0
 335. * .5 1.2 1.1 1.1 .2 .2 .2 .0
 340. * .5 1.3 1.2 1.1 .4 .4 .4 .0
 345. * .4 1.3 1.3 1.1 .5 .6 .6 .0
 350. * .3 1.3 1.3 1.1 .8 .8 .8 .1
 355. * .3 1.1 1.0 .9 1.1 1.2 1.2 .2
 360. * .2 .9 .8 .8 1.5 1.5 1.5 .3

MAX * 2.1 2.5 1.6 1.4 2.0 1.9 2.3 2.2

DEGR.* 265 260 220 205 155 15 260 115

THE HIGHEST CONCENTRATION IS 2.50 PPM AT 260 DEGREES FROM REC42.
 THE 2ND HIGHEST CONCENTRATION IS 2.30 PPM AT 0 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS 2.30 PPM AT 260 DEGREES FROM REC47.

1

JOB: Brent Spence Bridge

RUN: W 5th Street & Bakewell

DATE: 08/31/2010 TIME: 10:46:56.72

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)

* ANGLE (DEGREES)

* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

LINK #* 35 0 15 10 340 340 275 280 280 280 285 280 285 280 275 280 280 5 295 290

1 * .5 .5 .1 .1 .1 .1 .4 .2 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
 2 * .5 .1 .0 .0 .1 .0 .6 .3 .2 .2 .1 .1 .1 .1 .1 .1 .1 .0 .0 .0
 3 * .0 .0 .1 .1 .0 .1 .1 .4 .5 .3 .2 .1 .1 .1 .0 .0 .0 .0 .0 .0
 4 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2 .3 .1 .1 .0 .0 .0 .0 .0 .0
 5 * .0
 6 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .2 .5 .6 .6 .7 .1 .1 .1 .2
 7 * .5 .5 .2 .2 .2 .2 .8 .9 .9 .7 .7 .9 .9 .9 .8 .4 .0 .2 .3
 8 * .0
 9 * .0 .0 .1 .1 .2 .2 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM
 DATE: 08/31/2010 TIME: 13:52:55.55

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 NB Cent McF Appr	* 270186.0	289164.0	270108.0	289529.0	*	373.	348.	AG	310.	12.6	.0	44.0		
2. 2 NB Thr W 4th Appr	* 270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	240.	12.6	.0	44.0		
3. 3 NB Cent NB Queue	* 270067.0	289730.0	270072.7	289707.8	*	23.	166.	AG	229.	100.0	.0	24.0	.23	1.2
4. 4 NB Cen W 4th Depr	* 270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	500.	12.6	.0	44.0		
5. 5 NB Cen W 4th Dept	* 270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	500.	12.6	.0	44.0		
6. 6 NB Lt W 4th Appr	* 270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	70.	12.6	.0	44.0		
7. 7 NB LefttNB Queue	* 270049.0	289728.0	270085.1	289578.4	*	154.	166.	AG	360.	100.0	.0	24.0	1.46	7.8
8. 10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168.	AG	220.	12.6	.0	44.0		
9. 11 SB CentSB Queue	* 270007.0	289828.0	270002.1	289851.6	*	24.	348.	AG	262.	100.0	.0	24.0	.28	1.2
10. 12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166.	AG	230.	12.6	.0	44.0		
11. 13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168.	AG	230.	12.6	.0	44.0		
12. 14 WB W 4tTo Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259.	AG	560.	12.6	.0	44.0		
13. 15 WB W 4tFr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257.	AG	560.	12.6	.0	44.0		
14. 16 WB W 4tTo Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258.	AG	560.	12.6	.0	56.0		
15. 17 WB W 4tWB Queue	* 270089.0	289764.0	270126.8	289772.2	*	39.	78.	AG	374.	100.0	.0	36.0	.41	2.0
16. 16 WB W 4tFrom Cent	* 270040.0	289746.0	269741.0	289687.0	*	305.	259.	AG	360.	12.6	.0	56.0		
17. 16 WB W 4tTo CD	* 269740.0	289694.0	269544.0	289656.0	*	200.	259.	AG	250.	12.6	.0	44.0		
18. 18 WB W 4tRt Queue	* 269564.0	289660.0	269586.8	289664.3	*	23.	79.	AG	223.	100.0	.0	24.0	.25	1.2
19. 19 WB W 4tRt to CD	* 269544.0	289656.0	269495.0	289688.0	*	59.	303.	AG	250.	12.6	.0	44.0		
20. 20 WB W 4tLt to CD	* 269743.0	289676.0	269548.0	289635.0	*	199.	258.	AG	110.	12.6	.0	32.0		
21. 21 WB W 4tLt Queue	* 269568.0	289639.0	269587.4	289643.1	*	20.	78.	AG	108.	100.0	.0	12.0	.19	1.0
22. 22 WB W 4tLt to CD	* 269548.0	289635.0	269512.0	289576.0	*	69.	211.	AG	110.	12.6	.0	32.0		
23. 23 NB CD To W 4th	* 269358.0	289340.0	269495.0	289688.0	*	374.	21.	AG	1070.	12.6	.0	44.0		
24. 24 NB CD NB Queue	* 269451.0	289575.0	269410.2	289471.6	*	111.	202.	AG	216.	100.0	.0	24.0	.82	5.6
25. 25 NB CD Fr W 4th	* 269495.0	289688.0	269471.0	289839.0	*	153.	351.	AG	1320.	12.6	.0	56.0		
26. 26 NB CD Fr W 4th	* 269471.0	289839.0	269432.0	290034.0	*	199.	349.	AG	1320.	12.6	.0	68.0		
27. 27 SB CD To W 4th	* 269353.0	290020.0	269416.0	289697.0	*	329.	169.	AG	1470.	12.6	.0	56.0		
28. 27 SB CD SB Queue	* 269408.0	289737.0	269387.5	289842.1	*	107.	349.	AG	334.	100.0	.0	36.0	.82	5.4
29. 28 SB CD @ W 4th	* 269416.0	289697.0	269512.0	289576.0	*	154.	142.	AG	1470.	12.6	.0	56.0		
30. 29 SB CD @ W 4th	* 269512.0	289576.0	269537.0	289433.0	*	145.	170.	AG	1580.	12.6	.0	56.0		
31. 30 WB Off 3rd-SB 75	* 270480.0	289330.0	270388.0	289332.0	*	92.	271.	BR	280.	12.1	.0	32.0		
32. 31 WB Off 3rd-SB 75	* 270388.0	289332.0	270294.0	289352.0	*	96.	282.	BR	280.	12.1	.0	32.0		
33. 32 WB Off 3rd-SB 75	* 270294.0	289352.0	270197.0	289396.0	*	106.	294.	BR	280.	12.1	.0	32.0		
34. 33 WB Off 3rd-SB 75	* 270197.0	289396.0	270134.0	289442.0	*	78.	306.	BR	280.	12.1	.0	32.0		
35. 34 WB Off 3rd-SB 75	* 270134.0	289442.0	269989.0	289567.0	*	191.	311.	BR	280.	12.1	.0	32.0		
36. 35 WB Off 3rd-SB 75	* 269989.0	289567.0	269874.0	289640.0	*	136.	302.	BR	280.	12.1	.0	32.0		
37. 36 WB Off 3rd-SB 75	* 269874.0	289640.0	269770.0	289675.0	*	110.	289.	AG	280.	12.1	.0	32.0		
38. 37 WB Off 71-SB 75	* 270428.0	289285.0	270297.0	289305.0	*	133.	279.	BR	2500.	12.1	.0	44.0		
39. 38 WB Off 71-SB 75	* 270297.0	289305.0	270202.0	289342.0	*	102.	291.	BR	2500.	12.1	.0	44.0		
40. 39 WB Off 71-SB 75	* 270202.0	289342.0	270133.0	289389.0	*	83.	304.	BR	2500.	12.1	.0	44.0		
41. 40 WB Off 71-SB 75	* 270133.0	289389.0	270002.0	289505.0	*	175.	312.	BR	2500.	12.1	.0	44.0		
42. 41 WB Off 71-SB 75	* 270002.0	289505.0	269880.0	289607.0	*	159.	310.	BR	2500.	12.1	.0	44.0		
43. 42 WB Off 71-SB 75	* 269880.0	289607.0	269770.0	289675.0	*	129.	302.	BR	2500.	12.1	.0	44.0		
44. 43 WB Off 71-SB 75	* 269770.0	289675.0	269688.0	289703.0	*	87.	289.	BR	2780.	12.1	.0	56.0		

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM
 DATE: 08/31/2010 TIME: 13:52:55.55

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
45. 44 WB Off 71-SB 75	* 269688.0	289703.0	269608.0	289715.0	*	81.	279.	BR	2780.	12.1	.0	56.0		
46. 45 WB Off 71-SB 75	* 269608.0	289715.0	269523.0	289714.0	*	85.	269.	BR	2780.	12.1	.0	56.0		
47. 46 WB Off 71-SB 75	* 269523.0	289714.0	269442.0	289700.0	*	82.	260.	BR	2780.	12.1	.0	56.0		
48. 47 WB Off 71-SB 75	* 269442.0	289700.0	269379.0	289680.0	*	66.	252.	BR	2780.	12.1	.0	56.0		
49. 48 WB Off 71-SB 75	* 269379.0	289680.0	269317.0	289651.0	*	68.	245.	BR	2780.	12.1	.0	56.0		
50. 49 WB Off 71-SB 75	* 269317.0	289651.0	269246.0	289603.0	*	86.	236.	BR	2780.	12.1	.0	56.0		

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM
 DATE: 08/31/2010 TIME: 13:52:55.55

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	EM	FAC	TYPE	RATE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
3. 3 NB Cent NB Queue	* 60	35	2.0	240	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 60	55	2.0	70	1474	73.30	1	3
9. 11 SB CentSB Queue	* 60	40	2.0	220	1501	73.30	1	3
15. 17 WB W 4tWB Queue	* 60	38	2.0	560	1504	73.30	1	3
18. 18 WB W 4tRt Queue	* 60	34	2.0	250	1349	73.30	1	3
21. 21 WB W 4tLt Queue	* 60	33	2.0	110	1550	73.30	1	3
24. 24 NB CD NB Queue	* 60	33	2.0	1070	1707	73.30	1	3
28. 27 SB CD SB Queue	* 60	34	2.0	1470	1628	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT)			*
	X	Y	Z	
1. R1 SE Mid	270140.0	289517.0	5.0	*
2. R2 SE 164	270124.0	289585.0	5.0	*
3. R3 SE 82	270105.0	289664.0	5.0	*
4. R4 SE Corner	270088.0	289735.0	5.0	*
5. R5 SE 82	270158.0	289749.0	5.0	*
6. R6 SE 164	270239.0	289766.0	5.0	*
7. R7 SE Mid	270274.0	289773.0	5.0	*
8. R8 NE Mid	270256.0	289830.0	5.0	*
9. R9 NE 164	270223.0	289823.0	5.0	*
10. R10 NE 82	270142.0	289806.0	5.0	*
11. R11 NE Corner	270072.0	289791.0	5.0	*
12. R12 NE 82	270057.0	289862.0	5.0	*
13. R13 NE 164	270040.0	289942.0	5.0	*
14. R14 NE Mid	270034.0	289968.0	5.0	*
15. R15 NW 164	269944.0	290010.0	5.0	*
16. R16 NW 82	269961.0	289930.0	5.0	*
17. R17 NW Corner	269976.0	289859.0	5.0	*
18. R18 SW Corner	270010.0	289716.0	5.0	*
19. R19 SW 82	270028.0	289646.0	5.0	*
20. R20 SW 164	270046.0	289566.0	5.0	*
21. R21 SW Mid	270055.0	289525.0	5.0	*
22. R22 Near CD	269775.0	289723.0	5.0	*

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JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	.4	.3	.8	.2	.2	.2	.0	.0	.0	.1	.1	.1	.1	.2	.2	.3	.5	.5	.7	
5.	.1	.2	.3	.8	.2	.2	.0	.0	.0	.1	.1	.1	.1	.2	.2	.4	.5	.5	.9	
10.	.1	.2	.3	.9	.2	.2	.0	.0	.0	.0	.0	.0	.1	.2	.3	.3	.5	.8	1.1	
15.	.1	.1	.3	1.0	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.5	.9	1.2	
20.	.1	.1	.2	1.0	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.5	1.0	1.2	
25.	.0	.1	.2	1.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.5	1.2	1.2	
30.	.0	.1	.2	1.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.4	1.3	1.2	
35.	.0	.1	.1	1.1	.3	.3	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.5	1.3	1.1	
40.	.0	.1	.1	1.1	.3	.3	.3	.0	.0	.0	.0	.0	.0	.2	.2	.2	.5	1.2	1.0	
45.	.0	.0	.1	1.0	.3	.3	.3	.0	.0	.0	.0	.0	.0	.2	.2	.2	.5	1.2	1.0	
50.	.0	.0	.1	1.0	.3	.3	.3	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	1.2	.9	
55.	.0	.0	.1	.9	.3	.4	.3	.0	.0	.0	.0	.0	.0	.2	.2	.2	.7	1.2	.8	
60.	.0	.0	.1	.8	.3	.4	.3	.0	.0	.1	.1	.0	.0	.2	.2	.2	.9	1.1	.8	
65.	.0	.0	.0	.7	.3	.3	.3	.1	.1	.1	.1	.0	.0	.2	.2	.2	1.0	1.1	.7	
70.	.0	.0	.0	.6	.3	.3	.3	.1	.1	.1	.1	.0	.0	.2	.2	.2	1.1	1.0	.6	
75.	.0	.0	.0	.5	.2	.3	.3	.2	.2	.2	.3	.0	.0	.2	.2	.2	1.2	.9	.5	
80.	.0	.0	.0	.3	.2	.3	.2	.2	.3	.2	.4	.0	.0	.2	.2	.3	1.3	.9	.4	
85.	.0	.0	.0	.2	.1	.1	.2	.3	.3	.3	.5	.0	.0	.2	.2	.3	1.3	1.0	.4	
90.	.0	.0	.0	.1	.1	.1	.1	.3	.3	.3	.6	.0	.0	.2	.2	.3	1.2	1.0	.3	
95.	.0	.0	.0	.1	.1	.1	.0	.3	.4	.3	.7	.1	.0	.2	.2	.5	1.1	1.0	.3	
100.	.0	.0	.0	.1	.0	.0	.0	.3	.4	.3	.8	.1	.0	.2	.2	.6	1.0	1.0	.2	
105.	.0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.1	.0	.2	.2	.7	1.0	.9	.1	
110.	.0	.0	.0	.0	.0	.0	.0	.3	.3	1.0	.1	.0	.0	.2	.3	.8	1.1	.9	.1	
115.	.0	.0	.0	.0	.0	.0	.0	.3	.3	1.0	.1	.1	.0	.2	.3	.8	1.1	.9	.1	
120.	.1	.0	.0	.0	.0	.0	.0	.2	.3	1.1	.1	.1	.0	.2	.3	.8	1.0	1.0	.2	
125.	.1	.1	.0	.0	.0	.0	.0	.2	.2	1.1	.2	.1	.1	.2	.4	.8	1.0	.9	.4	
130.	.2	.1	.0	.0	.0	.0	.0	.2	.2	1.0	.2	.1	.1	.2	.4	1.0	1.0	1.0	.5	
135.	.2	.1	.1	.0	.0	.0	.0	.2	.2	1.0	.2	.1	.1	.3	.5	1.0	1.1	1.0	.6	
140.	.2	.2	.1	.1	.0	.0	.0	.2	.2	.9	.3	.1	.1	.3	.6	.9	1.1	.9	.8	
145.	.4	.2	.2	.1	.0	.0	.0	.2	.2	.9	.3	.2	.2	.4	.6	.8	1.1	.9	.9	
150.	.4	.3	.2	.2	.1	.0	.0	.2	.2	.3	.8	.3	.2	.3	.4	.6	1.1	.8	.9	
155.	.5	.3	.4	.3	.1	.1	.0	.2	.2	1.1	.4	.4	.4	.3	.6	.7	.9	.8	1.0	
160.	.4	.4	.3	.4	.2	.1	.1	.2	.3	1.1	.5	.4	.4	.4	.5	.6	.7	.7	.9	
165.	.5	.5	.5	.6	.2	.1	.1	.3	.3	1.2	.8	.6	.6	.3	.5	.6	.6	.6	1.0	
170.	.5	.5	.6	.6	.2	.2	.1	.3	.3	1.2	.9	.7	.6	.4	.5	.6	.5	.4	.7	
175.	.5	.5	.6	.9	.3	.2	.2	.3	.3	1.2	1.0	.6	.5	.4	.4	.4	.5	.6	.7	
180.	.7	.6	.7	1.0	.2	.1	.2	.3	.3	1.3	.8	.6	.8	.1	.3	.4	.4	.4	.6	
185.	.8	.7	.6	1.3	.2	.2	.1	.2	.3	1.4	.8	.8	.7	.2	.1	.4	.3	.3	.6	
190.	.7	.7	.7	1.5	.2	.2	.2	.3	.3	1.4	.7	.8	.7	.2	.2	.3	.3	.4	.6	
195.	.7	.6	.8	1.6	.3	.2	.2	.3	.3	1.3	.7	.7	.6	.2	.2	.3	.4	.3	.6	
200.	.8	.6	1.0	1.5	.4	.1	.2	.3	.4	1.1	1.3	.5	.7	.7	.1	.2	.3	.4	.6	
205.	.7	.4	1.2	1.7	.5	.1	.1	.4	.4	1.2	1.2	.5	.7	.7	.2	.1	.3	.3	.4	.6

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JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E AM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

210.	.7	.4	1.2	1.7	.5	.2	.1	.4	.6	1.5	1.0	.6	.6	.5	.2	.4	.3	.3	.6
215.	.7	.4	1.3	1.7	.5	.2	.2	.6	.7	1.4	.9	.7	.5	.4	.1	.2	.3	.3	.6
220.	.7	.4	1.2	1.7	.6	.4	.3	.7	.8	1.4	.8	.7	.5	.5	.2	.2	.3	.3	.6

225.	*	.7	.5	1.2	1.7	.6	.4	.3	.6	.7	1.3	.8	.6	.5	.5	.2	.2	.3	.3	.4	.6
230.	*	.7	.5	1.2	1.7	.6	.3	.4	.7	.7	1.4	.6	.8	.5	.5	.2	.3	.2	.3	.4	.6
235.	*	.7	.5	1.2	1.6	.7	.3	.3	.8	.9	1.2	.6	.8	.5	.5	.1	.4	.4	.4	.3	.7
240.	*	.7	.6	1.2	1.6	.6	.5	.4	.7	.8	1.1	.6	.7	.5	.4	.0	.2	.3	.4	.4	.6
245.	*	.7	.6	1.3	1.6	.7	.5	.5	.7	.7	1.1	.6	.8	.4	.3	.1	.2	.3	.3	.4	.6
250.	*	.8	.8	1.3	1.6	.9	.6	.6	.6	.7	.9	.7	.7	.3	.3	.1	.0	.3	.5	.3	.6
255.	*	.7	.8	1.3	1.5	.8	.6	.5	.4	.6	.8	.8	.8	.4	.4	.2	.1	.2	.6	.4	.6
260.	*	.7	.9	1.3	1.4	1.0	.6	.5	.3	.3	.6	.8	.5	.4	.4	.2	.1	.2	.6	.4	.6
265.	*	.6	1.1	1.4	1.2	1.0	.7	.5	.2	.2	.3	.7	.5	.4	.4	.2	.2	.1	.6	.5	.7
270.	*	.7	1.1	1.3	1.0	1.0	.6	.4	.1	.1	.1	.4	.5	.4	.3	.0	.2	.1	.6	.6	.7
275.	*	.7	1.2	1.4	.7	.9	.5	.4	.1	.1	.4	.4	.5	.3	.3	.0	.2	.2	.6	.5	.7
280.	*	.7	1.3	1.4	.6	.8	.5	.4	.0	.1	.2	.4	.3	.3	.3	.0	.0	.2	.5	.7	.8
285.	*	.6	1.3	1.4	.7	1.0	.4	.4	.1	.1	.2	.5	.3	.3	.3	.0	.0	.0	.3	.6	.9
290.	*	.6	1.2	1.0	.4	1.0	.4	.3	.1	.1	.2	.5	.3	.3	.3	.0	.0	.0	.3	.5	.9
295.	*	.8	1.2	1.0	.5	.9	.4	.3	.1	.1	.1	.5	.3	.3	.3	.0	.0	.0	.2	.3	.8
300.	*	.7	1.0	1.0	.4	1.0	.4	.1	.1	.1	.1	.5	.3	.3	.3	.0	.0	.0	.2	.1	.4
305.	*	.6	1.0	1.1	.5	.8	.4	.4	.1	.1	.1	.4	.3	.3	.3	.0	.0	.0	.2	.1	.3
310.	*	.5	1.0	.9	.6	.8	.3	.3	.1	.1	.1	.5	.4	.4	.4	.0	.0	.0	.2	.1	.1
315.	*	.6	1.0	.8	.7	.7	.3	.3	.1	.1	.1	.5	.4	.4	.4	.0	.0	.0	.2	.1	.0
320.	*	.6	1.1	.8	.7	.6	.3	.3	.0	.1	.1	.5	.4	.4	.4	.0	.0	.0	.2	.1	.0
325.	*	.7	.9	.8	.7	.5	.3	.2	.0	.1	.1	.5	.4	.4	.4	.0	.0	.0	.1	.1	.0
330.	*	.7	.8	.9	.7	.4	.2	.2	.0	.0	.1	.5	.4	.4	.4	.0	.0	.0	.1	.1	.0
335.	*	.6	.9	.8	.8	.4	.2	.2	.0	.0	.1	.5	.4	.4	.4	.0	.0	.0	.1	.2	.1
340.	*	.6	.8	.6	.8	.3	.2	.2	.0	.0	.1	.5	.4	.4	.3	.1	.1	.1	.2	.2	.2
345.	*	.6	.6	.7	.7	.2	.2	.2	.0	.0	.0	.3	.3	.3	.1	.1	.1	.2	.4	.4	.4
350.	*	.5	.5	.6	.7	.2	.2	.2	.0	.0	.0	.2	.2	.2	.2	.2	.2	.2	.5	.5	.5
355.	*	.4	.4	.5	.7	.2	.2	.2	.0	.0	.0	.2	.2	.2	.2	.2	.2	.2	.5	.5	.6
360.	*	.4	.3	.3	.8	.2	.2	.2	.0	.0	.0	.1	.1	.1	.1	.2	.2	.3	.5	.5	.7
MAX	*	.8	1.3	1.4	1.7	1.0	.7	.6	.8	.9	1.5	1.4	1.0	.8	.8	.4	.6	1.0	1.3	1.3	1.2
DEGR.	*	250	280	265	215	265	265	250	235	235	210	185	175	185	180	145	140	130	80	30	15

1

PAGE 6

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22

0.	*	.8	.0
5.	*	1.0	.0
10.	*	1.1	.0
15.	*	1.0	.0
20.	*	1.0	.0
25.	*	.8	.0
30.	*	.7	.0
35.	*	.6	.0
40.	*	.4	.0
45.	*	.3	.0
50.	*	.3	.0
55.	*	.2	.0
60.	*	.2	.0
65.	*	.2	.1
70.	*	.1	.1
75.	*	.1	.2
80.	*	.1	.4
85.	*	.1	.4
90.	*	.2	.3
95.	*	.2	.3
100.	*	.2	.4
105.	*	.3	.4
110.	*	.3	.4
115.	*	.4	.5
120.	*	.5	.8
125.	*	.8	.9
130.	*	.8	1.0
135.	*	.9	1.2
140.	*	1.1	1.2
145.	*	1.1	1.2
150.	*	1.2	1.3
155.	*	1.2	1.1
160.	*	1.2	1.1
165.	*	1.2	.9
170.	*	1.0	1.1
175.	*	.9	.9
180.	*	.8	.9
185.	*	.8	.9
190.	*	.8	.9
195.	*	.8	.9
200.	*	.8	1.0
205.	*	.8	.9

1

PAGE 7

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E AM

WIND ANGLE RANGE: 0.-360.


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42 * .1 .2 .1 .2 .0 .0 .1 .1 .1 .1 .1 .0 .1 .1 .0 .0 .0 .0 .0
43 * .0 .1 .2 .0 .1 .1 .1 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
44 * .0 .1 .1 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
45 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

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1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM

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* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

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REC19 REC20
LINK # * 250 280 265 215 265 265 250 235 235 210 185 175 185 180 145 140 130 80 30 15
-----*-----
46 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
47 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
48 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
49 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0
50 * .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

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1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM
DATE: 08/31/2010 TIME: 13:52:55.55

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

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* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21 REC22

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LINK # * 150 260

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-----*-----
1 * .1 .0
2 * .0 .0
3 * .0 .0
4 * .0 .0
5 * .0 .0
6 * .0 .0
7 * .0 .0
8 * .0 .0
9 * .0 .0
10 * .0 .0
11 * .1 .0
12 * .0 .0
13 * .0 .0
14 * .0 .0
15 * .0 .0
16 * .0 .1
17 * .0 .1
18 * .0 .0
19 * .0 .0
20 * .0 .0
21 * .0 .0
22 * .0 .0
23 * .0 .1
24 * .0 .0
25 * .0 .0
26 * .0 .0
27 * .0 .0
28 * .0 .0
29 * .0 .1
30 * .0 .0
31 * .0 .0
32 * .0 .0
33 * .0 .0
34 * .0 .0
35 * .2 .0
36 * .0 .0
37 * .0 .0
38 * .0 .0
39 * .1 .0
40 * .2 .0
41 * .5 .0
42 * .0 .0
43 * .0 .0
44 * .0 .6
45 * .0 .4

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1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E AM

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* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21 REC22

```

LINK # * 150 260

```

-----*-----
46 * .0 .2
47 * .0 .1
48 * .0 .1
49 * .0 .1
50 * .0 .1

```

1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E PM
DATE: 08/31/2010 TIME: 13:56:27.45

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 NB Cent McF Appr	* 270186.0	289164.0	270108.0	289529.0	*	373.	348.	AG	1310.	12.6	.0	44.0		
2. 2 NB Thr W 4th Appr	* 270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	540.	12.6	.0	44.0		
3. 3 NB Cent NB Queue	* 270067.0	289730.0	270090.8	289637.0	*	96.	166.	AG	213.	100.0	.0	24.0	.42	4.9
4. 4 NB Cen W 4th Depr	* 270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	950.	12.6	.0	44.0		
5. 5 NB Cen W 4th Dept	* 270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	950.	12.6	.0	44.0		
6. 6 NB Lt W 4th Appr	* 270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	770.	12.6	.0	44.0		
7. 7 NB LefttNB Queue	* 270049.0	289728.0	270125.1	289412.8	*	324.	166.	AG	279.	100.0	.0	24.0	1.01	16.5
8. 10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168.	AG	280.	12.6	.0	44.0		
9. 11 SB CentSB Queue	* 270007.0	289828.0	269982.8	289943.5	*	118.	348.	AG	338.	100.0	.0	24.0	.94	6.0
10. 12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166.	AG	220.	12.6	.0	44.0		
11. 13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168.	AG	220.	12.6	.0	44.0		
12. 14 WB W 4tTo Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259.	AG	1660.	12.6	.0	44.0		
13. 15 WB W 4tFr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257.	AG	1660.	12.6	.0	44.0		
14. 16 WB W 4tTo Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258.	AG	1660.	12.6	.0	56.0		
15. 17 WB W 4tWB Queue	* 270089.0	289764.0	270315.8	289812.9	*	232.	78.	AG	329.	100.0	.0	36.0	.88	11.8
16. 16 WB W 4tFrom Cent	* 270040.0	289746.0	269741.0	289687.0	*	305.	259.	AG	2080.	12.6	.0	56.0		
17. 16 WB W 4tTo CD	* 269740.0	289694.0	269544.0	289656.0	*	200.	259.	AG	1790.	12.6	.0	44.0		
18. 18 WB W 4tRt Queue	* 269564.0	289660.0	270075.6	289756.6	*	521.	79.	AG	125.	100.0	.0	24.0	1.02	26.4
19. 19 WB W 4tRt to CD	* 269544.0	289656.0	269495.0	289688.0	*	59.	303.	AG	1790.	12.6	.0	44.0		
20. 20 WB W 4tLt to CD	* 269743.0	289676.0	269548.0	289635.0	*	199.	258.	AG	290.	12.6	.0	32.0		
21. 21 WB W 4tLt Queue	* 269568.0	289639.0	269723.4	289671.9	*	159.	78.	AG	146.	100.0	.0	12.0	.83	8.1
22. 22 WB W 4tLt to CD	* 269548.0	289635.0	269512.0	289576.0	*	69.	211.	AG	290.	12.6	.0	32.0		
23. 23 NB CD To W 4th	* 269358.0	289340.0	269495.0	289688.0	*	374.	21.	AG	740.	12.6	.0	44.0		
24. 24 NB CD NB Queue	* 269451.0	289575.0	269359.9	289343.8	*	248.	202.	AG	292.	100.0	.0	24.0	.96	12.6
25. 25 NB CD Fr W 4th	* 269495.0	289688.0	269471.0	289839.0	*	153.	351.	AG	2540.	12.6	.0	56.0		
26. 26 NB CD Fr W 4th	* 269471.0	289839.0	269432.0	290034.0	*	199.	349.	AG	2540.	12.6	.0	68.0		
27. 27 SB CD To W 4th	* 269353.0	290020.0	269416.0	289697.0	*	329.	169.	AG	1720.	12.6	.0	56.0		
28. 27 SB CD SB Queue	* 269408.0	289737.0	269385.2	289853.9	*	119.	349.	AG	187.	100.0	.0	36.0	.54	6.0
29. 28 SB CD @ W 4th	* 269416.0	289697.0	269512.0	289576.0	*	154.	142.	AG	1720.	12.6	.0	56.0		
30. 29 SB CD @ W 4th	* 269512.0	289576.0	269537.0	289433.0	*	145.	170.	AG	2010.	12.6	.0	56.0		
31. 30 WB Off 3rd-SB 75	* 270480.0	289330.0	270388.0	289332.0	*	92.	271.	BR	1450.	12.6	.0	32.0		
32. 31 WB Off 3rd-SB 75	* 270388.0	289332.0	270294.0	289352.0	*	96.	282.	BR	1450.	12.6	.0	32.0		
33. 32 WB Off 3rd-SB 75	* 270294.0	289352.0	270197.0	289396.0	*	106.	294.	BR	1450.	12.6	.0	32.0		
34. 33 WB Off 3rd-SB 75	* 270197.0	289396.0	270134.0	289442.0	*	78.	306.	BR	1450.	12.6	.0	32.0		
35. 34 WB Off 3rd-SB 75	* 270134.0	289442.0	269989.0	289567.0	*	191.	311.	BR	1450.	12.6	.0	32.0		
36. 35 WB Off 3rd-SB 75	* 269989.0	289567.0	269874.0	289640.0	*	136.	302.	BR	1450.	12.6	.0	32.0		
37. 36 WB Off 3rd-SB 75	* 269874.0	289640.0	269770.0	289675.0	*	110.	289.	AG	1450.	12.6	.0	32.0		
38. 37 WB Off 71-SB 75	* 270428.0	289285.0	270297.0	289305.0	*	133.	279.	BR	3490.	12.6	.0	44.0		
39. 38 WB Off 71-SB 75	* 270297.0	289305.0	270202.0	289342.0	*	102.	291.	BR	3490.	12.6	.0	44.0		
40. 39 WB Off 71-SB 75	* 270202.0	289342.0	270133.0	289389.0	*	83.	304.	BR	3490.	12.6	.0	44.0		
41. 40 WB Off 71-SB 75	* 270133.0	289389.0	270002.0	289505.0	*	175.	312.	BR	3490.	12.6	.0	44.0		
42. 41 WB Off 71-SB 75	* 270002.0	289505.0	269880.0	289607.0	*	159.	310.	BR	3490.	12.6	.0	44.0		
43. 42 WB Off 71-SB 75	* 269880.0	289607.0	269770.0	289675.0	*	129.	302.	BR	3490.	12.6	.0	44.0		
44. 43 WB Off 71-SB 75	* 269770.0	289675.0	269688.0	289703.0	*	87.	289.	BR	4940.	12.6	.0	56.0		

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E PM
 DATE: 08/31/2010 TIME: 13:56:27.45

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
45. 44 WB Off 71-SB 75	* 269688.0	289703.0	269608.0	289715.0	*	81.	279.	BR	4940.	12.6	.0	56.0		
46. 45 WB Off 71-SB 75	* 269608.0	289715.0	269523.0	289714.0	*	85.	269.	BR	4940.	12.6	.0	56.0		
47. 46 WB Off 71-SB 75	* 269523.0	289714.0	269442.0	289700.0	*	82.	260.	BR	4940.	12.6	.0	56.0		
48. 47 WB Off 71-SB 75	* 269442.0	289700.0	269379.0	289680.0	*	66.	252.	BR	4910.	12.6	.0	56.0		
49. 48 WB Off 71-SB 75	* 269379.0	289680.0	269317.0	289651.0	*	68.	245.	BR	4940.	12.6	.0	56.0		
50. 49 WB Off 71-SB 75	* 269317.0	289651.0	269246.0	289603.0	*	86.	236.	BR	4940.	12.6	.0	56.0		

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E PM
 DATE: 08/31/2010 TIME: 13:56:27.45

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	EM	FAC	TYPE	RATE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
3. 3 NB Cent NB Queue	* 120	65	2.0	540	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 120	85	2.0	770	1474	73.30	1	3
9. 11 SB CentSB Queue	* 120	103	2.0	280	1376	73.30	1	3
15. 17 WB W 4tWB Queue	* 120	67	2.0	1660	1534	73.30	1	3
18. 18 WB W 4tRt Queue	* 120	38	2.0	1790	1349	73.30	1	3
21. 21 WB W 4tLt Queue	* 120	89	2.0	290	1550	73.30	1	3
24. 24 NB CD NB Queue	* 120	89	2.0	740	1707	73.30	1	3
28. 27 SB CD SB Queue	* 120	38	2.0	1720	1628	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 SE Mid	* 270140.0	289517.0		5.0	*
2. R2 SE 164	* 270124.0	289585.0		5.0	*
3. R3 SE 82	* 270105.0	289664.0		5.0	*

4. R4 SE Corner	*	270088.0	289735.0	5.0	*
5. R5 SE 82	*	270158.0	289749.0	5.0	*
6. R6 SE 164	*	270239.0	289766.0	5.0	*
7. R7 SE Mid	*	270274.0	289773.0	5.0	*
8. R8 NE Mid	*	270256.0	289830.0	5.0	*
9. R9 NE 164	*	270223.0	289823.0	5.0	*
10. R10 NE 82	*	270142.0	289806.0	5.0	*
11. R11 NE Corner	*	270072.0	289791.0	5.0	*
12. R12 NE 82	*	270057.0	289862.0	5.0	*
13. R13 NE 164	*	270040.0	289942.0	5.0	*
14. R14 NE Mid	*	270034.0	289968.0	5.0	*
15. R15 NW 164	*	269944.0	290010.0	5.0	*
16. R16 NW 82	*	269961.0	289930.0	5.0	*
17. R17 NW Corner	*	269976.0	289859.0	5.0	*
18. R18 SW Corner	*	270010.0	289716.0	5.0	*
19. R19 SW 82	*	270028.0	289646.0	5.0	*
20. R20 SW 164	*	270046.0	289566.0	5.0	*
21. R21 SW Mid	*	270055.0	289525.0	5.0	*
22. R22 Near CD	*	269775.0	289723.0	5.0	*

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	*	.6	.7	.9	1.2	1.5	1.5	1.5	.0	.0	.0	.2	.2	.2	.4	.4	1.1	1.9	1.5	1.5	
5.	*	.5	.5	.7	1.2	1.5	1.5	1.5	.0	.0	.0	.1	.1	.1	.2	.5	.5	1.3	2.0	1.4	1.7
10.	*	.4	.6	.8	1.2	1.5	1.5	1.5	.0	.0	.0	.1	.1	.1	.1	.5	.5	1.4	1.8	1.7	1.8
15.	*	.4	.6	.7	1.4	1.6	1.6	1.5	.0	.0	.0	.1	.1	.1	.1	.5	.5	1.5	1.8	1.6	1.7
20.	*	.4	.5	.7	1.5	1.7	1.7	1.6	.0	.0	.0	.0	.0	.0	.0	.5	.5	1.5	1.9	1.9	1.7
25.	*	.3	.5	.7	1.6	1.7	1.7	1.6	.0	.0	.1	.1	.0	.0	.0	.4	.5	1.5	1.8	1.9	1.7
30.	*	.2	.5	.8	1.6	1.8	1.7	1.6	.1	.1	.1	.1	.0	.0	.0	.4	.5	1.5	1.9	2.0	1.8
35.	*	.3	.4	.8	1.8	1.9	1.8	1.7	.1	.1	.1	.1	.0	.0	.0	.4	.5	1.4	2.0	2.0	1.7
40.	*	.3	.5	.7	1.9	1.9	1.8	1.7	.1	.1	.1	.1	.0	.0	.0	.4	.6	1.4	1.8	2.1	1.6
45.	*	.1	.3	.7	2.0	2.1	1.9	1.5	.1	.1	.1	.1	.0	.0	.0	.4	.7	1.4	2.1	2.1	1.6
50.	*	.1	.3	.8	2.1	2.1	1.8	1.5	.1	.1	.1	.1	.0	.0	.0	.4	.7	1.4	2.4	2.1	1.4
55.	*	.0	.3	.6	2.1	2.2	1.8	1.5	.1	.1	.1	.1	.0	.0	.0	.4	.8	1.4	2.5	2.0	1.3
60.	*	.0	.2	.5	2.3	2.1	1.9	1.4	.1	.1	.3	.3	.0	.0	.0	.4	.9	1.3	2.7	1.9	1.3
65.	*	.0	.0	.4	2.3	2.1	1.6	1.3	.3	.4	.4	.5	.0	.0	.0	.4	1.0	1.3	2.9	1.8	1.0
70.	*	.0	.0	.4	2.1	1.8	1.5	1.1	.4	.6	.7	.8	.0	.0	.0	.3	1.1	1.3	2.6	1.6	1.0
75.	*	.0	.0	.1	1.8	1.5	1.2	1.0	.7	.9	1.1	1.2	.0	.0	.0	.3	1.1	1.3	2.7	1.5	1.0
80.	*	.0	.0	.0	1.5	1.2	1.0	.8	1.0	1.1	1.5	1.7	.0	.0	.0	.3	1.1	1.2	2.6	1.3	1.0
85.	*	.0	.0	.0	1.0	.8	.6	.6	1.2	1.4	1.8	2.0	.4	.0	.0	.3	1.2	1.5	2.0	1.3	1.0
90.	*	.0	.0	.0	.5	.6	.4	.3	1.4	1.6	2.0	2.2	.4	.0	.0	.4	1.2	1.5	2.0	1.2	1.0
95.	*	.0	.0	.0	.3	.3	.2	.2	1.5	1.9	2.1	2.3	.6	.1	.0	.4	1.5	1.7	1.7	1.2	1.0
100.	*	.0	.0	.0	.3	.1	.1	.1	1.6	1.9	2.1	2.1	.6	.2	.1	.4	1.7	1.8	1.6	1.2	1.0
105.	*	.0	.0	.0	.1	.1	.1	.1	1.6	1.9	2.1	2.0	.7	.3	.2	.4	1.7	1.8	1.6	1.2	1.1
110.	*	.0	.0	.0	.1	.1	.1	.1	1.6	1.9	2.1	2.0	.7	.3	.3	.7	1.8	1.9	1.5	1.2	1.1
115.	*	.1	.0	.0	.1	.1	.1	.1	1.8	1.8	1.9	1.8	.7	.4	.3	.6	1.8	1.9	1.5	1.2	1.2
120.	*	.2	.0	.0	.1	.1	.1	.1	1.7	1.8	1.9	1.7	.8	.4	.4	.6	2.0	1.9	1.5	1.1	1.3
125.	*	.4	.1	.0	.1	.1	.1	.1	1.7	1.7	1.8	1.6	.8	.4	.4	.8	2.0	1.8	1.7	1.3	1.7
130.	*	.5	.1	.1	.1	.1	.1	.1	1.7	1.7	1.7	1.5	.7	.5	.4	.8	1.9	1.7	1.7	1.5	1.7
135.	*	.5	.4	.1	.1	.0	.0	.0	1.7	1.7	1.7	1.4	.7	.5	.4	1.1	1.9	1.9	1.6	1.5	1.9
140.	*	.8	.5	.3	.2	.0	.0	.0	1.5	1.6	1.6	1.4	.7	.5	.5	1.1	2.0	2.0	1.8	1.9	2.5
145.	*	.8	.5	.3	.3	.1	.0	.0	1.5	1.5	1.6	1.3	.8	.6	.5	1.1	2.2	1.8	2.0	2.0	2.6
150.	*	.9	.8	.6	.4	.1	.0	.0	1.5	1.5	1.6	1.6	.8	.6	.6	1.1	2.5	1.9	1.9	1.9	2.3
155.	*	1.0	.9	.7	.8	.2	.1	.1	1.5	1.6	1.6	1.7	1.4	.7	.8	1.7	2.3	1.9	1.7	1.9	2.4
160.	*	1.1	1.2	1.1	1.2	.2	.1	.1	1.6	1.6	1.7	2.4	1.7	1.2	.9	1.7	1.9	1.8	1.8	1.6	2.2
165.	*	1.4	1.4	1.2	1.6	.4	.2	.1	1.7	1.7	2.0	2.7	1.8	1.4	1.3	1.6	1.7	1.8	1.4	1.5	1.9
170.	*	1.5	1.5	1.7	1.9	.4	.2	.2	1.8	1.8	2.1	2.9	1.8	1.7	1.6	1.3	1.4	1.3	1.2	1.3	1.8
175.	*	1.8	1.7	1.8	2.1	.5	.2	.2	1.8	1.9	2.1	3.0	2.3	1.9	1.9	.9	1.1	1.3	.9	1.1	1.5
180.	*	2.0	2.2	1.9	2.4	.6	.4	.2	1.8	1.8	2.2	2.9	2.2	1.9	1.8	1.0	1.0	1.0	.8	.9	1.3
185.	*	2.1	2.2	2.2	2.6	.8	.4	.3	1.8	2.0	2.5	3.0	2.1	2.0	1.6	.7	.9	.8	.8	.8	1.2
190.	*	2.1	2.1	2.2	2.7	1.0	.5	.4	2.0	1.9	2.5	2.9	1.8	1.8	1.7	.5	.7	.8	.7	.8	1.2
195.	*	2.3	1.9	2.3	2.5	.9	.4	.5	2.0	2.1	2.6	3.0	1.6	1.7	1.7	.6	.7	.8	.8	.8	1.3
200.	*	2.5	2.2	2.4	2.7	1.0	.6	.4	2.2	2.3	2.8	2.8	1.7	1.6	1.7	.5	.8	.8	.7	.8	1.1
205.	*	2.2	2.1	2.4	2.6	1.1	.7	.7	2.3	2.5	2.7	2.6	1.4	1.8	1.7	.5	.8	1.0	.7	.8	1.2

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E PM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

210.	*	2.2	1.9	2.4	2.7	1.1	.7	.7	2.5	2.6	2.8	2.6	1.5	1.7	1.8	.6	.7	.9	.7	.8	1.2
215.	*	2.2	1.8	2.4	2.5	1.2	1.0	.7	2.6	2.7	3.0	2.4	1.5	1.8	1.7	.6	.7	.9	.8	.8	1.2
220.	*	2.1	1.8	2.3	2.4	1.3	.8	.8	2.7	2.7	2.8	2.4	1.7	1.7	1.5	.7	.8	.8	.8	.7	1.2
225.	*	2.1	1.7	2.4	2.4	1.2	.9	.8	2.7	2.7	2.9	2.1	1.8	1.8	1.6	.7	.8	1.0	.9	.7	1.1
230.	*	2.1	1.7	2.4	2.5	1.1	1.0	.9	2.9	3.0	2.8	2.4	1.7	1.9	1.8	.7	.8	1.2	.7	.7	1.1
235.	*	2.1	1.8	2.3	2.1	1.3	.9	.9	3.0	2.9	2.8	2.6	1.9	1.9	1.7	.6	.7	1.1	1.0	.7	1.2
240.	*	2.1	1.8	2.3	2.3	1.3	1.3	1.3	2.9	2.8	2.8	2.6	1.9	1.7	1.4	.7	.7	1.0	1.2	.8	1.1
245.	*	2.2	1.7	2.2	2.7	1.4	1.4	1.4	2.8	2.8	2.6	2.7	1.9	1.6	1.4	.5	.8	.9	1.7	.8	1.1
250.	*	2.1	1.9	2.4	3.0	2.1	1.8	1.8	2.4	2.5	2.4	2.7	1.7	1.4	1.2	.3	.7	1.1	1.9	1.0	1.2

255.	*	2.2	2.1	2.6	3.1	2.3	2.0	1.9	2.1	2.3	2.0	2.4	1.8	1.4	.9	.2	.5	1.0	2.2	1.1	1.3
260.	*	2.1	2.0	2.9	3.5	2.5	2.5	2.4	1.8	1.9	1.8	2.1	1.6	1.2	.8	.2	.3	.6	2.7	1.3	1.6
265.	*	2.1	2.0	3.0	3.2	2.7	2.8	2.5	1.5	1.4	1.6	1.8	1.7	1.1	.8	.2	.5	3.0	1.6	1.6	
270.	*	2.3	2.2	3.1	3.3	3.1	2.6	2.5	.9	.9	1.2	1.5	1.4	1.0	.7	.2	.2	.3	3.0	1.9	1.6
275.	*	2.2	2.8	3.1	3.0	2.7	2.5	2.3	.6	.8	.7	1.2	1.3	.8	.6	.1	.2	.2	2.7	1.7	2.0
280.	*	2.7	2.7	3.4	2.8	2.3	2.5	2.5	.4	.5	.7	1.1	1.3	.8	.6	.0	.1	.2	2.5	1.7	2.5
285.	*	2.8	2.7	3.2	2.2	2.2	2.4	2.4	.3	.5	.5	.9	1.2	.6	.5	.0	.1	.1	2.3	1.8	2.4
290.	*	3.1	2.7	2.9	1.9	2.3	2.2	2.3	.3	.4	.6	.8	1.1	.6	.5	.0	.0	.1	1.8	1.5	2.2
295.	*	2.7	2.3	2.7	1.8	2.3	2.1	2.1	.3	.3	.6	.9	1.1	.5	.5	.0	.0	.0	1.7	1.1	2.1
300.	*	2.5	2.0	2.7	2.0	2.2	2.1	2.1	.3	.3	.6	.9	1.1	.5	.5	.0	.0	.0	1.6	.8	1.6
305.	*	2.3	2.0	2.5	1.8	2.1	2.1	2.0	.2	.3	.5	1.1	1.1	.6	.6	.0	.0	.0	1.4	.7	1.2
310.	*	2.1	1.9	2.4	1.9	2.1	1.9	1.9	.1	.2	.5	1.1	1.1	.6	.6	.0	.0	.0	1.3	.6	.8
315.	*	1.7	1.9	2.3	1.9	2.1	1.9	1.8	.1	.1	.3	1.1	1.0	.6	.6	.0	.0	.0	1.2	.6	.5
320.	*	1.8	1.9	2.3	1.7	2.0	1.8	1.8	.1	.1	.3	1.2	1.0	.7	.7	.0	.0	.0	1.2	.5	.4
325.	*	1.9	2.0	2.3	1.7	1.8	1.6	1.6	.1	.1	.3	1.1	.9	.7	.7	.0	.0	.0	1.2	.5	.4
330.	*	1.9	2.0	2.2	1.8	1.8	1.6	1.6	.1	.1	.2	1.2	.9	.7	.7	.0	.0	.0	1.2	.5	.3
335.	*	1.8	1.7	2.1	1.8	1.7	1.6	1.5	.0	.1	.2	1.1	.8	.7	.7	.1	.1	.2	1.4	.7	.6
340.	*	1.7	1.7	2.0	1.8	1.7	1.6	1.6	.0	.0	.1	1.0	.8	.7	.7	.1	.2	.3	1.6	.9	.7
345.	*	1.3	1.4	1.5	1.7	1.8	1.6	1.6	.0	.0	.1	.8	.7	.5	.6	.2	.2	.4	1.7	1.0	.8
350.	*	1.0	1.2	1.3	1.4	1.8	1.6	1.6	.0	.0	.1	.6	.5	.4	.5	.2	.3	.7	1.9	1.3	1.2
355.	*	1.0	.9	.9	1.4	1.6	1.6	1.6	.0	.0	.0	.4	.3	.3	.3	.4	.4	.9	1.9	1.3	1.4
360.	*	.6	.7	.9	1.2	1.5	1.5	1.5	.0	.0	.0	.2	.2	.2	.2	.4	.4	1.1	1.9	1.5	1.5

MAX * 3.1 2.8 3.4 3.5 3.1 2.8 2.5 3.0 3.0 3.0 3.0 2.3 2.0 1.9 1.7 2.5 2.0 3.0 2.1 2.6
DEGR * 290 275 280 260 270 265 280 235 230 215 185 175 185 175 155 150 140 265 40 145

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22

0.	*	1.7	.0
5.	*	1.9	.0
10.	*	1.7	.0
15.	*	1.8	.1
20.	*	1.7	.2
25.	*	1.7	.2
30.	*	1.6	.2
35.	*	1.5	.3
40.	*	1.4	.3
45.	*	1.3	.3
50.	*	1.3	.3
55.	*	1.2	.4
60.	*	1.1	.4
65.	*	1.1	.9
70.	*	1.2	.9
75.	*	1.2	1.2
80.	*	1.2	1.7
85.	*	1.2	2.0
90.	*	1.2	2.1
95.	*	1.3	2.2
100.	*	1.2	2.2
105.	*	1.3	2.1
110.	*	1.5	2.3
115.	*	1.9	2.5
120.	*	2.4	2.7
125.	*	2.7	3.1
130.	*	3.0	3.6
135.	*	3.1	3.6
140.	*	3.2	3.4
145.	*	3.3	3.3
150.	*	3.2	3.1
155.	*	3.1	2.9
160.	*	2.8	2.8
165.	*	2.4	2.8
170.	*	2.5	2.8
175.	*	2.1	2.7
180.	*	1.8	2.7
185.	*	1.7	2.8
190.	*	1.7	2.8
195.	*	1.7	2.7
200.	*	1.7	2.8
205.	*	1.6	2.7

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt E PM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22

210.	*	1.6	2.7
215.	*	1.6	2.9

220. * 1.5 3.3
 225. * 1.6 3.4
 230. * 1.6 3.7
 235. * 1.6 3.8
 240. * 1.6 4.2
 245. * 1.7 4.4
 250. * 1.7 4.7
 255. * 1.8 4.3
 260. * 1.8 4.0
 265. * 1.9 3.7
 270. * 2.1 3.3
 275. * 2.2 2.5
 280. * 2.7 1.9
 285. * 3.0 1.5
 290. * 3.3 .8
 295. * 3.5 .6
 300. * 3.3 .6
 305. * 2.6 .4
 310. * 2.4 .3
 315. * 1.7 .2
 320. * 1.3 .1
 325. * .9 .0
 330. * .8 .0
 335. * .7 .0
 340. * 1.0 .0
 345. * 1.1 .0
 350. * 1.4 .0
 355. * 1.5 .0
 360. * 1.7 .0

MAX * 3.5 4.7
 DEGR. * 295 250

THE HIGHEST CONCENTRATION IS 4.70 PPM AT 250 DEGREES FROM REC22.
 THE 2ND HIGHEST CONCENTRATION IS 3.50 PPM AT 260 DEGREES FROM REC4.
 THE 3RD HIGHEST CONCENTRATION IS 3.50 PPM AT 295 DEGREES FROM REC21.

1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt E PM
 DATE: 08/31/2010 TIME: 13:56:27.45

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20
 LINK # * 290 275 280 260 270 265 280 235 230 215 185 175 185 175 155 150 140 265 40 145

1	*	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.4
2	*	.1	.2	.2	.1	.0	.0	.1	.1	.1	.2	.1	.0	.1	.1	.0	.1	.0	.1
3	*	.0	.0	.7	.3	.1	.1	.0	.1	.1	.2	.3	.2	.1	.1	.1	.1	.0	.3
4	*	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1	.1	.0
5	*	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.5	.5	.2	.1	.1	.0	.0
6	*	.2	.3	.3	.2	.1	.0	.0	.1	.1	.1	.3	.2	.1	.1	.1	.1	.0	.3
7	*	.6	.6	.6	.3	.1	.1	.0	.1	.2	.3	.6	.4	.2	.2	.1	.2	.2	.6
8	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.2	.2	.1	.0	.0
9	*	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.1	.5	1.0	.6	.0	.0
10	*	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1
11	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
12	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	*	.0	.0	.0	.3	.7	.8	.9	.9	.9	.8	.6	.3	.1	.1	.1	.2	.0	.3
15	*	.0	.0	.0	.0	.5	.7	1.1	1.2	1.1	1.0	.0	.1	.0	.1	.1	.1	.1	.0
16	*	.1	.1	.4	.8	.4	.3	.1	.1	.1	.1	.2	.1	.1	.1	.1	1.3	.0	.0
17	*	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
18	*	.1	.1	.2	.4	.3	.2	.1	.1	.0	.2	.1	.1	.1	.0	.1	.1	.4	.0
19	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25	*	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
26	*	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27	*	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
34	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
35	*	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.0	.0	.0	.4
36	*	.1	.2	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
37	*	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0
38	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1
39	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
40	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.2
41	*	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.1	.1	.1	.0	.0	.0	.0	.3
42	*	.4	.3	.0	.0	.0	.0	.1	.2	.2	.1	.0	.1	.1	.0	.0	.0	.0	.0
43	*	.2	.2	.1	.2	.1	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.2	.0	.0
44	*	.1	.1	.1	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0
45	*	.1	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.0	.0

1

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

LINK #	* 290	275	280	260	270	265	280	235	230	215	185	175	185	175	155	150	140	265	40	145
46	*	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0		
47	*	.1	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0		
48	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0			
49	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0			
50	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0				

1

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22

LINK # * 295 250

1	*	.0	.0
2	*	.0	.0
3	*	.0	.0
4	*	.0	.0
5	*	.0	.0
6	*	.0	.0
7	*	.0	.0
8	*	.0	.0
9	*	.0	.0
10	*	.0	.0
11	*	.0	.0
12	*	.0	.0
13	*	.0	.0
14	*	.0	.0
15	*	.0	.0
16	*	.1	.4
17	*	.1	.7
18	*	.1	.4
19	*	.0	.1
20	*	.0	.1
21	*	.0	.2
22	*	.0	.0
23	*	.0	.1
24	*	.0	.1
25	*	.1	.0
26	*	.0	.0
27	*	.1	.0
28	*	.0	.0
29	*	.0	.1
30	*	.0	.0
31	*	.0	.0
32	*	.0	.0
33	*	.0	.0
34	*	.0	.0
35	*	1.0	.0
36	*	.3	.0
37	*	.1	.0
38	*	.0	.0
39	*	.0	.0
40	*	.0	.0
41	*	.0	.0
42	*	.8	.0
43	*	.3	.0
44	*	.2	1.4
45	*	.1	.5

1

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22

LINK # * 295 250

46	*	.1	.2
47	*	.1	.1
48	*	.0	.1
49	*	.0	.1
50	*	.0	.1

1

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	* X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 NB Cent McF Appr	* 270186.0	289164.0	270108.0	289529.0	*	373.	348.	AG	190.	12.6	.0	44.0			
2. 2 NB Thr W 4th Appr	* 270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	150.	12.6	.0	44.0			
3. 3 NB Cent NB Queue	* 270067.0	289730.0	270070.6	289716.1	*	14.	166.	AG	229.	100.0	.0	24.0	.14	.7	
4. 4 NB Cen W 4th Dep	* 270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	330.	12.6	.0	44.0			
5. 5 NB Cen W 4th Dep	* 270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	330.	12.6	.0	44.0			
6. 6 NB Lt W 4th Appr	* 270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	40.	12.6	.0	44.0			
7. 7 NB LefttNB Queue	* 270049.0	289728.0	270050.4	289722.1	*	6.	166.	AG	354.	100.0	.0	24.0	.41	.3	
8. 8 NB Ramp From W 4th	* 270042.0	289755.0	269974.0	289811.0	*	88.	309.	AG	270.	12.6	.0	44.0			
9. 9 NB Ramp From W 4th	* 269974.0	289811.0	269755.0	290270.0	*	509.	334.	AG	270.	12.6	.0	44.0			
10. 10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168.	AG	130.	12.6	.0	44.0			
11. 11 SB CentSB Queue	* 270007.0	289828.0	270004.2	289841.6	*	14.	348.	AG	256.	100.0	.0	24.0	.15	.7	
12. 12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166.	AG	150.	12.6	.0	44.0			
13. 13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168.	AG	150.	12.6	.0	44.0			
14. 14 WB W 4To Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259.	AG	430.	12.6	.0	44.0			
15. 15 WB W 4Fr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257.	AG	430.	12.6	.0	44.0			
16. 16 WB W 4To Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258.	AG	430.	12.6	.0	56.0			
17. 17 WB W 4WB Queue	* 270089.0	289764.0	270117.3	289770.1	*	29.	78.	AG	364.	100.0	.0	36.0	.30	1.5	
18. 18 WB Off 3rd-SB 75	* 270473.0	289330.0	270387.0	289337.0	*	86.	275.	BR	280.	12.1	.0	32.0			
19. 19 WB Off 3rd-SB 75	* 270387.0	289337.0	270291.0	289353.0	*	97.	279.	BR	280.	12.1	.0	32.0			
20. 20 WB Off 3rd-SB 75	* 270291.0	289353.0	270209.0	289396.0	*	93.	298.	BR	280.	12.1	.0	32.0			
21. 21 WB Off 3rd-SB 75	* 270209.0	289396.0	269996.0	289555.0	*	266.	307.	BR	280.	12.1	.0	28.0			
22. 22 WB Off 3rd-SB 75	* 269996.0	289555.0	269861.0	289614.0	*	147.	294.	BR	280.	12.1	.0	32.0			
23. 23 WB Off 71- SB 75	* 270427.0	289288.0	270271.0	289320.0	*	159.	282.	BR	190.	12.1	.0	44.0			
24. 24 WB Off 71- SB 75	* 270271.0	289320.0	270153.0	289385.0	*	135.	299.	BR	190.	12.1	.0	44.0			
25. 25 WB Off 71- SB 75	* 270153.0	289385.0	269986.0	289528.0	*	220.	311.	BR	190.	12.1	.0	44.0			
26. 26 WB Off 71- SB 75	* 269986.0	289528.0	269861.0	289614.0	*	152.	305.	BR	190.	12.1	.0	44.0			
27. 27 WB Off 71- SB 75	* 269861.0	289614.0	269702.0	289652.0	*	163.	283.	BR	470.	12.1	.0	44.0			
28. 28 WB Off 71- SB 75	* 269702.0	289652.0	269576.0	289645.0	*	126.	267.	BR	470.	12.1	.0	44.0			
29. 29 WB Off 71- SB 75	* 269576.0	289645.0	269470.0	289614.0	*	110.	254.	BR	470.	12.1	.0	44.0			

JOB: Brent Spence Bridge RUN: W 4th & Central Alt I AM
 DATE: 08/31/2010 TIME: 12:18:42.95

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE (SEC)	RED (SEC)	CLEARANCE (VPH)	APPROACH (VPH)	SATURATION (gm/hr)	IDLE (VPH)	SIGNAL (VPH)	ARRIVAL (VPH)
3. 3 NB Cent NB Queue	* 60	35	2.0	150	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 60	54	2.0	40	1474	73.30	1	3
11. 11 SB CentSB Queue	* 60	39	2.0	130	1504	73.30	1	3
17. 17 WB W 4WB Queue	* 60	37	2.0	430	1503	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	* (FT)
1. R1 SE Mid	* 270140.0	289517.0	5.0	*
2. R2 SE 164	* 270124.0	289585.0	5.0	*
3. R3 SE 82	* 270105.0	289664.0	5.0	*
4. R4 SE Corner	* 270088.0	289735.0	5.0	*
5. R5 SE 82	* 270158.0	289749.0	5.0	*
6. R6 SE 164	* 270239.0	289766.0	5.0	*
7. R7 SE Mid	* 270274.0	289773.0	5.0	*
8. R8 NE Mid	* 270256.0	289830.0	5.0	*
9. R9 NE 164	* 270223.0	289823.0	5.0	*
10. R10 NE 82	* 270142.0	289806.0	5.0	*
11. R11 NE Corner	* 270072.0	289791.0	5.0	*
12. R12 NE 82	* 270057.0	289862.0	5.0	*
13. R13 NE 164	* 270040.0	289942.0	5.0	*
14. R14 NE Mid	* 270034.0	289968.0	5.0	*
15. R15 NW 164	* 269944.0	290010.0	5.0	*
16. R16 NW 82	* 269961.0	289930.0	5.0	*
17. R17 NW Corner	* 269976.0	289859.0	5.0	*
18. R18 SW Corner	* 270010.0	289716.0	5.0	*
19. R19 SW 82	* 270028.0	289646.0	5.0	*
20. R20 SW 164	* 270046.0	289566.0	5.0	*
21. R21 SW Mid	* 270055.0	289525.0	5.0	*

JOB: Brent Spence Bridge RUN: W 4th & Central Alt I AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0-.360.

WIND * CONCENTRATION	ANGLE * (PPM)	(DEGR)* REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18
0. *	.0	.2	.3	.7	.2	.2	.0	.0	.0	.1	.1	.1	.1	.2	.2	.2	.3	.2	.1
5. *	.0	.2	.3	.8	.2	.2	.0	.0	.0	.0	.0	.1	.2	.2	.2	.3	.2	.2	
10. *	.0	.1	.3	.8	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.3	.1	.2	
15. *	.0	.1	.2	.9	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.4	.2	

20.	*	.0	.1	.2	.9	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.3	.4	.3
25.	*	.0	.1	.2	.9	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.4	.3
30.	*	.0	.1	.1	.9	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.4	.4	.2
35.	*	.0	.0	.1	.9	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.3	.4	.2
40.	*	.0	.0	.1	.8	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.4	.4	.1
45.	*	.0	.0	.1	.8	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.3	.3	.1
50.	*	.0	.0	.1	.7	.2	.2	.2	.0	.0	.0	.0	.0	.0	.2	.2	.2	.3	.3	.1
55.	*	.0	.0	.1	.6	.2	.2	.3	.0	.0	.0	.0	.0	.0	.2	.2	.2	.5	.2	.1
60.	*	.0	.0	.0	.6	.2	.3	.3	.0	.0	.1	.0	.0	.0	.2	.2	.2	.6	.2	.1
65.	*	.0	.0	.0	.6	.2	.3	.3	.0	.1	.1	.0	.0	.0	.2	.2	.2	.7	.1	.1
70.	*	.0	.0	.0	.4	.2	.3	.2	.1	.1	.1	.1	.0	.0	.2	.2	.2	.7	.1	.1
75.	*	.0	.0	.0	.3	.2	.3	.2	.2	.1	.1	.2	.0	.0	.2	.2	.2	.5	.1	.1
80.	*	.0	.0	.0	.3	.2	.1	.2	.2	.2	.3	.0	.0	.0	.2	.2	.2	.5	.1	.1
85.	*	.0	.0	.0	.1	.1	.1	.1	.2	.3	.2	.3	.0	.0	.2	.2	.2	.5	.1	.1
90.	*	.0	.0	.0	.1	.1	.1	.1	.3	.3	.2	.4	.0	.0	.2	.2	.2	.4	.1	.1
95.	*	.0	.0	.0	.1	.1	.0	.0	.3	.3	.2	.6	.0	.0	.2	.2	.2	.3	.1	.1
100.	*	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.6	.1	.0	.2	.2	.4	.3	.1	.1
105.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.6	.1	.0	.2	.2	.4	.2	.1	.1
110.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.7	.1	.0	.2	.2	.6	.1	.1	.1
115.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.1	.0	.2	.2	.6	.1	.1	.1
120.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.1	.0	.2	.3	.6	.1	.1	.1
125.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.1	.1	.0	.2	.3	.6	.1	.1
130.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.2	.1	.0	.2	.4	.5	.1	.1
135.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.2	.1	.0	.2	.4	.5	.1	.1
140.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.8	.2	.1	.0	.2	.3	.4	.1	.1
145.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.7	.3	.1	.0	.2	.3	.4	.1	.1
150.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.6	.3	.2	.0	.2	.2	.3	.1	.1
155.	*	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.6	.3	.2	.2	.2	.2	.4	.1	.1
160.	*	.1	.0	.1	.1	.0	.0	.0	.2	.2	.2	.6	.3	.2	.2	.1	.2	.4	.1	.1
165.	*	.2	.0	.1	.1	.0	.0	.0	.2	.2	.2	.7	.2	.2	.2	.1	.3	.1	.1	.2
170.	*	.2	.1	.1	.1	.0	.0	.0	.2	.2	.2	.6	.3	.2	.2	.1	.1	.2	.1	.1
175.	*	.2	.2	.1	.1	.0	.0	.0	.2	.2	.2	.6	.4	.1	.2	.1	.1	.2	.0	.1
180.	*	.2	.2	.1	.1	.0	.0	.0	.2	.2	.2	.5	.3	.2	.2	.1	.1	.1	.0	.1
185.	*	.2	.2	.1	.2	.0	.0	.0	.2	.2	.2	.5	.2	.2	.2	.1	.1	.1	.0	.1
190.	*	.2	.2	.1	.2	.0	.0	.0	.2	.2	.3	.6	.2	.2	.2	.1	.1	.1	.0	.1
195.	*	.2	.1	.1	.2	.0	.0	.0	.2	.2	.4	.5	.1	.2	.2	.1	.1	.1	.0	.1
200.	*	.2	.1	.1	.3	.0	.0	.0	.2	.2	.4	.5	.1	.3	.2	.1	.1	.1	.0	.1
205.	*	.2	.1	.1	.3	.0	.0	.2	.2	.5	.3	.1	.2	.2	.1	.1	.1	.0	.0	.1

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I AM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

210.	*	.2	.1	.1	.3	.0	.0	.2	.2	.6	.3	.1	.2	.2	.1	.1	.1	.0	.0	.1
215.	*	.2	.1	.1	.4	.0	.0	.2	.2	.6	.2	.1	.2	.2	.1	.1	.1	.0	.0	.1
220.	*	.2	.1	.1	.4	.0	.0	.2	.2	.6	.2	.2	.1	.2	.1	.1	.1	.0	.0	.1
225.	*	.2	.1	.1	.5	.0	.0	.2	.3	.6	.2	.2	.1	.1	.1	.1	.1	.0	.0	.1
230.	*	.2	.1	.1	.6	.0	.0	.2	.3	.6	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
235.	*	.2	.1	.1	.6	.0	.0	.3	.3	.6	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
240.	*	.2	.1	.1	.6	.0	.0	.3	.3	.5	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
245.	*	.2	.1	.1	.6	.2	.1	.1	.3	.5	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
250.	*	.2	.1	.1	.6	.3	.2	.1	.3	.4	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
255.	*	.2	.1	.1	.6	.3	.2	.2	.3	.3	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
260.	*	.2	.1	.1	.6	.4	.3	.3	.2	.2	.3	.2	.1	.1	.1	.1	.1	.0	.0	.1
265.	*	.2	.1	.1	.5	.4	.3	.3	.1	.2	.2	.2	.1	.1	.1	.1	.1	.0	.0	.1
270.	*	.2	.1	.1	.5	.5	.3	.3	.1	.1	.1	.2	.1	.1	.1	.1	.1	.0	.0	.1
275.	*	.2	.1	.1	.4	.5	.3	.3	.0	.0	.0	.2	.1	.1	.1	.1	.1	.0	.0	.1
280.	*	.1	.1	.1	.4	.6	.3	.3	.0	.0	.0	.2	.2	.1	.1	.1	.1	.0	.0	.1
285.	*	.0	.1	.1	.3	.6	.3	.2	.0	.0	.0	.1	.2	.1	.1	.1	.1	.0	.0	.1
290.	*	.0	.1	.1	.3	.6	.3	.2	.0	.0	.1	.2	.2	.1	.1	.1	.1	.0	.0	.1
295.	*	.0	.1	.1	.3	.6	.2	.2	.0	.0	.1	.3	.2	.1	.1	.1	.1	.0	.0	.0
300.	*	.0	.1	.1	.4	.5	.2	.2	.0	.0	.1	.4	.3	.2	.2	.1	.1	.2	.0	.0
305.	*	.0	.1	.1	.5	.5	.2	.2	.0	.0	.1	.4	.3	.2	.2	.1	.1	.2	.0	.0
310.	*	.1	.1	.2	.5	.5	.2	.2	.0	.0	.1	.4	.3	.2	.2	.1	.1	.2	.0	.0
315.	*	.1	.1	.2	.5	.5	.2	.2	.0	.0	.1	.4	.3	.2	.2	.1	.1	.2	.0	.0
320.	*	.1	.1	.2	.4	.4	.2	.2	.0	.0	.1	.4	.2	.2	.2	.1	.1	.2	.0	.0
325.	*	.1	.1	.2	.5	.4	.2	.2	.0	.0	.1	.2	.2	.2	.2	.1	.1	.2	.1	.0
330.	*	.1	.1	.3	.4	.3	.2	.2	.0	.0	.1	.3	.2	.2	.2	.0	.1	.2	.1	.0
335.	*	.1	.1	.5	.5	.3	.2	.2	.0	.0	.1	.3	.2	.2	.2	.0	.1	.2	.1	.0
340.	*	.1	.2	.5	.5	.2	.2	.2	.0	.0	.0	.3	.2	.2	.2	.0	.1	.2	.1	.1
345.	*	.1	.2	.5	.6	.2	.2	.2	.0	.0	.2	.2	.2	.2	.1	.1	.2	.3	.1	.1
350.	*	.2	.2	.5	.6	.2	.2	.2	.0	.0	.0	.2	.2	.2	.1	.2	.3	.4	.2	.1
355.	*	.0	.3	.3	.7	.2	.2	.2	.0	.0	.1	.1	.1	.1	.2	.2	.2	.3	.2	.1
360.	*	.0	.2	.3	.7	.2	.2	.2	.0	.0	.1	.1	.1	.1	.2	.2	.2	.3	.2	.1

MAX * .2 .3 .5 .9 .6 .3 .3 .3 .3 .6 .8 .4 .3 .2 .2 .4 .6 .7 .4 .4

DEGR. * 165 355 335 15 280 60 55 90 85 210 115 175 200 155 0 130 110 65 15 150

1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21

```

-----*-----
0. * .1
5. * .1
10. * .2
15. * .2
20. * .1
25. * .1
30. * .1
35. * .1
40. * .1
45. * .1
50. * .1
55. * .1
60. * .1
65. * .1
70. * .1
75. * .1
80. * .1
85. * .0
90. * .0
95. * .0
100. * .0
105. * .1
110. * .1
115. * .2
120. * .4
125. * .4
130. * .4
135. * .4
140. * .4
145. * .4
150. * .5
155. * .5
160. * .4
165. * .4
170. * .4
175. * .2
180. * .2
185. * .2
190. * .2
195. * .2
200. * .2
205. * .2
1

```

PAGE 6

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I AM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21

```

-----*-----
210. * .2
215. * .2
220. * .2
225. * .2
230. * .2
235. * .2
240. * .2
245. * .2
250. * .2
255. * .2
260. * .2
265. * .2
270. * .2
275. * .2
280. * .2
285. * .3
290. * .3
295. * .3
300. * .3
305. * .2
310. * .1
315. * .1
320. * .1
325. * .1
330. * .0
335. * .0
340. * .0
345. * .1
350. * .1
355. * .1
360. * .1

```

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-----*-----
MAX * .5
DEGR. * 150

```

THE HIGHEST CONCENTRATION IS .90 PPM AT 15 DEGREES FROM REC4.
 THE 2ND HIGHEST CONCENTRATION IS .80 PPM AT 115 DEGREES FROM REC11.
 THE 3RD HIGHEST CONCENTRATION IS .70 PPM AT 65 DEGREES FROM REC18.

1

PAGE 7

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I AM

DATE: 08/31/2010 TIME: 12:18:42.95

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20

LINK #	* 165	355	335	15	280	60	55	90	85	210	115	175	200	155	0	130	110	65	15	150	
1 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
2 *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.2	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0
8 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0
12 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
13 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
14 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.1	.1	.2	.2	.2	.2	.2	.2	.2	.1	.0	.0	.1	.1	.2	.1	.0	.0	.0	.0
17 *	.0	.1	.1	.7	.4	.0	.0	.0	.4	.6	.1	.0	.1	.0	.1	.1	.2	.1	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 12:18:42.95

RUN: W 4th & Central Alt I AM

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC21
LINK # * 150

1 *	.1
2 *	.0
3 *	.0
4 *	.0
5 *	.0
6 *	.0
7 *	.0
8 *	.0
9 *	.0
10 *	.0
11 *	.0
12 *	.0
13 *	.1
14 *	.0
15 *	.0
16 *	.0
17 *	.0
18 *	.0
19 *	.0
20 *	.0
21 *	.2
22 *	.0
23 *	.0
24 *	.0
25 *	.1
26 *	.0
27 *	.0
28 *	.0
29 *	.0

JOB: Brent Spence Bridge
DATE: 08/31/2010 TIME: 12:15:58.33

RUN: W 4th & Central Alt I PM

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	* LINK COORDINATES (FT)	X2	Y2	* (FT) (DEG)	* LENGTH BRG TYPE	VPH	EF	H	W	V/C	QUEUE
							(G/MI) (FT) (FT)	(VEH)					

1. 1 NB Cent McF Appr * 270186.0 289164.0 270108.0 289529.0 * 373. 348. AG 810. 12.6 .0 44.0

2.	2 NB Thr W 4th Appr*	270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	480.	12.6	.0	44.0		
3.	3 NB Cent NB Queue	* 270067.0	289730.0	270081.6	289672.8	*	59.	166.	AG	253.	100.0	.0	24.0	.53	3.0
4.	4 NB Cen W 4th Depr*	270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	620.	12.6	.0	44.0		
5.	5 NB Cen W 4th Depr*	270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	620.	12.6	.0	44.0		
6.	6 NB Lt W 4th Appr*	270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	330.	12.6	.0	44.0		
7.	7 NB LefttNB Queue	* 270049.0	289728.0	270074.4	289622.6	*	108.	166.	AG	326.	100.0	.0	24.0	.98	5.5
8.	8 NB Ramp From W 4th*	270042.0	289755.0	269974.0	289811.0	*	88.	309.	AG	1430.	12.6	.0	44.0		
9.	9 NB Ramp From W 4th*	269974.0	289811.0	269755.0	290270.0	*	509.	334.	AG	1430.	12.6	.0	44.0		
10.	10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168.	AG	180.	12.6	.0	44.0		
11.	11 SB CentSB Queue	* 270007.0	289828.0	270001.3	289855.0	*	28.	348.	AG	315.	100.0	.0	24.0	.45	1.4
12.	12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166.	AG	180.	12.6	.0	44.0		
13.	13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168.	AG	180.	12.6	.0	44.0		
14.	14 WB W 4tTo Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259.	AG	1320.	12.6	.0	44.0		
15.	15 WB W 4tFr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257.	AG	1320.	12.6	.0	44.0		
16.	16 WB W 4tTo Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258.	AG	1320.	12.6	.0	56.0		
17.	17 WB W 4tWB Queue	* 270089.0	289764.0	270176.0	289782.8	*	89.	78.	AG	312.	100.0	.0	36.0	.69	4.5
18.	18 WB Off 3rd-SB 75	* 270473.0	289330.0	270387.0	289337.0	*	86.	275.	BR	1450.	12.1	.0	32.0		
19.	19 WB Off 3rd-SB 75	* 270387.0	289337.0	270291.0	289353.0	*	97.	279.	BR	1450.	12.1	.0	32.0		
20.	20 WB Off 3rd-SB 75	* 270291.0	289353.0	270209.0	289396.0	*	93.	298.	BR	1450.	12.1	.0	32.0		
21.	21 WB Off 3rd-SB 75	* 270209.0	289396.0	269996.0	289555.0	*	266.	307.	BR	1450.	12.1	.0	28.0		
22.	22 WB Off 3rd-SB 75	* 269996.0	289555.0	269861.0	289614.0	*	147.	294.	BR	1450.	12.1	.0	32.0		
23.	23 WB Off 71- SB 75	* 270427.0	289288.0	270271.0	289320.0	*	159.	282.	BR	320.	12.1	.0	44.0		
24.	24 WB Off 71- SB 75	* 270271.0	289320.0	270153.0	289385.0	*	135.	299.	BR	320.	12.1	.0	44.0		
25.	25 WB Off 71- SB 75	* 270153.0	289385.0	269986.0	289528.0	*	220.	311.	BR	320.	12.1	.0	44.0		
26.	26 WB Off 71- SB 75	* 269986.0	289528.0	269861.0	289614.0	*	152.	305.	BR	320.	12.1	.0	44.0		
27.	27 WB Off 71- SB 75	* 269861.0	289614.0	269702.0	289652.0	*	163.	283.	BR	1770.	12.1	.0	44.0		
28.	28 WB Off 71- SB 75	* 269702.0	289652.0	269576.0	289645.0	*	126.	267.	BR	1770.	12.1	.0	44.0		
29.	29 WB Off 71- SB 75	* 269576.0	289645.0	269470.0	289614.0	*	110.	254.	BR	1770.	12.1	.0	44.0		

1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt I PM
 DATE: 08/31/2010 TIME: 12:15:58.33

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
3. 3 NB Cent NB Queue	* 70	45	2.0	480	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 70	58	2.0	330	1474	73.30	1	3
11. 11 SB CentSB Queue	* 70	56	2.0	180	1420	73.30	1	3
17. 17 WB W 4tWB Queue	* 70	37	2.0	1320	1535	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 SE Mid	* 270140.0	289517.0	5.0	*	
2. R2 SE 164	* 270124.0	289585.0	5.0	*	
3. R3 SE 82	* 270105.0	289664.0	5.0	*	
4. R4 SE Corner	* 270088.0	289735.0	5.0	*	
5. R5 SE 82	* 270158.0	289749.0	5.0	*	
6. R6 SE 164	* 270239.0	289766.0	5.0	*	
7. R7 SE Mid	* 270274.0	289773.0	5.0	*	
8. R8 NE Mid	* 270256.0	289830.0	5.0	*	
9. R9 NE 164	* 270223.0	289823.0	5.0	*	
10. R10 NE 82	* 270142.0	289806.0	5.0	*	
11. R11 NE Corner	* 270072.0	289791.0	5.0	*	
12. R12 NE 82	* 270057.0	289862.0	5.0	*	
13. R13 NE 164	* 270040.0	289942.0	5.0	*	
14. R14 NE Mid	* 270034.0	289968.0	5.0	*	
15. R15 NW 164	* 269944.0	290010.0	5.0	*	
16. R16 NW 82	* 269961.0	289930.0	5.0	*	
17. R17 NW Corner	* 269976.0	289859.0	5.0	*	
18. R18 SW Corner	* 270010.0	289716.0	5.0	*	
19. R19 SW 82	* 270028.0	289646.0	5.0	*	
20. R20 SW 164	* 270046.0	289566.0	5.0	*	
21. R21 SW Mid	* 270055.0	289525.0	5.0	*	

1

JOB: Brent Spence Bridge RUN: W 4th & Central Alt I PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

0.	*	.3	.6	.9	1.0	1.3	.5	.5	.0	.0	.0	.1	.1	.1	.2	.2	.3	.4	.9	.9	1.2
5.	*	.3	.5	.7	1.0	1.3	.5	.5	.0	.0	.0	.1	.1	.1	.1	.3	.3	.4	1.0	.9	1.3
10.	*	.2	.5	.7	1.1	1.3	.5	.5	.0	.0	.0	.1	.1	.1	.1	.3	.3	.4	.9	1.1	1.2
15.	*	.2	.3	.6	1.2	1.2	.5	.5	.0	.0	.0	.0	.0	.0	.3	.3	.4	1.0	1.4	1.2	
20.	*	.1	.3	.6	1.2	1.1	.5	.5	.0	.0	.0	.0	.0	.0	.3	.3	.4	.7	1.4	1.2	
25.	*	.1	.3	.6	1.4	1.2	.6	.5	.0	.0	.0	.0	.0	.0	.3	.3	.4	.7	1.5	1.1	
30.	*	.1	.2	.5	1.5	1.1	.6	.6	.0	.0	.0	.0	.0	.0	.3	.3	.3	.8	1.7	1.0	
35.	*	.1	.1	.5	1.5	1.0	.6	.6	.0	.0	.1	.1	.0	.0	.3	.3	.3	.8	1.8	.9	
40.	*	.2	.1	.4	1.6	1.0	.6	.7	.0	.0	.1	.1	.0	.0	.3	.3	.3	.9	1.8	.8	

45.	*	.1	.2	.3	1.6	1.0	.7	.7	.0	.1	.1	.1	.0	.0	.0	.3	.3	.3	1.1	1.8	.5
50.	*	.0	.2	.2	1.6	1.0	.7	.8	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	1.2	1.8	.5
55.	*	.0	.1	.3	1.7	.9	.7	.8	.1	.1	.1	.1	.0	.0	.0	.3	.3	.3	1.4	1.6	.4
60.	*	.0	.0	.2	1.6	.9	.9	.8	.1	.1	.1	.2	.0	.0	.0	.3	.3	.3	1.4	1.5	.3
65.	*	.0	.0	.2	1.6	.9	.9	.9	.2	.3	.2	.3	.0	.0	.0	.3	.3	.3	1.4	1.5	.3
70.	*	.0	.0	.2	1.4	.9	.8	.7	.4	.3	.4	.4	.0	.0	.0	.3	.3	.3	1.6	1.2	.3
75.	*	.0	.0	.0	1.2	.8	.8	.7	.6	.5	.5	.8	.0	.0	.0	.3	.3	.4	1.8	1.2	.3
80.	*	.0	.0	.0	.9	.7	.6	.6	.6	.7	.7	1.0	.0	.0	.0	.3	.3	.4	1.5	1.1	.3
85.	*	.0	.0	.0	.6	.4	.5	.4	.7	.8	.9	1.3	.2	.0	.0	.3	.3	.6	1.5	1.0	.3
90.	*	.0	.0	.0	.4	.2	.3	.3	.8	.9	.9	1.5	.2	.0	.0	.3	.3	.7	1.5	.9	.3
95.	*	.0	.0	.0	.2	.2	.1	.1	.8	.9	1.0	1.5	.2	.0	.0	.3	.3	.9	1.3	.9	.3
100.	*	.0	.0	.0	.1	.1	.1	.1	.7	.7	1.0	1.6	.3	.1	.0	.3	.4	1.1	1.4	.9	.3
105.	*	.0	.0	.0	.1	.1	.1	.1	.7	.7	1.0	1.5	.2	.2	.1	.3	.4	1.2	1.3	.8	.3
110.	*	.0	.0	.0	.1	.1	.1	.1	.7	.7	1.1	1.6	.3	.2	.2	.4	.4	1.4	1.3	.8	.4
115.	*	.0	.0	.0	.1	.1	.1	.1	.7	.6	1.1	1.6	.4	.1	.2	.4	.5	1.3	1.3	.7	.4
120.	*	.1	.0	.0	.1	.1	.1	.1	.6	.6	1.1	1.4	.5	.1	.1	.4	.6	1.4	1.2	.6	.5
125.	*	.2	.0	.0	.1	.1	.1	.1	.6	.6	1.2	1.4	.5	.2	.1	.4	.6	1.5	1.2	.6	.6
130.	*	.2	.0	.0	.0	.0	.0	.0	.6	.6	1.2	1.3	.6	.3	.1	.5	.6	1.5	1.1	.5	.7
135.	*	.3	.1	.0	.0	.0	.0	.0	.5	1.2	1.3	.6	.3	.3	.5	.7	1.6	1.0	.6	.8	
140.	*	.3	.2	.0	.0	.0	.0	.5	.5	1.2	1.1	.6	.3	.3	.5	.7	1.6	1.1	.6	.8	
145.	*	.3	.3	.1	.1	.0	.0	.5	.5	1.3	1.0	.6	.4	.3	.5	.8	1.7	1.0	.6	.8	
150.	*	.4	.4	.2	.1	.0	.0	.5	.5	1.3	1.2	.6	.5	.3	.6	1.0	1.6	.9	.6	1.0	
155.	*	.4	.4	.4	.3	.0	.0	.5	.5	1.3	1.2	.8	.5	.3	.8	1.0	1.8	.9	.6	1.0	
160.	*	.6	.6	.4	.5	.0	.0	.5	.5	1.4	1.4	.9	.6	.4	.8	1.2	1.7	.7	.5	1.0	
165.	*	.5	.5	.4	.7	.0	.0	.5	.5	1.4	1.6	1.2	.8	.7	.8	.9	1.4	.5	.4	.8	
170.	*	.6	.7	.5	1.0	.2	.0	.5	.5	1.6	1.9	1.2	1.0	1.1	.6	.8	1.0	.5	.4	.7	
175.	*	.7	.7	.8	1.2	.2	.0	.5	.5	1.6	1.8	1.3	1.0	.9	.5	.8	1.1	.2	.4	.6	
180.	*	.7	.7	.8	1.4	.2	.0	.5	.5	1.6	1.9	1.3	.9	.8	.3	.6	.9	.2	.2	.5	
185.	*	.8	.8	.7	1.6	.2	.2	.6	.7	1.8	1.9	1.1	.7	.7	.4	.7	.8	.2	.2	.5	
190.	*	.9	.7	.8	1.7	.3	.2	.1	.7	.7	1.9	1.8	1.1	.7	.9	.4	.6	.9	.2	.3	.5
195.	*	.9	.7	.8	1.8	.3	.2	.2	.7	.7	1.9	1.9	.8	.7	.7	.5	.7	.8	.1	.2	.5
200.	*	.9	.7	.7	2.0	.3	.2	.2	.7	.7	2.0	1.7	.8	.8	.8	.5	.6	.9	.1	.2	.5
205.	*	.9	.6	.7	2.2	.3	.2	.2	.7	.9	2.2	1.5	.6	.8	.8	.5	.6	.8	.2	.2	.5

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 JOB: Brent Spence Bridge
 RUN: W 4th & Central Alt I PM

PAGE 4

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

210.	*	.9	.6	.7	2.0	.6	.1	.2	.7	1.0	2.4	1.3	.6	.8	.8	.5	.6	.7	.2	.3	.5
215.	*	.9	.6	.8	1.9	.7	.2	.2	.9	1.2	2.3	1.2	.8	.9	.7	.5	.6	.7	.2	.2	.5
220.	*	.7	.5	.9	1.9	.9	.4	.2	.9	1.2	2.2	1.2	.7	.7	.6	.5	.6	.7	.1	.2	.5
225.	*	.7	.5	1.0	1.8	.9	.4	.3	1.1	1.6	1.9	1.3	.7	.6	.6	.4	.7	.7	.2	.2	.5
230.	*	.7	.5	1.1	1.8	.9	.4	.3	1.2	1.6	1.8	1.1	.8	.6	.5	.4	.6	.8	.2	.2	.4
235.	*	.7	.5	1.0	1.8	.9	.6	.3	1.3	1.5	1.8	1.0	.8	.4	.4	.4	.6	.8	.2	.2	.5
240.	*	.7	.5	1.0	1.8	1.0	.6	.4	1.2	1.5	1.5	1.1	.9	.4	.4	.4	.5	.7	.2	.2	.4
245.	*	.7	.6	1.1	1.7	1.1	.9	.6	1.3	1.6	1.3	1.1	1.0	.4	.4	.4	.5	.7	.2	.3	.4
250.	*	.7	.6	1.2	1.5	1.1	1.0	.7	1.3	1.3	1.1	1.1	.9	.5	.5	.4	.5	.6	.3	.3	.6
255.	*	.7	.5	1.2	1.5	1.0	.9	.9	1.0	1.1	1.0	1.1	.8	.5	.5	.4	.5	.6	.3	.3	.6
260.	*	.7	.5	1.2	1.3	1.2	1.2	1.3	.8	.8	.7	.9	.8	.5	.5	.4	.5	.6	.2	.4	.6
265.	*	.6	.7	1.4	1.4	1.3	1.3	1.2	.6	.7	.7	.8	.8	.5	.5	.4	.5	.6	.2	.4	.7
270.	*	.7	.6	1.3	1.1	1.3	1.3	1.1	.5	.5	.8	.9	.7	.4	.4	.4	.5	.6	.2	.4	.7
275.	*	.8	.6	1.3	.9	1.3	1.4	1.3	.2	.4	.5	.9	.6	.4	.4	.4	.5	.6	.0	.3	.8
280.	*	.7	.5	1.4	1.0	1.7	1.4	1.2	.3	.3	.5	.7	.6	.4	.4	.4	.5	.6	.0	.2	.9
285.	*	.9	.6	1.3	1.0	1.8	1.3	1.0	.3	.3	.6	.9	.6	.5	.5	.4	.5	.7	.0	.1	.7
290.	*	.9	.6	1.4	1.2	1.8	1.2	1.0	.3	.3	.5	.8	.6	.6	.5	.4	.5	.7	.0	.0	.6
295.	*	.7	.5	1.5	1.2	2.1	1.2	1.0	.3	.4	.5	.8	.6	.6	.5	.4	.6	.8	.0	.0	.3
300.	*	.6	.6	1.6	1.3	2.1	1.1	.9	.2	.2	.5	1.0	.7	.7	.6	.4	.6	.8	.0	.0	.2
305.	*	.4	.8	1.8	1.4	2.1	.9	.8	.2	.2	.3	1.1	.7	.6	.6	.4	.6	.9	.0	.0	.2
310.	*	.6	.9	1.8	1.4	2.0	.9	.8	.2	.2	.3	1.0	.7	.6	.6	.4	.6	.9	.1	.0	.0
315.	*	.7	1.2	2.1	1.7	1.7	.7	.7	.2	.2	.3	1.0	.7	.6	.6	.4	.6	1.0	.1	.0	.0
320.	*	.8	1.2	2.0	1.5	1.7	.7	.7	.1	.2	.2	.8	.7	.7	.6	.3	.6	1.0	.3	.1	.0
325.	*	.9	1.3	1.9	1.4	1.6	.6	.6	.0	.1	.2	.9	.7	.6	.6	.3	.5	1.0	.4	.2	.1
330.	*	1.0	1.6	2.0	1.4	1.6	.6	.5	.0	.1	.2	.8	.6	.6	.6	.2	.4	.9	.6	.3	.1
335.	*	1.2	1.5	1.8	1.5	1.5	.5	.5	.0	.0	.1	.6	.6	.4	.4	.1	.3	.8	.6	.4	.3
340.	*	1.1	1.4	1.4	1.1	1.5	.5	.5	.0	.0	.1	.5	.4	.4	.4	.2	.3	.7	1.0	.6	.5
345.	*	1.0	1.2	1.1	1.3	1.5	.5	.5	.0	.0	.1	.4	.4	.4	.4	.1	.3	.7	1.0	.6	.6
350.	*	.7	.7	.9	1.2	1.5	.6	.6	.0	.0	.0	.4	.3	.3	.3	.2	.3	.5	1.0	.9	.8
355.	*	.5	.9	.7	1.1	1.4	.5	.5	.0	.0	.2	.2	.2	.2	.2	.2	.4	1.0	.9	1.0	
360.	*	.3	.6	.9	1.0	1.3	.5	.5	.0	.0	.0	.1	.1	.1	.2	.2	.3	.4	.9	.9	1.2

MAX * 1.2 1.6 2.1 2.2 2.1 1.4 1.3 1.3 1.6 2.4 1.9 1.3 1.0 1.1 .8 1.2 1.8 1.8 1.8 1.3
 DEGR. * 335 330 315 205 295 275 260 235 225 210 170 175 170 170 155 160 155 75 35 5

1
 JOB: Brent Spence Bridge
 RUN: W 4th & Central Alt I PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21

0. * 1.2
 5. * 1.1
 10. * 1.0

15. * 1.0
 20. * .8
 25. * .6
 30. * .6
 35. * .5
 40. * .4
 45. * .4
 50. * .4
 55. * .3
 60. * .4
 65. * .4
 70. * .4
 75. * .5
 80. * .5
 85. * .5
 90. * .2
 95. * .4
 100. * .4
 105. * .5
 110. * .8
 115. * 1.0
 120. * 1.3
 125. * 1.5
 130. * 1.6
 135. * 1.6
 140. * 1.7
 145. * 1.6
 150. * 1.6
 155. * 1.4
 160. * 1.3
 165. * 1.2
 170. * 1.1
 175. * 1.0
 180. * .8
 185. * .8
 190. * .8
 195. * .7
 200. * .7
 205. * .7
 1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I PM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21
 -----*

210. * .7
 215. * .7
 220. * .7
 225. * .7
 230. * .7
 235. * .7
 240. * .7
 245. * .8
 250. * .8
 255. * .8
 260. * .8
 265. * 1.0
 270. * 1.1
 275. * 1.3
 280. * 1.4
 285. * 1.5
 290. * 1.5
 295. * 1.4
 300. * 1.3
 305. * 1.2
 310. * 1.0
 315. * .8
 320. * .5
 325. * .5
 330. * .4
 335. * .3
 340. * .7
 345. * .8
 350. * .9
 355. * 1.2
 360. * 1.2
 -----*

MAX * 1.7
 DEGR. * 140

THE HIGHEST CONCENTRATION IS 2.40 PPM AT 210 DEGREES FROM REC10.
 THE 2ND HIGHEST CONCENTRATION IS 2.20 PPM AT 205 DEGREES FROM REC4 .
 THE 3RD HIGHEST CONCENTRATION IS 2.10 PPM AT 315 DEGREES FROM REC3 .
 1

JOB: Brent Spence Bridge

RUN: W 4th & Central Alt I PM

DATE: 08/31/2010 TIME: 12:15:58.33

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)

REC19	REC20	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18			
LINK #	*	335	330	315	205	295	275	260	235	225	210	170	175	170	170	155	160	155	75	35	5	
1	*	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0
2	*	.3	.3	.3	.3	.0	.0	.0	.1	.1	.2	.1	.1	.1	.0	.1	.1	.1	.1	.1	.1	.1
3	*	.1	.2	.7	.8	.0	.0	.1	.1	.1	.2	.3	.1	.1	.1	.0	.1	.1	.1	.2	.3	.1
4	*	.0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	*	.1	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2	.3	.1	.0	.0	.0	.0	.0	.0	.1
6	*	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1
7	*	.3	.5	.5	.7	.0	.0	.1	.1	.2	.3	.3	.2	.1	.1	.1	.1	.2	.4	.7	.5	.5
8	*	.1	.1	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.1	.2	.4	.0	.0	.0	.1
9	*	.1	.2	.2	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.3	.0	.0	.0	.0
10	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0
11	*	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0
12	*	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1
13	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
16	*	.1	.1	.1	.0	.6	.7	.6	.7	.7	.6	.6	.2	.1	.1	.1	.1	.1	.5	.3	.1	.1
17	*	.0	.0	.0	.0	.9	.5	.3	.3	.4	.9	.1	.1	.1	.1	.0	.0	.3	.2	.1	.1	.1
18	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	*	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.1	.1	.1	.0	.1	.1	.1	.0	.0	.0	.0
22	*	.0	.0	.0	.1	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27	*	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 12:15:58.33

PAGE 8
 RUN: W 4th & Central Alt I PM

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21
 LINK # * 140

1	*	.3
2	*	.0
3	*	.0
4	*	.0
5	*	.0
6	*	.0
7	*	.0
8	*	.0
9	*	.0
10	*	.0
11	*	.0
12	*	.0
13	*	.1
14	*	.0
15	*	.0
16	*	.0
17	*	.0
18	*	.0
19	*	.0
20	*	.1
21	*	1.1
22	*	.0
23	*	.0
24	*	.0
25	*	.1
26	*	.0
27	*	.0
28	*	.0
29	*	.0

1

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000 PAGE 1

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 10:52:41.98

RUN: W 4th & Central No Bld AM

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	* (FT) (DEG)	LENGTH (G/M)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 NB Cent McF Appr	* 270186.0	289164.0	270108.0	289529.0	*	373.	348.	AG	370.	12.6	.0	44.0		
2. 2 NB Thr W 4th Appr	* 270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	270.	12.6	.0	44.0		
3. 3 NB Cent NB Queue	* 270067.0	289730.0	270073.0	289706.4	*	24.	166.	AG	216.	100.0	.0	24.0	.23	1.2
4. 4 NB Cen W 4th Depr	* 270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	340.	12.6	.0	44.0		
5. 5 NB Cen W 4th Dept	* 270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	340.	12.6	.0	44.0		
6. 6 NB Lt W 4th Appr	* 270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	100.	12.6	.0	44.0		

7. 7 NB LefttNB Queue	* 270049.0	289728.0	270063.0	289670.0	*	60.	166. AG	354.	100.0	.0	24.0	1.02	3.0
8. 8 NB Ramp From W 4th	* 270042.0	289755.0	269974.0	289811.0	*	88.	309. AG	290.	12.6	.0	44.0		
9. 9 NB Ramp From W 4th	* 269974.0	289811.0	269755.0	290270.0	*	509.	334. AG	290.	12.6	.0	44.0		
10. 10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168. AG	130.	12.6	.0	44.0		
11. 11 SB CentSB Queue	* 27007.2	89828.2	27021.4	89828.2	*	14.	89. AG	262.	100.0	.0	24.0	.16	.7
12. 12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166. AG	280.	12.6	.0	44.0		
13. 13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168. AG	280.	12.6	.0	44.0		
14. 14 WB W 4tTo Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259. AG	410.	12.6	.0	44.0		
15. 15 WB W 4tFr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257. AG	410.	12.6	.0	44.0		
16. 16 WB W 4tTo Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258. AG	410.	12.6	.0	56.0		
17. 17 WB W 4tWB Queue	* 270089.0	289764.0	270117.3	289770.1	*	29.	78. AG	383.	100.0	.0	36.0	.32	1.5
18. 18 WB Off 3rd-SB 75	* 270473.0	289330.0	270387.0	289337.0	*	86.	275. BR	260.	12.1	.0	32.0		
19. 19 WB Off 3rd-SB 75	* 270387.0	289337.0	270291.0	289353.0	*	97.	279. BR	260.	12.1	.0	32.0		
20. 20 WB Off 3rd-SB 75	* 270291.0	289353.0	270209.0	289396.0	*	93.	298. BR	260.	12.1	.0	32.0		
21. 21 WB Off 3rd-SB 75	* 270209.0	289396.0	269996.0	289555.0	*	266.	307. BR	260.	12.1	.0	28.0		
22. 22 WB Off 3rd-SB 75	* 269996.0	289555.0	269861.0	289614.0	*	147.	294. BR	260.	12.1	.0	32.0		
23. 23 WB Off 71- SB 75	* 270427.0	289288.0	270271.0	289320.0	*	159.	282. BR	2420.	12.1	.0	44.0		
24. 24 WB Off 71- SB 75	* 270271.0	289320.0	270153.0	289385.0	*	135.	299. BR	2420.	12.1	.0	44.0		
25. 25 WB Off 71- SB 75	* 270153.0	289385.0	269986.0	289528.0	*	220.	311. BR	2420.	12.1	.0	44.0		
26. 26 WB Off 71- SB 75	* 269986.0	289528.0	269861.0	289614.0	*	152.	305. BR	2420.	12.1	.0	44.0		
27. 27 WB Off 71- SB 75	* 269861.0	289614.0	269702.0	289652.0	*	163.	283. BR	2680.	12.1	.0	44.0		
28. 28 WB Off 71- SB 75	* 269702.0	289652.0	269576.0	289645.0	*	126.	267. BR	2680.	12.1	.0	44.0		
29. 29 WB Off 71- SB 75	* 269576.0	289645.0	269470.0	289614.0	*	110.	254. BR	2680.	12.1	.0	44.0		
30. 30 WB Off WB 71- 6th	* 270360.0	289236.0	270239.0	289258.0	*	123.	280. BR	2850.	12.1	.0	44.0		
31. 31 WB Off WB 71- 6th	* 270239.0	289258.0	270109.0	289317.0	*	143.	294. BR	2850.	12.1	.0	44.0		
32. 32 WB Off WB 71- 6th	* 270109.0	289317.0	270024.0	289390.0	*	112.	311. BR	2850.	12.1	.0	44.0		
33. 33 WB Off WB 71- 6th	* 270024.0	289390.0	269967.0	289470.0	*	98.	325. BR	2850.	12.1	.0	44.0		
34. 34 WB Off WB 71- 6th	* 269967.0	289470.0	269923.0	289566.0	*	106.	335. BR	2850.	12.1	.0	44.0		
35. 35 WB Off WB 71- 6th	* 269923.0	289566.0	269895.0	289698.0	*	135.	348. BR	2850.	12.1	.0	44.0		
36. 36 WB Off WB 71- 75	* 269895.0	289698.0	269888.0	289755.0	*	57.	353. AG	1910.	12.1	.0	32.0		
37. 37 WB Off WB 71- 75	* 269888.0	289755.0	269844.0	289970.0	*	219.	348. AG	1910.	12.1	.0	32.0		
38. 38 WB Off WB 71- 75	* 269844.0	289970.0	269818.0	290061.0	*	95.	344. AG	1910.	12.1	.0	32.0		
39. 39 WB Off WB 71- 75	* 269818.0	290061.0	269729.0	290257.0	*	215.	336. AG	1910.	12.1	.0	32.0		
40. 40 WB Off WB 71-6th	* 269895.0	289698.0	269874.0	289754.0	*	60.	339. AG	940.	12.1	.0	32.0		
41. 41 WB Off WB 71-6th	* 269874.0	289754.0	269831.0	289896.0	*	148.	343. AG	940.	12.1	.0	32.0		
42. 42 WB Off WB 71-6th	* 269831.0	289896.0	269791.0	289993.0	*	105.	338. AG	940.	12.1	.0	32.0		
43. 43 WB Off WB 71-6th	* 269791.0	289993.0	269680.0	290221.0	*	254.	334. AG	940.	12.1	.0	32.0		

JOB: Brent Spence Bridge RUN: W 4th & Central No Bld AM
 DATE: 08/31/2010 TIME: 10:52:41.98

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
3. 3 NB Cent NB Queue	* 60	33	2.0	270	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 60	54	2.0	100	1474	73.30	1	3
11. 11 SB CentSB Queue	* 60	40	2.0	130	1522	73.30	1	3
17. 17 WB W 4tWB Queue	* 60	39	2.0	410	1487	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	Y	Z	*
1. R1 SE Mid	* 270140.0	289517.0	5.0	*	
2. R2 SE 164	* 270124.0	289585.0	5.0	*	
3. R3 SE 82	* 270105.0	289664.0	5.0	*	
4. R4 SE Corner	* 270088.0	289735.0	5.0	*	
5. R5 SE 82	* 270158.0	289749.0	5.0	*	
6. R6 SE 164	* 270239.0	289766.0	5.0	*	
7. R7 SE Mid	* 270274.0	289773.0	5.0	*	
8. R8 NE Mid	* 270256.0	289830.0	5.0	*	
9. R9 NE 164	* 270223.0	289823.0	5.0	*	
10. R10 NE 82	* 270142.0	289806.0	5.0	*	
11. R11 NE Corner	* 270072.0	289791.0	5.0	*	
12. R12 NE 82	* 270057.0	289862.0	5.0	*	
13. R13 NE 164	* 270040.0	289942.0	5.0	*	
14. R14 NE Mid	* 270034.0	289968.0	5.0	*	
15. R15 NW 164	* 269944.0	290010.0	5.0	*	
16. R16 NW 82	* 269961.0	289930.0	5.0	*	
17. R17 NW Corner	* 269976.0	289859.0	5.0	*	
18. R18 SW Corner	* 270010.0	289716.0	5.0	*	
19. R19 SW 82	* 270028.0	289646.0	5.0	*	
20. R20 SW 164	* 270046.0	289566.0	5.0	*	
21. R21 SW Mid	* 270055.0	289525.0	5.0	*	
22. R22 Near CD	* 269775.0	289723.0	5.0	*	

JOB: Brent Spence Bridge RUN: W 4th & Central No Bld AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22

Angle (DEGR)	REC21 (PPM)	REC22 (PPM)
0.	.4	.4
5.	.6	.5
10.	.5	.5
15.	.5	.6
20.	.4	.4
25.	.2	.3
30.	.2	.4
35.	.2	.4
40.	.2	.4
45.	.2	.4
50.	.2	.4
55.	.2	.3
60.	.2	.3
65.	.2	.4
70.	.2	.5
75.	.1	.4
80.	.1	.4
85.	.1	.6
90.	.2	.5
95.	.3	.5
100.	.3	.5
105.	.3	.6
110.	.4	.5
115.	.5	.7
120.	.6	.8
125.	.8	1.0
130.	1.0	1.3
135.	1.2	1.6
140.	1.3	1.4
145.	1.7	1.4
150.	1.8	1.1
155.	1.8	.8
160.	1.8	.7
165.	1.6	.5
170.	1.4	.5
175.	1.5	.5
180.	1.4	.5
185.	1.4	.5
190.	1.3	.5
195.	1.3	.5
200.	1.2	.5
205.	1.3	.6

1

JOB: Brent Spence Bridge

PAGE 6
RUN: W 4th & Central No Bld AM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22

Angle (DEGR)	REC21 (PPM)	REC22 (PPM)
210.	1.2	.5
215.	1.2	.6
220.	1.3	.5
225.	1.3	.6
230.	1.2	.6
235.	1.3	.7
240.	1.3	.6
245.	1.3	.7
250.	1.4	.5
255.	1.4	.5
260.	1.3	.3
265.	1.4	.2
270.	1.6	.2
275.	1.9	.0
280.	1.9	.0
285.	2.0	.0
290.	1.8	.0
295.	1.7	.0
300.	1.4	.0
305.	1.0	.0
310.	.7	.0
315.	.7	.0
320.	.6	.0
325.	.5	.0
330.	.2	.0
335.	.4	.0
340.	.3	.0
345.	.3	.1
350.	.2	.2
355.	.3	.2
360.	.4	.4

MAX * 2.0 1.6
DEGR. * 285 135

THE HIGHEST CONCENTRATION IS 2.00 PPM AT 285 DEGREES FROM REC21.
THE 2ND HIGHEST CONCENTRATION IS 2.00 PPM AT 215 DEGREES FROM REC4.
THE 3RD HIGHEST CONCENTRATION IS 1.60 PPM AT 190 DEGREES FROM REC11.

1

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

LINK #	* 285	270	265	215	240	255	265	235	225	210	190	175	185	185	225	170	155	80	20	275	
1 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2 *	.0	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0
3 *	.0	.0	.0	.5	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0
4 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0
6 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7 *	.0	.0	.2	.7	.3	.1	.1	.1	.1	.2	.4	.2	.1	.1	.0	.1	.2	.5	.6	.0	.0
8 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.1	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0
13 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16 *	.0	.0	.0	.0	.1	.2	.2	.2	.2	.1	.0	.0	.0	.0	.0	.1	.1	.0	.1	.0	.0
17 *	.0	.0	.0	.0	.1	.1	.1	.1	.4	.0	.1	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0
18 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
23 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0
25 *	.1	.0	.0	.1	.0	.0	.0	.1	.1	.2	.1	.1	.1	.1	.0	.1	.1	.0	.0	.0	.0
26 *	.3	.3	.1	.2	.1	.1	.0	.1	.1	.1	.0	.1	.1	.0	.1	.1	.0	.0	.0	.5	.0
27 *	.1	.1	.2	.0	.1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0
28 *	.1	.1	.1	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.0
29 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.0
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0
33 *	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.1	.1	.0	.1	.0	.1	.0	.0	.0	.0	.0
34 *	.2	.1	.0	.2	.1	.0	.0	.1	.1	.1	.0	.1	.1	.1	.0	.1	.0	.0	.0	.2	.0
35 *	.2	.2	.3	.1	.2	.1	.1	.1	.1	.0	.0	.1	.1	.0	.1	.0	.1	.0	.0	.3	.0
36 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
37 *	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	.0	.0
38 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
39 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
41 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
42 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
43 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22

LINK #	* 285	135
1 *	.0	.0
2 *	.0	.0
3 *	.0	.0
4 *	.0	.0
5 *	.0	.0
6 *	.0	.0
7 *	.0	.0
8 *	.0	.0
9 *	.0	.0
10 *	.0	.0
11 *	.0	.0
12 *	.0	.0
13 *	.0	.0
14 *	.0	.0
15 *	.0	.0
16 *	.0	.0
17 *	.0	.0
18 *	.0	.0
19 *	.0	.0
20 *	.0	.0
21 *	.2	.0
22 *	.0	.0
23 *	.0	.0
24 *	.0	.1
25 *	.3	.2
26 *	.6	.3
27 *	.2	.2

28 * .1 .0
 29 * .1 .0
 30 * .0 .0
 31 * .0 .1
 32 * .0 .1
 33 * .0 .1
 34 * .3 .2
 35 * .2 .3
 36 * .0 .0
 37 * .0 .0
 38 * .0 .0
 39 * .0 .0
 40 * .0 .0
 41 * .0 .0
 42 * .0 .0
 43 * .0 .0

JOB: Brent Spence Bridge RUN: W 4th & Central No Bld PM
 DATE: 08/31/2010 TIME: 10:59:15.96

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	* (FT) (DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. 1 NB Cent McF Appr	* 270186.0	289164.0	270108.0	289529.0	*	373.	348.	AG	1350.	12.6	.0	44.0		
2. 2 NB Thr W 4th Appr	* 270117.0	289531.0	270060.0	289759.0	*	235.	346.	AG	500.	12.6	.0	44.0		
3. 3 NB Cent NB Queue	* 270067.0	289730.0	270084.3	289662.5	*	70.	166.	AG	191.	100.0	.0	24.0	.35	3.5
4. 4 NB Cen W 4th Dep	* 270060.0	289759.0	270043.0	289808.0	*	52.	341.	AG	650.	12.6	.0	44.0		
5. 5 NB Cen W 4th Dept	* 270043.0	289808.0	269933.0	290337.0	*	540.	348.	AG	650.	12.6	.0	44.0		
6. 6 NB Lt W 4th Appr	* 270099.0	289527.0	270042.0	289755.0	*	235.	346.	AG	850.	12.6	.0	44.0		
7. 7 NB LefttNB Queue	* 270049.0	289728.0	270093.6	289543.5	*	190.	166.	AG	251.	100.0	.0	24.0	.89	9.6
8. 8 NB Ramp From W 4th	* 270042.0	289755.0	269974.0	289811.0	*	88.	309.	AG	1600.	12.6	.0	44.0		
9. 9 NB Ramp From W 4th	* 269974.0	289811.0	269755.0	290270.0	*	509.	334.	AG	1600.	12.6	.0	44.0		
10. 10 SB CentSB Appr	* 269902.0	290330.0	270023.0	289751.0	*	591.	168.	AG	160.	12.6	.0	44.0		
11. 11 SB CentSB Queue	* 27007.2	89828.2	27303.8	89829.0	*	297.	90.	AG	333.	100.0	.0	24.0	1.36	15.1
12. 12 SB CentSB Dep	* 270023.0	289751.0	270080.0	289522.0	*	236.	166.	AG	350.	12.6	.0	44.0		
13. 13 SB CentSB Dep	* 270080.0	289522.0	270159.0	289159.0	*	371.	168.	AG	350.	12.6	.0	44.0		
14. 14 WB W 4tTo Plum	* 270636.0	289880.0	270490.0	289851.0	*	149.	259.	AG	1040.	12.6	.0	44.0		
15. 15 WB W 4tFr Plum	* 270490.0	289851.0	270352.0	289819.0	*	142.	257.	AG	1040.	12.6	.0	44.0		
16. 16 WB W 4tTo Cent	* 270352.0	289819.0	270042.0	289755.0	*	317.	258.	AG	1040.	12.6	.0	56.0		
17. 17 WB W 4tWB Queue	* 270089.0	289764.0	270211.1	289790.3	*	125.	78.	AG	371.	100.0	.0	36.0	.68	6.3
18. 18 WB Off 3rd-SB 75	* 270473.0	289330.0	270387.0	289337.0	*	86.	275.	BR	1200.	12.1	.0	32.0		
19. 19 WB Off 3rd-SB 75	* 270387.0	289337.0	270291.0	289353.0	*	97.	279.	BR	1200.	12.1	.0	32.0		
20. 20 WB Off 3rd-SB 75	* 270291.0	289353.0	270209.0	289396.0	*	93.	298.	BR	1200.	12.1	.0	32.0		
21. 21 WB Off 3rd-SB 75	* 270209.0	289396.0	269996.0	289555.0	*	266.	307.	BR	1200.	12.1	.0	28.0		
22. 22 WB Off 3rd-SB 75	* 269996.0	289555.0	269861.0	289614.0	*	147.	294.	BR	1200.	12.1	.0	32.0		
23. 23 WB Off 71- SB 75	* 270427.0	289288.0	270271.0	289320.0	*	159.	282.	BR	3140.	12.1	.0	44.0		
24. 24 WB Off 71- SB 75	* 270271.0	289320.0	270153.0	289385.0	*	135.	299.	BR	3140.	12.1	.0	44.0		
25. 25 WB Off 71- SB 75	* 270153.0	289385.0	269986.0	289528.0	*	220.	311.	BR	3140.	12.1	.0	44.0		
26. 26 WB Off 71- SB 75	* 269986.0	289528.0	269861.0	289614.0	*	152.	305.	BR	3140.	12.1	.0	44.0		
27. 27 WB Off 71- SB 75	* 269861.0	289614.0	269702.0	289652.0	*	163.	283.	BR	4340.	12.1	.0	44.0		
28. 28 WB Off 71- SB 75	* 269702.0	289652.0	269576.0	289645.0	*	126.	267.	BR	4340.	12.1	.0	44.0		
29. 29 WB Off 71- SB 75	* 269576.0	289645.0	269470.0	289614.0	*	110.	254.	BR	4340.	12.1	.0	44.0		
30. 30 WB Off WB 71- 6th	* 270360.0	289236.0	270239.0	289258.0	*	123.	280.	BR	3050.	12.1	.0	44.0		
31. 31 WB Off WB 71- 6th	* 270239.0	289258.0	270109.0	289317.0	*	143.	294.	BR	3050.	12.1	.0	44.0		
32. 32 WB Off WB 71- 6th	* 270109.0	289317.0	270024.0	289390.0	*	112.	311.	BR	3050.	12.1	.0	44.0		
33. 33 WB Off WB 71- 6th	* 270024.0	289390.0	269967.0	289470.0	*	98.	325.	BR	3050.	12.1	.0	44.0		
34. 34 WB Off WB 71- 6th	* 269967.0	289470.0	269923.0	289566.0	*	106.	335.	BR	3050.	12.1	.0	44.0		
35. 35 WB Off WB 71- 6th	* 269923.0	289566.0	269895.0	289698.0	*	135.	348.	BR	3050.	12.1	.0	44.0		
36. 36 WB Off WB 71- 75	* 269895.0	289698.0	269888.0	289755.0	*	57.	353.	AG	1600.	12.1	.0	32.0		
37. 37 WB Off WB 71- 75	* 269888.0	289755.0	269844.0	289970.0	*	219.	348.	AG	1600.	12.1	.0	32.0		
38. 38 WB Off WB 71- 75	* 269844.0	289970.0	269818.0	290061.0	*	95.	344.	AG	1600.	12.1	.0	32.0		
39. 39 WB Off WB 71- 75	* 269818.0	290061.0	269729.0	290257.0	*	215.	336.	AG	1600.	12.1	.0	32.0		
40. 40 WB Off WB 71- 6th	* 269895.0	289698.0	269874.0	289754.0	*	60.	339.	AG	1450.	12.1	.0	32.0		
41. 41 WB Off WB 71- 6th	* 269874.0	289754.0	269831.0	289896.0	*	148.	343.	AG	1450.	12.1	.0	32.0		
42. 42 WB Off WB 71- 6th	* 269831.0	289896.0	269791.0	289993.0	*	105.	338.	AG	1450.	12.1	.0	32.0		
43. 43 WB Off WB 71- 6th	* 269791.0	289993.0	269680.0	290221.0	*	254.	334.	AG	1450.	12.1	.0	32.0		

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE (SEC)	RED TIME (SEC)	CLEARANCE (VPH)	APPROACH (VPH)	SATURATION (gm/hr)	IDLE	SIGNAL	ARRIVAL
	* LENGTH (SEC)	* TIME (SEC)	* VOL (VPH)	* FLOW RATE (VPH)	* EM FAC (gm/hr)	* TYPE	* RATE	
3. 3 NB Cent NB Queue	* 105	51	2.0	500	1522	73.30	1	3
7. 7 NB LefttNB Queue	* 105	67	2.0	850	1474	73.30	1	3
11. 11 SB CentSB Queue	* 105	89	2.0	160	522	73.30	1	3
17. 17 WB W 4tWB Queue	* 105	66	2.0	1040	1528	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	*
1. R1 SE Mid	* 270140.0	289517.0	5.0	*
2. R2 SE 164	* 270124.0	289585.0	5.0	*

250.	*	1.7	2.1	2.1	2.3	1.6	1.3	1.2	1.7	1.9	1.5	1.7	1.1	.9	.9	.7	.9	1.3	1.1	1.2	1.4
255.	*	1.9	2.1	2.3	2.2	1.6	1.6	1.6	1.5	1.5	1.3	1.9	1.0	1.0	.7	.8	.9	1.3	1.2	1.3	1.6
260.	*	1.8	2.1	2.4	2.1	1.5	1.8	1.8	1.2	1.2	1.6	.9	.9	.7	.8	.9	1.0	1.0	1.4	1.8	
265.	*	1.9	2.6	2.4	2.0	1.7	1.9	1.6	1.0	1.1	1.1	1.4	.9	.8	.8	.8	1.0	.9	1.5	1.9	
270.	*	2.4	2.2	2.2	1.8	1.8	1.8	1.7	.8	.7	.8	1.1	.9	.8	.9	.8	.8	1.1	.6	1.3	2.0
275.	*	2.0	2.3	2.1	1.7	1.8	2.0	1.7	.5	.7	.6	1.0	1.0	.9	1.0	.7	.9	1.1	.5	1.2	2.1
280.	*	2.3	2.2	2.1	1.5	1.9	2.0	1.5	.4	.4	.7	1.1	.9	1.0	.9	.9	1.0	1.1	.4	.9	2.0
285.	*	2.4	2.1	2.1	1.2	2.0	2.0	1.4	.4	.5	.7	1.1	.8	1.0	.9	.9	1.0	1.2	.4	.8	2.0
290.	*	2.2	1.7	2.1	1.4	2.1	1.9	1.2	.3	.4	.4	1.1	.8	.9	.9	.9	1.0	1.2	.4	.7	1.6
295.	*	2.0	1.5	1.9	1.5	2.3	1.8	1.1	.4	.4	.4	1.1	1.0	.9	.9	1.0	1.0	1.2	.5	.4	1.3
300.	*	1.8	1.5	2.0	1.5	2.2	1.6	1.0	.3	.4	.5	1.0	1.0	.9	.9	1.0	1.3	1.4	.4	.5	1.0
305.	*	1.6	1.6	2.2	1.7	2.2	1.6	.9	.3	.5	.5	1.2	.9	.9	.8	.9	1.2	1.5	.4	.5	.6
310.	*	1.6	1.7	2.2	1.8	2.0	1.3	.7	.2	.3	.5	1.2	.9	.8	.7	.8	1.1	1.5	.5	.5	.8
315.	*	1.6	1.8	2.5	1.7	2.0	1.1	.6	.2	.2	.5	1.3	1.1	.7	.8	.7	1.0	1.6	.6	.6	.6
320.	*	1.6	1.8	2.3	1.6	1.9	1.0	.6	.1	.2	.4	1.2	1.0	.8	.7	.6	1.1	1.5	.8	.5	.6
325.	*	1.6	1.7	2.4	1.5	1.6	.9	.5	.1	.1	.2	.9	.8	.7	.6	.4	.9	1.4	1.1	.6	.5
330.	*	1.8	1.8	2.0	1.4	1.6	.7	.4	.0	.1	.2	.8	.6	.5	.5	.3	.6	1.4	1.0	.8	.6
335.	*	1.8	1.5	1.6	1.2	1.5	.5	.4	.0	.0	.1	.6	.5	.4	.4	.1	.4	1.0	1.1	.8	.6
340.	*	1.5	1.5	1.4	1.0	1.6	.4	.4	.0	.0	.1	.5	.4	.4	.4	.1	.3	.9	1.2	.8	.7
345.	*	1.2	1.2	1.2	1.1	1.6	.4	.4	.0	.0	.1	.4	.4	.4	.4	.2	.3	.7	1.1	.7	.9
350.	*	.9	.9	.8	1.1	1.5	.4	.4	.0	.0	.0	.4	.3	.3	.3	.2	.3	.5	1.0	.8	.9
355.	*	.7	.8	.8	1.1	1.5	.4	.4	.0	.0	.0	.2	.2	.2	.2	.2	.5	1.0	.8	1.3	
360.	*	.4	.5	.8	1.0	1.4	.4	.4	.0	.0	.0	.1	.2	.2	.2	.3	.3	.5	1.0	1.0	1.5
MAX	*	2.4	2.6	2.5	2.6	2.3	2.0	1.8	2.0	2.5	2.9	2.7	2.2	1.6	1.5	1.2	1.7	2.2	2.0	2.0	2.3
DEGR	*	285	265	315	210	295	275	260	230	230	215	180	175	175	170	170	170	155	150	145	150

1

JOB: Brent Spence Bridge

PAGE 5
 RUN: W 4th & Central No Bld PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22

0.	*	1.6	.4
5.	*	1.6	.7
10.	*	1.6	.8
15.	*	1.6	.6
20.	*	1.6	.7
25.	*	1.5	.8
30.	*	1.3	.7
35.	*	1.3	.7
40.	*	1.3	.7
45.	*	1.0	.7
50.	*	.9	.6
55.	*	.9	.6
60.	*	.7	.6
65.	*	.8	.8
70.	*	.8	.8
75.	*	.7	.7
80.	*	.7	.7
85.	*	.7	.7
90.	*	.6	.8
95.	*	.8	.7
100.	*	.8	.6
105.	*	.8	.7
110.	*	1.0	.8
115.	*	1.2	1.0
120.	*	1.6	1.5
125.	*	2.1	1.7
130.	*	2.5	2.1
135.	*	2.6	2.1
140.	*	2.8	2.2
145.	*	3.0	1.9
150.	*	3.0	1.5
155.	*	3.0	1.2
160.	*	2.9	1.0
165.	*	2.7	.9
170.	*	2.6	.8
175.	*	2.4	.8
180.	*	2.2	.8
185.	*	2.1	.8
190.	*	2.1	.8
195.	*	2.0	.8
200.	*	1.9	.8
205.	*	1.9	.9

1

JOB: Brent Spence Bridge

PAGE 6
 RUN: W 4th & Central No Bld PM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21 REC22

210.	*	1.9	.9
------	---	-----	----

215. * 1.9 .8
 220. * 1.9 1.0
 225. * 1.9 1.1
 230. * 2.0 1.1
 235. * 1.9 1.1
 240. * 1.9 1.1
 245. * 2.1 1.0
 250. * 2.1 .9
 255. * 2.2 .7
 260. * 2.2 .5
 265. * 2.4 .3
 270. * 2.9 .2
 275. * 2.9 .0
 280. * 3.0 .0
 285. * 3.0 .0
 290. * 3.1 .0
 295. * 2.8 .0
 300. * 2.5 .0
 305. * 2.0 .0
 310. * 1.5 .0
 315. * 1.3 .0
 320. * 1.0 .0
 325. * .9 .0
 330. * .7 .0
 335. * .8 .0
 340. * .8 .1
 345. * 1.1 .1
 350. * .9 .3
 355. * 1.3 .4
 360. * 1.6 .4

MAX * 3.1 2.2
 DEGR. * 290 140

THE HIGHEST CONCENTRATION IS 3.10 PPM AT 290 DEGREES FROM REC21.
 THE 2ND HIGHEST CONCENTRATION IS 2.90 PPM AT 215 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS 2.70 PPM AT 180 DEGREES FROM REC11.

1

JOB: Brent Spence Bridge
 DATE: 08/31/2010 TIME: 10:59:15.96

RUN: W 4th & Central No Bld PM

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
 REC19 REC20

LINK # * 285 265 315 210 295 275 260 230 230 215 180 175 175 170 170 155 150 145 150

1	*	.3	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.2	.2	.4
2	*	.1	.2	.3	.3	.0	.0	.1	.1	.1	.2	.1	.1	.1	.0	.0	.1	.1	.1
3	*	.0	.0	.6	.6	.0	.0	.1	.1	.1	.1	.3	.1	.1	.0	.0	.1	.0	.0
4	*	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0
5	*	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.3	.3	.0	.0	.0	.0	.0
6	*	.2	.3	.3	.3	.0	.0	.1	.1	.1	.1	.3	.2	.1	.1	.1	.2	.3	.3
7	*	.1	.5	.4	.6	.0	.0	.1	.1	.2	.2	.5	.3	.2	.1	.1	.2	.5	.4
8	*	.0	.0	.2	.0	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.2	.4	.0	.0
9	*	.0	.0	.2	.0	.2	.1	.0	.0	.0	.0	.0	.0	.0	.3	.4	.3	.0	.0
10	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0
11	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12	*	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.1	.2	.2	.1
13	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
14	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16	*	.0	.0	.1	.0	.5	.6	.5	.5	.5	.5	.4	.2	.1	.1	.0	.1	.0	.0
17	*	.0	.0	.0	.0	1.1	1.0	.5	.6	1.1	1.1	.0	.1	.1	.1	.0	.0	.0	.0
18	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	*	.2	.1	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.1	.1	.1	.4
22	*	.1	.1	.0	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1
24	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.1	.0	.0	.1	.1	.2	.2
25	*	.2	.1	.0	.1	.0	.0	.1	.0	.1	.2	.2	.1	.1	.1	.1	.2	.2	.5
26	*	.3	.4	.0	.2	.0	.0	.1	.1	.2	.0	.0	.0	.1	.1	.0	.0	.0	.0
27	*	.2	.2	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	*	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	*	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1
31	*	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.0	.0	.1	.1	.1	.2
32	*	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.0	.0	.1
33	*	.0	.0	.1	.0	.0	.0	.0	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0
34	*	.2	.2	.0	.2	.0	.0	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0
35	*	.2	.2	.0	.0	.0	.1	.1	.1	.1	.0	.0	.0	.1	.1	.0	.0	.0	.0
36	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
37	*	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
38	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
39	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
41	*	.0	.0	.1	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
42	*	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
43	*	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

1

JOB: Brent Spence Bridge

RUN: W 4th & Central No Bld PM

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22
 LINK # * 290 140

LINK #	290	140
1	.0	.1
2	.0	.0
3	.0	.0
4	.0	.0
5	.0	.0
6	.0	.0
7	.0	.0
8	.0	.0
9	.0	.0
10	.0	.0
11	.0	.0
12	.0	.0
13	.0	.0
14	.0	.0
15	.0	.0
16	.0	.0
17	.0	.0
18	.0	.0
19	.0	.0
20	.0	.0
21	.7	.1
22	.3	.1
23	.0	.0
24	.0	.1
25	.3	.2
26	.7	.4
27	.4	.5
28	.1	.0
29	.1	.0
30	.0	.0
31	.0	.1
32	.0	.1
33	.0	.1
34	.2	.2
35	.3	.2
36	.0	.0
37	.0	.0
38	.0	.0
39	.0	.0
40	.0	.0
41	.0	.0
42	.0	.0
43	.0	.0

JOB: Central & McMillan Alt E AM RUN: Central & McMillan Alt E AM
 DATE: 08/27/2010 TIME: 14:07:00.91

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S ZO = 321. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	* (FT) (DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. EB McM	* 264826.0	298986.0	265320.0	298926.0	* 498.	97. BR	2390.	12.1	15.0	56.0			
2. EB McM	* 265320.0	298926.0	265465.0	298936.0	* 145.	86. BR	2390.	12.1	15.0	56.0			
3. EB McM	* 265465.0	298936.0	265632.0	298995.0	* 177.	71. BR	2390.	12.1	15.0	56.0			
4. EB McM	* 265632.0	298995.0	265738.0	299076.0	* 133.	53. BR	2390.	12.1	15.0	56.0			
5. EB McM TH	* 265738.0	299076.0	265818.0	299184.0	* 134.	37. BR	930.	12.1	15.0	44.0			
6. EB McM TH	* 265818.0	299184.0	265950.0	299333.0	* 199.	42. BR	930.	12.1	15.0	44.0			
7. EB McM TH	* 265928.0	299309.0	265872.4	299245.5	* 84.	221. BR	216.	100.0	15.0	24.0	.72	4.3	
8. EB McM RT	* 265738.0	299076.0	265889.0	299231.0	* 216.	44. BR	1460.	12.1	15.0	44.0			
9. EB McM RT	* 265889.0	299231.0	265954.0	299262.0	* 72.	64. BR	1460.	12.1	15.0	44.0			
10. EB McM RT	* 265954.0	299262.0	266019.0	299236.0	* 70.	112. BR	1460.	12.1	15.0	44.0			
11. EB McM RT	* 266019.0	299236.0	266061.0	299150.0	* 96.	154. BR	1460.	12.1	15.0	44.0			
12. EB McM dep	* 265950.0	299333.0	266013.0	299414.0	* 103.	38. AG	1080.	12.1		.44.0			
13. EB McM dep	* 266013.0	299414.0	266179.0	299586.0	* 239.	44. AG	1080.	12.1		.44.0			
14. EB McM dep	* 266179.0	299586.0	266265.0	299652.0	* 108.	52. AG	1080.	12.1		.44.0			
15. EB McM dep	* 266265.0	299652.0	266419.0	299706.0	* 163.	71. AG	1080.	12.1		.44.0			
16. WB McM aprch	* 266393.0	299727.0	266254.0	299670.0	* 150.	248. AG	300.	12.1		.44.0			
17. WB McM aprch	* 266254.0	299670.0	266166.0	299603.0	* 111.	233. AG	300.	12.1		.44.0			
18. WB McM aprch	* 266166.0	299603.0	265955.0	299385.0	* 303.	224. BR	300.	12.1	15.0	44.0			
19. WB McM TH	* 265993.0	299424.0	266011.8	299443.5	* 27.	44. BR	216.	100.0	15.0	24.0	.23	1.4	
20. WB McM depart	* 265955.0	299385.0	265793.0	299222.0	* 230.	225. BR	500.	12.1	15.0	44.0			
21. WB McM depart	* 265793.0	299222.0	265665.0	299086.0	* 187.	223. BR	500.	12.1	15.0	56.0			
22. WB McM depart	* 265665.0	299086.0	265558.0	299020.0	* 126.	238. BR	500.	12.1	15.0	56.0			
23. WB McM depart	* 265558.0	299020.0	265431.0	298984.0	* 132.	254. BR	500.	12.1	15.0	56.0			
24. WB McM depart	* 265431.0	298984.0	265282.0	298980.0	* 149.	268. BR	500.	12.1	15.0	56.0			
25. WB McM depart	* 265282.0	298980.0	264828.0	299042.0	* 458.	278. BR	500.	12.1	15.0	56.0			
26. WB Conn ap	* 266061.0	299150.0	266083.0	299066.0	* 87.	165. AG	1460.	12.1		.56.0			
27. WB Conn ap	* 266083.0	299066.0	266082.0	298968.0	* 98.	181. AG	1460.	12.1		.56.0			
28. WB Conn ap	* 266082.0	298968.0	266046.0	298872.0	* 103.	201. AG	1460.	12.1		.56.0			

29. WB	Conn ap	* 266046.0	298872.0	265993.0	298803.0	*	87.	218. AG	1460.	12.1	.0	56.0			
30. WB	Conn ap	* 265993.0	298803.0	265875.0	298712.0	*	149.	232. AG	1460.	12.1	.0	56.0			
31. WB	Conn ap	* 265916.0	298744.0	265972.8	298787.8	*	72.	52. AG	265.	100.0	.0	36.0	.67	3.6	
32. NB	Cen ap	* 266302.0	298032.0	266154.0	298263.0	*	274.	327. AG	530.	12.1	.0	56.0			
33. NB	Cen ap	* 266154.0	298263.0	265990.0	298522.0	*	307.	328. AG	530.	12.1	.0	68.0			
34. NB	Cen ap	* 265990.0	298522.0	265910.0	298684.0	*	181.	334. AG	530.	12.1	.0	68.0			
35. NB	Cen ap	* 265918.0	298668.0	265930.4	298642.7	*	28.	154. AG	511.	100.0	.0	48.0	.33	1.4	
36. NB	Cen depart*	265910.0	298684.0	265863.0	298827.0	*	151.	342. AG	390.	12.1	.0	56.0			
37. NB	Cen depart*	265863.0	298827.0	265839.0	298979.0	*	154.	351. AG	390.	12.1	.0	56.0			
38. NB	Cen depart*	265839.0	298979.0	265832.0	299119.0	*	140.	357. AG	390.	12.1	.0	56.0			
39. NB	Cen depart*	265832.0	299119.0	265857.0	299590.0	*	472.	3. AG	390.	12.1	.0	56.0			
40. NB	Cen depart*	265857.0	299590.0	265854.0	299736.0	*	146.	359. AG	390.	12.1	.0	56.0			
41. NB	Cen depart*	265854.0	299736.0	265839.0	299907.0	*	172.	355. AG	390.	12.1	.0	56.0			
42. SB	Cen ap	* 265813.0	299907.0	265830.0	299690.0	*	218.	176. AG	640.	12.1	.0	44.0			
43. SB	Cen ap	* 265830.0	299690.0	265832.0	299574.0	*	116.	179. AG	640.	12.1	.0	44.0			
44. SB	Cen ap	* 265832.0	299574.0	265822.0	299461.0	*	113.	185. AG	640.	12.1	.0	44.0			

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JOB: Central & McMillan Alt E AM RUN: Central & McMillan Alt E AM
 DATE: 08/27/2010 TIME: 14:07:00.91

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	X2	Y2	* (FT)	(DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
45. SB	Cen ap	* 265822.0	299461.0	265786.0	299087.0	*	376.	186. AG	640.	12.1	.0	44.0			
46. SB	Cen ap	* 265786.0	299087.0	265808.0	298897.0	*	191.	173. AG	640.	12.1	.0	44.0			
47. SB	Cen ap	* 265808.0	298897.0	265855.0	298729.0	*	174.	164. AG	640.	12.1	.0	56.0			
48. SB	Cen ap	* 265846.0	298759.0	265833.8	298802.8	*	45.	344. AG	383.	100.0	.0	36.0	.54	2.3	
49. SB	Cen depart*	265855.0	298729.0	265878.0	298636.0	*	96.	166. AG	1890.	12.1	.0	44.0			
50. SB	Cen depart*	265878.0	298636.0	265930.0	298525.0	*	123.	155. AG	1890.	12.1	.0	44.0			
51. SB	Cen depart*	265930.0	298525.0	266171.0	298181.0	*	420.	145. AG	1890.	12.1	.0	44.0			
52. SB	Cen depart*	266171.0	298181.0	266281.0	298020.0	*	195.	146. AG	1890.	12.1	.0	44.0			
53. NB	Conn dep	* 265886.0	298692.0	265989.0	298763.0	*	125.	55. AG	350.	12.1	.0	44.0			
54. NB	Conn dep	* 265989.0	298763.0	266061.0	298843.0	*	108.	42. AG	350.	12.1	.0	44.0			
55. NB	Conn dep	* 266061.0	298843.0	266101.0	298938.0	*	103.	23. AG	350.	12.1	.0	44.0			
56. NB	Conn dep	* 266101.0	298938.0	266114.0	299035.0	*	98.	8. AG	350.	12.1	.0	44.0			
57. NB	Conn dep	* 266114.0	299035.0	266099.0	299124.0	*	90.	350. AG	350.	12.1	.0	44.0			
58. NB	Conn dep	* 266099.0	299124.0	266074.0	299186.0	*	67.	338. AG	350.	12.1	.0	44.0			
59. NB	Conn dep	* 266074.0	299186.0	265986.0	299361.0	*	196.	333. BR	350.	12.1	15.0	44.0			
60. NB	Conn dep	* 266000.0	299333.0	266009.4	299314.3	*	21.	153. BR	324.	100.0	15.0	36.0	.19	1.1	
61. NB	I-75	* 265327.0	298041.0	265368.0	298889.0	*	849.	3. AG	5070.	12.9	.0	80.0			
62. NB	I-75	* 265368.0	298889.0	265421.0	299301.0	*	415.	7. AG	5070.	12.9	.0	80.0			
63. NB	I-75	* 265421.0	299301.0	265572.0	299874.0	*	593.	15. AG	5070.	12.9	.0	80.0			
64. SB	I-75	* 265463.0	299836.0	265358.0	299399.0	*	449.	194. AG	7870.	12.9	.0	80.0			
65. SB	I-75	* 265358.0	299399.0	265280.0	298741.0	*	663.	187. AG	7870.	12.9	.0	80.0			
66. SB	I-75	* 265280.0	298741.0	265243.0	298097.0	*	645.	183. AG	7870.	12.9	.0	80.0			

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JOB: Central & McMillan Alt E AM RUN: Central & McMillan Alt E AM
 DATE: 08/27/2010 TIME: 14:07:00.91

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE (SEC)	RED TIME (SEC)	CLEARANCE (VPH)	APPROACH (VPH)	SATURATION VOL (VPH)	IDLE RATE (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
7. EB	McM TH	* 60	33	2.0	930	1691	73.30	1 3
19. WB	McM TH	* 60	33	2.0	300	1691	73.30	1 3
31. WB	Conn ap	* 60	27	2.0	1460	1506	73.30	1 3
35. NB	Cen ap	* 60	39	2.0	530	1399	73.30	1 3
48. SB	Cen ap	* 60	39	2.0	640	1403	73.30	1 3
60. NB	Conn dep	* 60	33	2.0	350	1630	73.30	1 3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z
1. SE MID S	* 266089.0	298420.0	5.0 *
2. SE 164 S	* 266017.0	298537.0	5.0 *
3. SE 82 S	* 265980.0	298608.0	5.0 *
4. SE CNR	* 265952.0	298689.0	5.0 *
5. SE 82 E	* 266009.0	298754.0	5.0 *
6. SE 164 E	* 266067.0	298814.0	5.0 *
7. SE MID E	* 266130.0	298970.0	5.0 *
8. SE 164 S	* 266081.0	299220.0	5.0 *
9. SE 82 S	* 266044.0	299294.0	5.0 *
10. SE CNR	* 266014.0	299370.0	5.0 *
11. SE 82 E	* 266072.0	299443.0	5.0 *
12. SE 164 E	* 266129.0	299503.0	5.0 *
13. SE MID E	* 266236.0	299603.0	5.0 *
14. NE MID E	* 266197.0	299656.0	5.0 *
15. NE 164 E	* 266064.0	299530.0	5.0 *
16. NE 82 E	* 266006.0	299471.0	5.0 *
17. NE CNR	* 265950.0	299412.0	5.0 *
18. NE CNR	* 265869.0	299339.0	5.0 *
19. NE 82 N	* 265872.0	299412.0	5.0 *
20. NE 164 N	* 265876.0	299494.0	5.0 *
21. NE MID N	* 265881.0	299614.0	5.0 *

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JOB: Central & McMillan Alt E AM RUN: Central & McMillan Alt E AM

MODEL RESULTS

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21
-----*

0. * .2
5. * .1
10. * .1
15. * .1
20. * .1
25. * .0
30. * .0
35. * .0
40. * .0
45. * .0
50. * .0
55. * .0
60. * .0
65. * .0
70. * .0
75. * .0
80. * .0
85. * .0
90. * .0
95. * .1
100. * .1
105. * .1
110. * .1
115. * .1
120. * .1
125. * .1
130. * .1
135. * .1
140. * .1
145. * .1
150. * .1
155. * .1
160. * .1
165. * .1
170. * .2
175. * .3
180. * .6
185. * .7
190. * .8
195. * .8
200. * 1.0
205. * 1.1

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21
-----*

210. * 1.2
215. * 1.3
220. * 1.5
225. * 1.6
230. * 1.4
235. * 1.5
240. * 1.5
245. * 1.3
250. * 1.1
255. * 1.2
260. * 1.3
265. * 1.3
270. * 1.3
275. * 1.3
280. * 1.3
285. * 1.3
290. * 1.2
295. * 1.1
300. * .9
305. * .9
310. * .7
315. * .8
320. * .5
325. * .5
330. * .4
335. * .4
340. * .4

62. NB	I-75	* 265368.0	298889.0	265421.0	299301.0	*	415.	7. AG	7923.	12.9	.0	80.0
63. NB	I-75	* 265421.0	299301.0	265572.0	299874.0	*	593.	15. AG	7923.	12.9	.0	80.0
64. SB	I-75	* 265463.0	299836.0	265358.0	299399.0	*	449.	194. AG	5980.	12.9	.0	80.0
65. SB	I-75	* 265358.0	299399.0	265280.0	298741.0	*	663.	187. AG	5980.	12.9	.0	80.0
66. SB	I-75	* 265280.0	298741.0	265243.0	298097.0	*	645.	183. AG	5980.	12.9	.0	80.0

JOB: Central & McMillan Alt E PM RUN: Central & McMillan Alt E PM
 DATE: 08/27/2010 TIME: 14:19:21.36

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (gm/hr)	IDLE EM FAC	SIGNAL TYPE	ARRIVAL RATE
7. EB McM TH	* 60	37	2.0	390	1691	73.30	1 3	
19. WB McM TH	* 60	37	2.0	890	1691	73.30	1 3	
31. WB Conn ap	* 60	34	2.0	740	1673	73.30	1 3	
35. NB Cen ap	* 60	32	2.0	2100	1555	73.30	1 3	
48. SB Cen ap	* 60	32	2.0	780	1299	73.30	1 3	
60. NB Conn dep	* 60	29	2.0	1290	1677	73.30	1 3	

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	* *
1. SE MID S	* 266089.0	298420.0	5.0	*
2. SE 164 S	* 266017.0	298537.0	5.0	*
3. SE 82 S	* 265980.0	298608.0	5.0	*
4. SE CNR	* 265952.0	298689.0	5.0	*
5. SE 82 E	* 266009.0	298754.0	5.0	*
6. SE 164 E	* 266067.0	298814.0	5.0	*
7. SE MID E	* 266130.0	298970.0	5.0	*
8. SE 164 S	* 266081.0	299220.0	5.0	*
9. SE 82 S	* 266044.0	299294.0	5.0	*
10. SE CNR	* 266014.0	299370.0	5.0	*
11. SE 82 E	* 266072.0	299443.0	5.0	*
12. SE 164 E	* 266129.0	299503.0	5.0	*
13. SE MID E	* 266236.0	299603.0	5.0	*
14. NE MID E	* 266197.0	299656.0	5.0	*
15. NE 164 E	* 266064.0	299530.0	5.0	*
16. NE 82 E	* 266006.0	299471.0	5.0	*
17. NE CNR	* 265950.0	299412.0	5.0	*
18. NE CNR	* 265869.0	299339.0	5.0	*
19. NE 82 N	* 265872.0	299412.0	5.0	*
20. NE 164 N	* 265876.0	299494.0	5.0	*
21. NE MID N	* 265881.0	299614.0	5.0	*

JOB: Central & McMillan Alt E PM RUN: Central & McMillan Alt E PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .2	.3	.7	1.0	.8	1.3	.7	.3	.4	.7	.6	.4	.4	.0	.0	.0	.0	.7	.7	.8
5.	* .1	.3	.7	.9	1.1	1.0	.5	.2	.3	.7	.5	.4	.5	.0	.0	.0	.0	.5	.5	.5
10.	* .1	.2	.4	1.0	1.1	1.1	.3	.1	.3	.7	.6	.5	.5	.0	.0	.0	.0	.4	.4	.4
15.	* .1	.1	.4	.8	1.2	.9	.3	.0	.3	.7	.6	.5	.5	.0	.0	.0	.0	.3	.3	.3
20.	* .1	.1	.4	.9	1.1	.8	.1	.0	.2	.8	.5	.4	.5	.0	.0	.0	.1	.2	.2	.2
25.	* .1	.1	.4	.9	1.1	.8	.1	.0	.2	.7	.5	.4	.6	.0	.1	.1	.2	.1	.1	.1
30.	* .1	.1	.2	.8	1.1	.5	.1	.0	.0	.7	.6	.5	.6	.1	.1	.1	.2	.3	.1	.1
35.	* .1	.1	.1	.7	.9	.3	.1	.0	.0	.5	.5	.6	.6	.1	.1	.3	.4	.4	.1	.1
40.	* .1	.1	.1	.5	.7	.3	.0	.0	.0	.3	.4	.5	.5	.1	.3	.3	.5	.5	.1	.1
45.	* .0	.0	.1	.4	.5	.2	.0	.0	.0	.2	.3	.5	.4	.2	.3	.5	.7	.6	.2	.1
50.	* .0	.0	.0	.2	.4	.1	.0	.0	.0	.1	.2	.4	.4	.3	.4	.7	.8	.8	.3	.1
55.	* .0	.0	.0	.1	.3	.0	.0	.0	.0	.1	.2	.3	.3	.6	.8	.9	.8	.3	.1	.1
60.	* .0	.0	.0	.1	.2	.0	.0	.0	.0	.1	.1	.3	.4	.6	.7	.9	.9	.3	.0	.0
65.	* .0	.0	.0	.0	.1	.0	.0	.0	.0	.1	.1	.3	.6	.5	.8	.9	.8	.5	.1	.1
70.	* .0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.6	.5	.9	.8	.9	.5	.1	.1	.1
75.	* .1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.6	.4	1.0	.7	.8	.5	.2	.2	.2
80.	* .1	.1	.0	.0	.1	.0	.0	.0	.0	.0	.0	.7	.4	1.0	.8	.9	.5	.2	.2	.2
85.	* .1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.7	.3	1.0	.7	.8	.4	.3	.3	.3
90.	* .1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.7	.3	.9	.5	.8	.3	.3	.3	.3
95.	* .1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.0	.7	.3	.8	.4	.8	.4	.4	.4	.4
100.	* .1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.7	.3	.8	.4	1.0	.5	.4	.4	.4
105.	* .1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.7	.3	.7	.3	1.0	.6	.4	.4	.4
110.	* .1	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.5	.3	.7	.3	1.0	.6	.3	.3	.3
115.	* .2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.4	.3	.7	.4	.9	.6	.2	.2	.2
120.	* .2	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.4	.3	.7	.5	1.1	.7	.2	.2	.2
125.	* .3	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.4	.3	.7	.5	1.0	.7	.3	.3	.3
130.	* .5	.4	.3	.1	.0	.0	.0	.1	.0	.0	.0	.4	.3	.7	.6	.9	.6	.5	.5	.5
135.	* .6	.6	.6	.2	.0	.0	.1	.1	.1	.0	.0	.5	.3	.7	.6	1.1	.7	.5	.5	.5
140.	* .8	.9	.8	.5	.0	.0	.1	.1	.2	.0	.0	.5	.3	.7	.7	.9	.6	.5	.5	.5
145.	* 1.2	1.1	1.1	.8	.0	.0	.2	.3	.2	.0	.0	.5	.4	.7	.8	.9	.7	.5	.5	.5

150. * 1.4 1.4 1.4 1.1 .2 .0 .0 .3 .4 .4 .0 .0 .0 .5 .4 .8 .8 .9 .7 .5
 155. * 1.4 1.5 1.7 1.3 .2 .0 .0 .4 .5 .6 .0 .0 .0 .4 .4 .9 .8 .8 .6 .5
 160. * 1.6 1.5 1.8 1.7 .4 .2 .0 .7 .6 .7 .0 .0 .0 .4 .5 .9 .9 .8 .7 .6
 165. * 1.5 1.5 2.0 2.0 .4 .2 .0 .8 .8 .9 .0 .0 .0 .4 .5 1.0 .7 1.0 .8 .4
 170. * 1.6 1.6 1.9 2.0 .5 .3 .2 .9 .9 .9 .1 .0 .0 .4 .7 1.1 .8 1.0 .9 .6
 175. * 1.4 1.4 2.1 2.2 .5 .4 .4 .9 1.0 .9 .1 .0 .0 .5 .7 1.1 .7 1.0 1.0 .7
 180. * 1.4 1.4 2.0 2.2 .6 .3 .4 .9 .9 1.0 .2 .0 .0 .5 .9 1.1 .8 1.2 1.2 .9
 185. * 1.3 1.3 2.1 2.2 .7 .5 .5 1.0 .6 .9 .2 .1 .0 .6 1.0 1.2 .9 1.5 1.2 1.2
 190. * 1.2 1.3 2.1 2.2 .8 .5 .7 .9 .6 .9 .3 .1 .0 .7 1.1 1.0 1.0 1.7 1.4 1.3
 195. * 1.2 1.2 2.1 2.2 .9 .5 .9 1.0 .5 1.0 .4 .2 .0 .7 1.3 1.2 1.1 1.9 1.6 1.4
 200. * 1.2 1.2 2.1 2.1 1.1 .7 1.2 .7 .8 .9 .5 .4 .1 .9 1.4 1.5 1.5 2.0 1.8 1.4
 205. * 1.1 1.1 2.1 2.1 .9 .8 1.0 .7 1.0 1.0 .7 .6 .3 1.2 1.6 1.6 1.7 2.2 1.8 1.8

1

JOB: Central & McMillan Alt E PM

RUN: Central & McMillan Alt E PM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18

REC19 REC20

-----*-----
 210. * 1.1 1.1 2.0 2.0 1.0 .9 1.3 .8 1.1 1.3 .9 .8 .4 1.2 1.9 1.7 2.1 2.5 2.1 1.9
 215. * 1.1 1.0 2.3 2.0 1.1 1.0 1.4 .8 1.1 1.9 1.2 .9 .9 1.4 2.0 1.9 2.2 2.7 2.0 1.8
 220. * 1.1 1.2 2.4 2.2 1.4 1.2 1.9 1.0 1.3 2.1 1.5 1.6 1.2 1.5 1.9 1.7 2.1 2.5 2.1 2.0
 225. * 1.1 1.2 2.6 2.2 1.6 1.8 2.0 .9 1.5 1.9 1.6 1.7 1.1 1.5 1.8 1.6 2.0 2.4 2.0 1.8
 230. * 1.2 1.4 2.6 2.2 1.7 1.8 1.6 1.1 1.6 2.1 1.7 1.7 1.5 1.5 1.7 1.6 1.8 2.3 1.7 1.9
 235. * 1.2 1.4 2.8 2.1 2.0 1.9 1.4 1.1 1.9 2.2 2.0 1.8 1.3 1.4 1.4 1.5 1.6 2.2 1.7 1.8
 240. * 1.4 1.5 3.0 2.2 1.9 2.1 1.4 1.2 2.2 2.2 1.8 2.1 1.4 .9 1.4 1.4 1.5 1.9 1.8 1.7
 245. * 1.4 1.6 3.1 2.3 2.0 2.2 1.5 1.2 2.2 2.3 2.0 1.9 1.4 1.0 1.2 1.1 1.3 1.7 1.6 1.7
 250. * 1.5 1.7 3.1 2.1 2.1 2.2 1.5 1.5 2.3 2.1 1.9 1.8 1.5 .9 .8 1.1 1.4 1.7 1.7 1.7
 255. * 1.6 1.8 3.1 1.9 2.1 2.0 1.6 1.5 2.4 1.8 1.9 1.7 1.4 .9 .9 1.1 1.1 1.7 1.6 1.8
 260. * 1.7 1.8 3.0 1.8 2.4 2.0 1.4 1.6 2.3 1.8 1.8 1.5 1.3 .7 1.0 1.1 1.2 1.5 1.6 1.7
 265. * 1.8 1.7 2.9 1.9 2.4 1.8 1.6 1.7 2.1 1.7 1.7 1.6 1.3 .6 .9 1.0 1.2 1.6 1.6 1.6
 270. * 1.8 1.9 3.1 1.8 2.5 2.0 1.5 1.7 2.1 1.5 1.6 1.4 1.1 .6 1.0 .9 1.3 1.6 1.6 1.6
 275. * 1.8 1.9 3.1 2.0 2.4 2.0 1.5 1.6 2.3 1.6 1.5 1.4 1.1 .6 .9 1.1 1.2 1.6 1.6 1.6
 280. * 1.8 1.9 3.2 1.9 2.4 1.8 1.6 1.9 2.2 1.5 1.7 1.3 1.0 .5 .9 1.0 1.2 1.6 1.6 1.6
 285. * 1.9 2.2 3.4 2.2 2.3 1.6 1.5 1.6 2.2 1.5 1.7 1.2 .9 .4 .9 1.0 1.1 1.6 1.6 1.6
 290. * 1.9 2.3 3.4 2.2 2.1 1.4 1.6 1.9 2.1 1.5 1.6 1.1 .7 .3 .7 1.0 1.1 1.6 1.6 1.6
 295. * 2.2 2.6 3.4 2.1 2.3 1.5 1.5 1.9 1.9 1.3 1.5 1.0 .8 .1 .7 1.0 1.1 1.6 1.6 1.6
 300. * 2.2 2.7 3.6 2.1 2.0 1.5 1.4 1.7 2.1 1.3 1.5 .9 .6 .1 .5 .7 1.1 1.6 1.6 1.5
 305. * 2.2 2.8 3.3 2.2 2.1 1.6 1.7 1.6 1.9 1.1 1.3 .8 .6 .0 .4 .8 1.1 1.6 1.5 1.5
 310. * 2.1 2.8 3.5 2.2 1.9 1.4 1.6 1.6 1.9 1.1 1.3 .5 .5 .0 .3 .7 1.0 1.5 1.5 1.3
 315. * 2.3 2.8 3.4 2.2 1.8 1.7 1.4 1.5 1.5 .9 1.2 .5 .5 .0 .2 .5 .8 1.5 1.3 1.2
 320. * 2.2 2.9 3.3 2.3 1.8 1.6 1.6 1.4 1.5 .9 1.0 .4 .5 .0 .2 .3 .7 1.4 1.4 1.2
 325. * 2.0 2.6 3.2 2.4 1.6 1.7 1.5 1.2 1.3 .8 .9 .4 .5 .0 .1 .2 .5 1.3 1.2 1.1
 330. * 1.7 2.7 3.2 2.4 1.5 1.5 1.1 1.0 .8 .7 .4 .5 .0 .0 .2 .4 1.2 1.1 1.0
 335. * 1.5 2.2 2.5 2.1 1.4 1.3 1.5 .8 .8 .6 .7 .4 .5 .0 .0 .2 .3 1.1 .9 .9
 340. * .9 1.7 2.0 1.8 1.2 1.3 1.4 .7 .6 .6 .7 .4 .5 .0 .0 .0 .2 1.0 .9 .9
 345. * .7 1.3 1.6 1.8 1.0 1.1 1.1 .5 .4 .5 .7 .4 .5 .0 .0 .1 .9 .9 .9
 350. * .5 .8 1.3 1.5 1.1 1.0 1.0 .4 .4 .7 .7 .4 .4 .0 .0 .1 .9 .9 .9
 355. * .2 .6 .8 1.3 1.0 1.2 .9 .3 .5 .7 .6 .4 .4 .0 .0 .0 .7 .9 .9
 360. * .2 .3 .7 1.0 .8 1.3 .7 .3 .4 .7 .6 .4 .4 .0 .0 .0 .7 .7 .8

MAX * 2.3 2.9 3.6 2.4 2.5 2.2 2.0 1.9 2.4 2.3 2.0 2.1 1.5 1.5 2.0 1.9 2.2 2.7 2.1 2.0
 DEGR * 315 320 300 325 270 245 225 280 255 245 240 230 225 215 215 215 210 220

1

JOB: Central & McMillan Alt E PM

RUN: Central & McMillan Alt E PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to
 the maximum concentration, only the first
 angle, of the angles with same maximum
 concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21

-----*-----
 0. * .6
 5. * .4
 10. * .3
 15. * .2
 20. * .1
 25. * .1
 30. * .1
 35. * .1
 40. * .1
 45. * .1
 50. * .1
 55. * .0
 60. * .0
 65. * .0
 70. * .0
 75. * .0
 80. * .0
 85. * .0
 90. * .0
 95. * .1
 100. * .1
 105. * .1
 110. * .1
 115. * .2

120. * .2
 125. * .2
 130. * .2
 135. * .2
 140. * .2
 145. * .3
 150. * .3
 155. * .6
 160. * .5
 165. * .5
 170. * .4
 175. * .7
 180. * .9
 185. * 1.3
 190. * 1.3
 195. * 1.4
 200. * 1.6
 205. * 1.8
 1

JOB: Central & McMillan Alt E PM

RUN: Central & McMillan Alt E PM

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
 ANGLE * (PPM)
 (DEGR)* REC21

-----*-----
 210. * 1.9
 215. * 1.9
 220. * 1.9
 225. * 1.9
 230. * 2.0
 235. * 1.9
 240. * 1.9
 245. * 1.7
 250. * 1.8
 255. * 1.6
 260. * 1.8
 265. * 1.6
 270. * 1.6
 275. * 1.7
 280. * 1.7
 285. * 1.7
 290. * 1.5
 295. * 1.5
 300. * 1.3
 305. * 1.1
 310. * 1.0
 315. * .9
 320. * 1.0
 325. * .8
 330. * .8
 335. * .8
 340. * .9
 345. * .7
 350. * .6
 355. * .6
 360. * .6
 -----*-----
 MAX * 2.0
 DEGR. * 230

THE HIGHEST CONCENTRATION IS 3.60 PPM AT 300 DEGREES FROM REC3 .
 THE 2ND HIGHEST CONCENTRATION IS 2.90 PPM AT 320 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS 2.70 PPM AT 215 DEGREES FROM REC18.

JOB: Central & McMillan Alt I AM

RUN: Central & McMillan Alt I AM

DATE: 08/27/2010 TIME: 11:43:39.24

SITE & METEOROLOGICAL VARIABLES

-----*-----
 VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	* X2	Y2	(FT) (DEG)	* LENGTH BRG TYPE	VPH	EF	H	W	V/C	QUEUE
							(G/MI) (FT) (FT)	(VEH)					
1. NB	Cen aprch	* 266300.0	298030.0	265981.0	298520.0	*	585. 327. AG	400. 12.1	.0	56.0			
2. NB	Cen aprch	* 265981.0	298520.0	265930.0	298621.0	*	113. 333. AG	400. 12.1	.0	56.0			
3. NB	Cen th+rt	* 265930.0	298621.0	265887.0	298770.0	*	155. 344. AG	250. 12.1	.0	44.0			
4. NB	Cen thru	* 265887.0	298770.0	265848.0	298926.0	*	161. 346. AG	240. 12.1	.0	44.0			
5. NB	Cen thru	* 265860.0	298880.0	265863.8	298864.7	*	16. 166. AG	145. 100.0	.0	24.0	.12	.8	
6. NB	Cen right	* 265896.0	298777.0	265889.0	298867.0	*	90. 356. AG	10. 12.1	.0	32.0			
7. NB	Cen right	* 265890.0	298859.0	265890.1	298857.7	*	1. 176. AG	73. 100.0	.0	12.0	.01	.1	
8. NB	Cen right	* 265889.0	298867.0	265913.0	298986.0	*	121. 11. AG	10. 12.1	.0	32.0			
9. NB	Cen left	* 265930.0	298621.0	265871.0	298749.0	*	141. 335. AG	150. 12.1	.0	44.0			
10. NB	Cen left	* 265871.0	298749.0	265834.0	298915.0	*	170. 347. AG	150. 12.1	.0	44.0			
11. NB	Cen left	* 265843.0	298876.0	265845.1	298866.4	*	10. 168. AG	145. 100.0	.0	24.0	.19	.5	
12. NB	Cen depart	* 265848.0	298926.0	265835.0	299123.0	*	197. 356. AG	450. 12.1	.0	56.0			
13. NB	Cen depart	* 265835.0	299123.0	265854.0	299553.0	*	430. 3. AG	450. 12.1	.0	56.0			
14. NB	Cen depart	* 265854.0	299553.0	265853.0	299734.0	*	181. 360. AG	450. 12.1	.0	56.0			
15. NB	Cen depart	* 265853.0	299734.0	265840.0	299908.0	*	174. 356. AG	450. 12.1	.0	56.0			

17. SB	Cen aprch	* 265829.0	299697.0	265831.0	299539.0	*	158.	179. AG	720.	12.1	.0	44.0	
18. SB	Cen aprch	* 265831.0	299539.0	265800.0	299112.0	*	428.	184. AG	720.	12.1	.0	44.0	
19. SB	Cen aprch	* 265800.0	299112.0	265807.0	298918.0	*	194.	178. AG	720.	12.1	.0	56.0	
20. SB	Cen aprch	* 265805.0	298976.0	265803.9	299007.5	*	31.	358. AG	218.	100.0	.0	36.0	.26 1.6
21. SB	Cen depart	* 265807.0	298918.0	265870.0	298694.0	*	233.	164. AG	1320.	12.1	.0	44.0	
22. SB	Cen depart	* 265870.0	298694.0	265929.0	298554.0	*	152.	157. AG	1320.	12.1	.0	44.0	
23. SB	Cen depart	* 265929.0	298554.0	266278.0	298019.0	*	639.	147. AG	1320.	12.1	.0	44.0	
24. EB	McM aprch	* 264648.0	299034.0	265403.0	298932.0	*	762.	98. BR	1540.	12.1	15.0	44.0	
25. EB	McM thru+I	* 265403.0	298932.0	265612.0	298913.0	*	210.	95. BR	910.	12.1	15.0	44.0	
26. EB	McM thru+I	* 265612.0	298913.0	265821.0	298881.0	*	211.	99. AG	910.	12.1	.0	44.0	
27. EB	McM thr+I	* 265773.0	298888.0	265689.4	298900.9	*	85.	279. AG	206.	100.0	.0	24.0	.66 4.3
28. EB	McM right	* 265403.0	298932.0	265757.0	298877.0	*	358.	99. AG	630.	12.1	.0	32.0	
29. EB	McM right	* 265751.0	298878.0	265474.7	298920.9	*	280.	279. AG	103.	100.0	.0	12.0	1.01 14.2
30. EB	McM right	* 265757.0	298877.0	265798.0	298862.0	*	44.	110. AG	630.	12.1	.0	32.0	
31. EB	McM right	* 265798.0	298862.0	265827.0	298834.0	*	40.	134. AG	630.	12.1	.0	32.0	
32. EB	McM depart	* 265821.0	298884.0	265876.0	298929.0	*	71.	51. AG	710.	12.1	.0	44.0	
33. EB	McM depart	* 265876.0	298929.0	265913.0	298986.0	*	68.	33. AG	710.	12.1	.0	44.0	
34. EB	McM depart	* 265912.0	298988.0	265938.0	299116.0	*	131.	11. AG	720.	12.1	.0	44.0	
35. EB	McM depart	* 265938.0	299116.0	265975.0	299226.0	*	116.	19. AG	720.	12.1	.0	44.0	
36. EB	McM depart	* 265975.0	299226.0	266163.0	299539.0	*	365.	31. AG	720.	12.1	.0	44.0	
37. EB	McM depart	* 266163.0	299539.0	266220.0	299610.0	*	91.	39. AG	720.	12.1	.0	44.0	
38. EB	McM depart	* 266220.0	299610.0	266293.0	299664.0	*	91.	54. AG	720.	12.1	.0	44.0	
39. EB	McM depart	* 266293.0	299664.0	266414.0	299711.0	*	130.	69. AG	720.	12.1	.0	44.0	
40. WB	McM aprch	* 266380.0	299736.0	266244.0	299666.0	*	153.	243. AG	200.	12.1	.0	44.0	
41. WB	McM aprch	* 266244.0	299666.0	266173.0	299596.0	*	100.	225. AG	200.	12.1	.0	44.0	
42. WB	McM aprch	* 266173.0	299596.0	265969.0	299259.0	*	394.	211. AG	200.	12.1	.0	44.0	
43. WB	McM aprch	* 265969.0	299259.0	265933.0	299173.0	*	93.	203. AG	200.	12.1	.0	44.0	
44. WB	McM aprch	* 265933.0	299173.0	265909.0	299091.0	*	85.	196. AG	200.	12.1	.0	44.0	

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JOB: Central & McMillan Alt I AM RUN: Central & McMillan Alt I AM
 DATE: 08/27/2010 TIME: 11:43:39.24

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	X2	Y2	* (FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
45. WB	McM aprch	* 265909.0	299091.0	265892.0	299010.0	*	83.	192. AG	200.	12.1	.0	44.0			
46. WB	McM aprch	* 265892.0	299010.0	265856.0	298942.0	*	77.	208. AG	200.	12.1	.0	44.0			
47. WB	McM aprch	* 265892.0	299011.0	265880.1	298988.2	*	26.	208. AG	284.	100.0	.0	24.0	.28 1.3		
48. WB	McM depart	* 265856.0	298942.0	265752.0	298914.0	*	108.	255. AG	370.	12.1	.0	44.0			
49. WB	McM depart	* 265752.0	298914.0	264661.0	299060.0	*	1101.	278. BR	370.	12.1	15.0	44.0			
50. NB	I-75	* 265324.0	298040.0	265380.0	298899.0	*	861.	4. AG	5840.	12.9	.0	80.0			
51. NB	I-75	* 265380.0	298899.0	265402.0	299143.0	*	245.	5. AG	5840.	12.9	.0	80.0			
52. NB	I-75	* 265402.0	299143.0	265454.0	299420.0	*	282.	11. AG	5840.	12.9	.0	80.0			
53. NB	I-75	* 265454.0	299420.0	265576.0	299875.0	*	471.	15. AG	5840.	12.9	.0	80.0			
54. SB	I-75	* 265474.0	299844.0	265416.0	299648.0	*	204.	196. AG	8750.	12.9	.0	80.0			
55. SB	I-75	* 265416.0	299648.0	265345.0	299344.0	*	312.	193. AG	8750.	12.9	.0	80.0			
56. SB	I-75	* 265345.0	299344.0	265316.0	299152.0	*	194.	189. AG	8750.	12.9	.0	80.0			
57. SB	I-75	* 265316.0	299152.0	265292.0	298925.0	*	228.	186. AG	8750.	12.9	.0	80.0			
58. SB	I-75	* 265292.0	298925.0	265238.0	298100.0	*	827.	184. AG	8750.	12.9	.0	80.0			

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JOB: Central & McMillan Alt I AM RUN: Central & McMillan Alt I AM
 DATE: 08/27/2010 TIME: 11:43:39.24

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH (SEC)	TIME (SEC)	LOST TIME (SEC)	VOL (VPH)	FLOW RATE (VPH)	EM (gm/hr)	FAC	TYPE	RATE
5. NB	Cen thru	* 65	24	2.0	240	1691	73.30	1 3
7. NB	Cen right	* 65	24	2.0	10	1509	73.30	1 3
11. NB	Cen left	* 65	24	2.0	150	685	73.30	1 3
20. SB	Cen aprch	* 65	24	2.0	720	1630	73.30	1 3
27. EB	McM thr+I	* 65	34	2.0	910	1650	73.30	1 3
29. EB	McM right	* 65	34	2.0	630	1509	73.30	1 3
47. WB	McM aprch	* 65	47	2.0	200	1678	73.30	1 3

RECEPTOR LOCATIONS

RECEPTOR	* X	Y	Z	*
1. SE MID S	* 265957.0	298638.0	5.0	*
2. SE 164 S	* 265938.0	298713.0	5.0	*
3. SE 82 S	* 265912.0	298793.0	5.0	*
4. SE CNR	* 265918.0	298875.0	5.0	*
5. SE 82 E	* 265934.0	298958.0	5.0	*
6. SE 164 E	* 265949.0	299039.0	5.0	*
7. SE MID E	* 265999.0	299214.0	5.0	*
8. NE MID E	* 265976.0	299319.0	5.0	*
9. NE 164 E	* 265908.0	299163.0	5.0	*
10. NE 82 E	* 265886.0	299084.0	5.0	*
11. NE CNR	* 265865.0	298999.0	5.0	*
12. NE 82 N	* 265859.0	299083.0	5.0	*
13. NE 164 N	* 265860.0	299164.0	5.0	*
14. NE MID N	* 265871.0	299350.0	5.0	*

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JOB: Central & McMillan Alt I AM RUN: Central & McMillan Alt I AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to

the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14

0.	* .0	.0	.1	.3	.3	.3	.5	.0	.1	.2	.4	.4	.4	.3
5.	* .0	.0	.1	.2	.3	.4	.5	.0	.0	.1	.3	.3	.3	.2
10.	* .0	.0	.0	.2	.4	.4	.5	.0	.0	.0	.2	.3	.3	.1
15.	* .0	.0	.0	.1	.3	.3	.5	.0	.1	.3	.3	.2	.2	.1
20.	* .0	.0	.0	.1	.2	.3	.5	.0	.2	.3	.5	.3	.1	.1
25.	* .0	.0	.0	.0	.2	.3	.4	.2	.2	.3	.6	.1	.1	.1
30.	* .0	.0	.0	.0	.1	.3	.2	.4	.3	.5	.2	.2	.0	.0
35.	* .0	.0	.0	.0	.0	.0	.2	.2	.4	.4	.7	.2	.1	.0
40.	* .0	.0	.0	.0	.0	.0	.2	.3	.4	.5	.7	.2	.1	.0
45.	* .0	.0	.0	.0	.0	.1	.3	.4	.5	.6	.2	.1	.0	.0
50.	* .0	.0	.0	.0	.0	.1	.3	.4	.3	.8	.2	.1	.0	.0
55.	* .0	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.1	.2	.1
60.	* .0	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.2	.2	.1
65.	* .0	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.2	.2	.1
70.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.2	.2	.1
75.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.2	1.0	.2	.1	.1
80.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1
85.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1
90.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1
95.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.1	.1	.1	.1
100.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.2	.1	.1
105.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.3	.1	.1
110.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.3	.1	.1
115.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.3	.1	.1
120.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.3	.2	.1
125.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.8	.2	.2	.1
130.	* .0	.0	.0	.0	.0	.0	.0	.3	.3	.3	.7	.2	.1	.1
135.	* .1	.0	.0	.0	.0	.0	.0	.3	.4	.3	.6	.2	.1	.1
140.	* .2	.1	.0	.0	.0	.0	.0	.3	.3	.3	.5	.3	.1	.0
145.	* .4	.1	.1	.0	.0	.0	.0	.3	.3	.3	.5	.3	.1	.1
150.	* .4	.2	.1	.1	.0	.0	.0	.3	.3	.3	.6	.4	.1	.1
155.	* .5	.3	.1	.1	.1	.0	.0	.3	.3	.5	.6	.5	.1	.1
160.	* .5	.3	.3	.1	.1	.1	.0	.3	.5	.5	.6	.5	.2	.2
165.	* .5	.5	.4	.1	.1	.1	.0	.3	.5	.5	.7	.5	.4	.1
170.	* .5	.4	.3	.2	.1	.1	.1	.4	.4	.6	.7	.6	.6	.1
175.	* .6	.5	.4	.2	.2	.1	.1	.5	.4	.6	.9	.6	.5	.1
180.	* .6	.6	.4	.3	.2	.2	.1	.3	.4	.6	.9	.4	.4	.3
185.	* .5	.5	.5	.3	.3	.3	.1	.3	.4	.5	.8	.5	.4	.4
190.	* .5	.4	.4	.2	.2	.4	.2	.3	.5	.5	.8	.5	.4	.5
195.	* .5	.5	.4	.2	.2	.3	.3	.5	.6	.6	.8	.8	.7	.6
200.	* .4	.4	.5	.3	.2	.5	.6	.4	.6	.6	1.1	1.1	.9	.9
205.	* .4	.4	.5	.5	.4	.6	.6	.5	.7	.9	1.2	1.2	1.1	1.0

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JOB: Central & McMillan Alt I AM

RUN: Central & McMillan Alt I AM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14

210.	* .5	.5	.6	.5	.5	.9	.9	.6	.9	1.1	1.5	1.4	1.2	1.1
215.	* .5	.6	.7	.7	.8	1.1	1.0	.7	1.0	1.1	1.4	1.5	1.4	1.3
220.	* .6	.7	.8	.9	1.0	1.4	1.2	.8	1.1	1.3	1.5	1.6	1.4	1.4
225.	* .7	.8	1.0	1.0	1.1	1.4	1.1	1.1	1.1	1.4	1.7	1.8	1.4	1.4
230.	* .8	1.0	1.1	1.1	1.3	2.0	1.2	1.0	1.1	1.5	2.0	1.7	1.4	1.5
235.	* 1.0	1.0	1.2	1.2	1.5	2.0	1.3	1.1	1.2	1.4	1.9	1.7	1.4	1.5
240.	* 1.2	1.1	1.3	1.2	1.5	1.7	1.0	1.1	1.2	1.3	1.8	1.6	1.4	1.5
245.	* 1.2	1.3	1.3	1.2	1.4	2.0	1.3	1.2	1.3	1.1	2.0	1.6	1.5	1.5
250.	* 1.1	1.3	1.3	1.4	1.7	1.7	1.5	1.1	1.2	1.2	2.2	1.4	1.4	1.5
255.	* 1.2	1.2	1.3	1.3	2.0	1.7	1.5	1.1	1.4	1.3	2.1	1.5	1.5	1.5
260.	* 1.2	1.2	1.3	1.7	2.0	1.6	1.4	1.1	1.1	1.2	1.9	1.4	1.4	1.4
265.	* 1.2	1.2	1.2	1.9	2.0	1.5	1.3	1.1	1.2	1.2	1.8	1.5	1.4	1.5
270.	* 1.2	1.1	1.4	2.1	1.7	1.5	1.2	1.1	1.1	1.2	1.7	1.4	1.4	1.3
275.	* 1.2	1.3	1.4	2.1	1.6	1.5	1.4	1.0	1.2	1.2	1.6	1.4	1.4	1.5
280.	* 1.4	1.4	1.7	2.1	1.5	1.4	1.4	1.0	1.1	1.2	1.6	1.3	1.3	1.3
285.	* 1.5	1.3	1.8	2.1	1.5	1.4	1.4	1.0	1.0	1.2	1.4	1.2	1.4	1.4
290.	* 1.5	1.3	1.8	1.6	1.5	1.4	1.4	1.1	1.1	1.3	1.5	1.4	1.3	1.4
295.	* 1.5	1.3	1.8	1.5	1.4	1.5	1.4	.9	.9	1.1	1.4	1.2	1.4	1.3
300.	* 1.3	1.6	1.7	1.4	1.5	1.3	1.4	1.0	1.2	1.1	1.4	1.3	1.3	1.3
305.	* 1.4	1.5	1.5	1.1	1.4	1.1	1.4	.9	1.1	1.2	1.3	1.3	1.4	1.4
310.	* 1.4	1.5	1.4	1.3	1.5	1.3	1.2	.8	1.0	1.3	1.3	1.4	1.3	1.3
315.	* 1.3	1.5	1.4	1.3	1.6	1.2	1.1	.8	1.0	1.1	1.3	1.4	1.3	1.2
320.	* 1.4	1.4	1.3	1.4	1.4	1.3	1.1	.7	.9	1.2	1.2	1.4	1.2	1.2
325.	* 1.2	1.1	1.4	1.0	1.5	1.2	.7	.5	.8	.9	1.3	1.2	1.2	.9
330.	* 1.0	1.1	1.0	1.1	1.2	1.1	.7	.2	.8	.9	1.2	1.1	1.0	.8
335.	* .8	.8	1.1	.9	1.0	.8	.4	.1	.5	.9	1.0	1.0	1.0	.7
340.	* .6	.6	.8	.9	.9	.8	.4	.0	.5	.5	.9	.7	.8	.5
345.	* .4	.3	.8	.7	.7	.7	.3	.0	.3	.4	.8	.8	.7	.6
350.	* .1	.1	.3	.5	.5	.6	.4	.0	.2	.3	.5	.6	.6	.4
355.	* .0	.1	.1	.4	.2	.3	.4	.0	.2	.2	.5	.6	.5	.4
360.	* .0	.0	.1	.3	.3	.3	.5	.0	.1	.2	.4	.4	.4	.3

MAX * 1.5 1.6 1.8 2.1 2.0 2.0 1.5 1.2 1.4 1.5 2.2 1.8 1.5 1.5

DEGR.* 295 300 290 270 255 245 250 245 255 230 250 225 255 245

THE HIGHEST CONCENTRATION IS 2.20 PPM AT 250 DEGREES FROM REC11.
THE 2ND HIGHEST CONCENTRATION IS 2.10 PPM AT 270 DEGREES FROM REC4 .
THE 3RD HIGHEST CONCENTRATION IS 2.00 PPM AT 255 DEGREES FROM REC5 .

JOB: Central & McMillan Alt I PM RUN: Central & McMillan Alt I PM
 DATE: 08/27/2010 TIME: 11:47:19.93

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		(FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
1. NB	Cen aprch	* 266300.0	298030.0	265981.0	298520.0 *	585.	327.	AG	1600.	12.1	.0	.56	.0	
2. NB	Cen aprch	* 265981.0	298520.0	265930.0	298621.0 *	113.	333.	AG	1600.	12.1	.0	.56	.0	
3. NB	Cen th+rt	* 265930.0	298621.0	265887.0	298770.0 *	155.	344.	AG	990.	12.1	.0	.44	.0	
4. NB	Cen thru	* 265887.0	298770.0	265848.0	298926.0 *	161.	346.	AG	970.	12.1	.0	.44	.0	
5. NB	Cen thru	* 265860.0	298880.0	265896.0	298735.9 *	149.	166.	AG	184.	100.0	.0	.24	.57	7.5
6. NB	Cen right	* 265896.0	298777.0	265889.0	298867.0 *	90.	356.	AG	20.	12.1	.0	.32	.0	
7. NB	Cen right	* 265890.0	298859.0	265890.4	298852.9 *	6.	176.	AG	92.	100.0	.0	.12	.03	.3
8. NB	Cen right	* 265889.0	298867.0	265913.0	298986.0 *	121.	11.	AG	20.	12.1	.0	.32	.0	
9. NB	Cen left	* 265930.0	298621.0	265871.0	298749.0 *	141.	335.	AG	610.	12.1	.0	.44	.0	
10. NB	Cen left	* 265871.0	298749.0	265834.0	298915.0 *	170.	347.	AG	610.	12.1	.0	.44	.0	
11. NB	Cen left	* 265843.0	298876.0	265880.1	298705.5 *	175.	168.	AG	295.	100.5	.0	.24	.86	8.9
12. NB	Cen depart	* 265848.0	298926.0	265835.0	299123.0 *	197.	356.	AG	1150.	12.1	.0	.56	.0	
13. NB	Cen depart	* 265835.0	299123.0	265854.0	299553.0 *	430.	3.	AG	1150.	12.1	.0	.56	.0	
14. NB	Cen depart	* 265854.0	299553.0	265853.0	299734.0 *	181.	360.	AG	1150.	12.1	.0	.56	.0	
15. NB	Cen depart	* 265853.0	299734.0	265840.0	299908.0 *	174.	356.	AG	1150.	12.1	.0	.56	.0	
16. SB	Cen aprch	* 265814.0	299905.0	265829.0	299697.0 *	209.	176.	AG	820.	12.1	.0	.44	.0	
17. SB	Cen aprch	* 265829.0	299697.0	265831.0	299539.0 *	158.	179.	AG	820.	12.1	.0	.44	.0	
18. SB	Cen aprch	* 265831.0	299539.0	265800.0	299112.0 *	428.	184.	AG	820.	12.1	.0	.44	.0	
19. SB	Cen aprch	* 265800.0	299112.0	265807.0	298918.0 *	194.	178.	AG	820.	12.1	.0	.56	.0	
20. SB	Cen aprch	* 265805.0	298976.0	265800.2	299105.8 *	130.	358.	AG	428.	100.0	.0	.36	.69	6.6
21. SB	Cen depart	* 265807.0	298918.0	265870.0	298694.0 *	233.	164.	AG	910.	12.1	.0	.44	.0	
22. SB	Cen depart	* 265870.0	298694.0	265929.0	298554.0 *	152.	157.	AG	910.	12.1	.0	.44	.0	
23. SB	Cen depart	* 265929.0	298554.0	266278.0	298019.0 *	639.	147.	AG	910.	12.1	.0	.44	.0	
24. EB	McM aprch	* 264648.0	299034.0	265403.0	298932.0 *	762.	98.	BR	660.	12.1	15.0	.44	.0	
25. EB	McM thru+*	265403.0	298932.0	265612.0	298913.0 *	210.	95.	BR	430.	12.1	15.0	.44	.0	
26. EB	McM thru+*	265612.0	298913.0	265821.0	298881.0 *	211.	99.	AG	430.	12.1	.0	.44	.0	
27. EB	McM thr+lt*	265773.0	298888.0	265684.7	298901.6 *	89.	279.	AG	249.	100.0	.0	.24	.37	4.5
28. EB	McM right	* 265403.0	298932.0	265757.0	298877.0 *	358.	99.	AG	230.	12.1	.0	.32	.0	
29. EB	McM right	* 265751.0	298878.0	265656.6	298892.7 *	96.	279.	AG	125.	100.0	.0	.12	.41	4.9
30. EB	McM right	* 265757.0	298877.0	265798.0	298862.0 *	44.	110.	AG	230.	12.1	.0	.32	.0	
31. EB	McM right	* 265798.0	298862.0	265827.0	298834.0 *	40.	134.	AG	230.	12.1	.0	.32	.0	
32. EB	McM depart	* 265821.0	298884.0	265876.0	298929.0 *	71.	51.	AG	270.	12.1	.0	.44	.0	
33. EB	McM depart	* 265876.0	298929.0	265913.0	298986.0 *	68.	33.	AG	270.	12.1	.0	.44	.0	
34. EB	McM depart	* 265912.0	298988.0	265938.0	299116.0 *	131.	11.	AG	290.	12.1	.0	.44	.0	
35. EB	McM depart	* 265938.0	299116.0	265975.0	299226.0 *	116.	19.	AG	290.	12.1	.0	.44	.0	
36. EB	McM depart	* 265975.0	299226.0	266163.0	299539.0 *	365.	31.	AG	290.	12.1	.0	.44	.0	
37. EB	McM depart	* 266163.0	299539.0	266220.0	299610.0 *	91.	39.	AG	290.	12.1	.0	.44	.0	
38. EB	McM depart	* 266220.0	299610.0	266293.0	299664.0 *	91.	54.	AG	290.	12.1	.0	.44	.0	
39. EB	McM depart	* 266293.0	299664.0	266414.0	299711.0 *	130.	69.	AG	290.	12.1	.0	.44	.0	
40. WB	McM aprch	* 266380.0	299736.0	266244.0	299666.0 *	153.	243.	AG	610.	12.1	.0	.44	.0	
41. WB	McM aprch	* 266244.0	299666.0	266173.0	299596.0 *	100.	225.	AG	610.	12.1	.0	.44	.0	
42. WB	McM aprch	* 266173.0	299596.0	265969.0	299259.0 *	394.	211.	AG	610.	12.1	.0	.44	.0	
43. WB	McM aprch	* 265969.0	299259.0	265933.0	299173.0 *	93.	203.	AG	610.	12.1	.0	.44	.0	
44. WB	McM aprch	* 265933.0	299173.0	265909.0	299091.0 *	85.	196.	AG	610.	12.1	.0	.44	.0	

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JOB: Central & McMillan Alt I PM RUN: Central & McMillan Alt I PM
 DATE: 08/27/2010 TIME: 11:47:19.93

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)		(FT) (DEG)	LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
45. WB	McM aprch	* 265909.0	299091.0	265892.0	299010.0 *	83.	192.	AG	610.	12.1	.0	.44	.0	
46. WB	McM aprch	* 265892.0	299010.0	265856.0	298942.0 *	77.	208.	AG	610.	12.1	.0	.44	.0	
47. WB	McM aprch	* 265892.0	299011.0	265822.9	298878.5 *	149.	208.	AG	285.	100.0	.0	.24	.75	7.6
48. WB	McM depart	* 265856.0	298942.0	265752.0	298914.0 *	108.	255.	AG	1340.	12.1	.0	.44	.0	
49. WB	McM depart	* 265752.0	298914.0	264661.0	299060.0 *	1101.	278.	BR	1340.	12.1	15.0	.44	.0	
50. NB	I-75	* 265324.0	298040.0	265380.0	298899.0 *	861.	4.	AG	7856.	12.9	.0	.80	.0	
51. NB	I-75	* 265380.0	298899.0	265402.0	299143.0 *	245.	5.	AG	7856.	12.9	.0	.80	.0	
52. NB	I-75	* 265402.0	299143.0	265454.0	299420.0 *	282.	11.	AG	7856.	12.9	.0	.80	.0	
53. NB	I-75	* 265454.0	299420.0	265576.0	299875.0 *	471.	15.	AG	7856.	12.9	.0	.80	.0	
54. SB	I-75	* 265474.0	299844.0	265416.0	299648.0 *	204.	196.	AG	6720.	12.9	.0	.80	.0	
55. SB	I-75	* 265416.0	299648.0	265345.0	299344.0 *	312.	193.	AG	6720.	12.9	.0	.80	.0	
56. SB	I-75	* 265345.0	299344.0	265316.0	299152.0 *	194.	189.	AG	6720.	12.9	.0	.80	.0	
57. SB	I-75	* 265316.0	299152.0	265292.0	298925.0 *	228.	186.	AG	6720.	12.9	.0	.80	.0	
58. SB	I-75	* 265292.0	298925.0	265238.0	298100.0 *	827.	184.	AG	6720.	12.9	.0	.80	.0	

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JOB: Central & McMillan Alt I PM RUN: Central & McMillan Alt I PM
 DATE: 08/27/2010 TIME: 11:47:19.93

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	RATE	EM	FAC	TYPE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
5. NB	Cen thru	* 120	56	2.0	970	1691	73.30	1 3
7. NB	Cen right	* 120	56	2.0	20	1509	73.30	1 3
11. NB	Cen left	* 120	90	2.0	610	1638	73.30	1 3

20. SB	Cen aprch *	120	87	2.0	820	1630	73.30	1	3
27. EB	McM thr+lt*	120	76	2.0	430	1732	73.30	1	3
29. EB	McM right *	120	76	2.0	230	1687	73.30	1	3
47. WB	McM aprch *	120	87	2.0	610	1682	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT)			*
	X	Y	Z	
1. SE MID S	265957.0	298638.0	5.0	*
2. SE 164 S	265938.0	298713.0	5.0	*
3. SE 82 S	265912.0	298793.0	5.0	*
4. SE CNR	265918.0	298875.0	5.0	*
5. SE 82 E	265934.0	298958.0	5.0	*
6. SE 164 E	265949.0	299039.0	5.0	*
7. SE MID E	265999.0	299214.0	5.0	*
8. NE MID E	265976.0	299319.0	5.0	*
9. NE 164 E	265908.0	299163.0	5.0	*
10. NE 82 E	265886.0	299084.0	5.0	*
11. NE CNR	265865.0	298999.0	5.0	*
12. NE 82 N	265859.0	299083.0	5.0	*
13. NE 164 N	265860.0	299164.0	5.0	*
14. NE MID N	265871.0	299350.0	5.0	*

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JOB: Central & McMillan Alt I PM

RUN: Central & McMillan Alt I PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14

0.	.1	.2	.5	.3	.3	.5	.3	.0	.1	.4	.9	.8	.8	.8
5.	.0	.0	.2	.2	.2	.5	.4	.0	.2	.3	.8	.8	.7	.6
10.	.0	.0	.1	.0	.1	.2	.4	.1	.2	.2	.7	.6	.6	.5
15.	.0	.0	.0	.0	.2	.1	.4	.1	.3	.6	.6	.4	.4	.3
20.	.0	.0	.0	.0	.1	.4	.1	.4	.5	.8	.3	.3	.2	
25.	.0	.0	.0	.0	.1	.2	.2	.4	.5	.7	.5	.3	.1	
30.	.0	.0	.0	.0	.0	.2	.3	.5	.6	.8	.4	.3	.1	
35.	.0	.0	.0	.0	.0	.2	.4	.5	.6	.8	.4	.2	.1	
40.	.0	.0	.0	.0	.0	.1	.4	.5	.6	.8	.4	.3	.1	
45.	.0	.0	.0	.0	.0	.0	.5	.6	.4	.8	.2	.4	.1	
50.	.0	.0	.0	.0	.0	.0	.5	.6	.4	1.0	.2	.4	.2	
55.	.0	.0	.0	.0	.0	.0	.4	.4	.3	1.1	.2	.3	.2	
60.	.0	.0	.0	.0	.0	.0	.4	.4	.4	1.1	.1	.2	.1	
65.	.0	.0	.0	.0	.0	.0	.4	.4	.4	1.0	.1	.1	.1	
70.	.0	.0	.0	.0	.0	.0	.4	.4	.3	1.1	.2	.1	.1	
75.	.0	.0	.0	.0	.0	.0	.4	.4	.3	1.1	.2	.1	.1	
80.	.0	.0	.0	.0	.0	.0	.4	.4	.4	1.1	.2	.2	.1	
85.	.0	.0	.0	.0	.0	.0	.4	.4	.4	1.2	.3	.3	.1	
90.	.0	.0	.0	.0	.0	.0	.3	.4	.4	1.1	.3	.2	.1	
95.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.1	.2	.1	.1	
100.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.1	.2	.1	.1	
105.	.0	.0	.0	.0	.0	.0	.3	.4	.3	1.1	.3	.1	.1	
110.	.0	.0	.0	.0	.0	.0	.3	.4	.3	1.2	.4	.1	.1	
115.	.0	.0	.0	.0	.0	.0	.3	.4	.3	1.4	.4	.1	.1	
120.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.4	.4	.1	.1	
125.	.1	.0	.0	.0	.0	.0	.3	.3	.3	1.4	.4	.2	.1	
130.	.2	.0	.0	.0	.0	.0	.3	.3	.4	1.4	.4	.2	.1	
135.	.2	.1	.0	.0	.0	.0	.3	.4	.4	1.4	.5	.2	.1	
140.	.5	.1	.1	.0	.0	.0	.3	.4	.4	1.4	.5	.2	.2	
145.	.6	.4	.2	.1	.0	.0	.3	.4	.4	1.4	.3	.3	.2	
150.	.7	.4	.5	.1	.1	.0	.3	.3	.5	1.6	.6	.3	.2	
155.	1.0	.4	.5	.2	.1	.1	.3	.4	.6	2.1	.7	.6	.2	
160.	1.1	.8	.6	.3	.2	.1	.3	.5	.6	2.1	1.2	.5	.1	
165.	1.0	.7	.8	.4	.2	.2	.4	.6	1.0	2.6	1.4	.8	.3	
170.	1.1	.9	.9	.5	.2	.1	.5	.7	1.2	2.9	1.6	1.1	.6	
175.	1.0	.8	.9	.8	.5	.2	.1	.5	.8	1.3	3.0	1.7	1.3	.8
180.	.9	.8	1.1	.9	.5	.3	.1	.4	1.1	1.3	3.0	2.0	1.6	1.0
185.	1.0	.9	1.0	1.0	.4	.4	.1	.5	1.1	1.6	2.9	1.9	1.8	1.3
190.	.9	.9	1.3	.9	.6	.5	.2	.6	1.2	1.6	2.9	1.9	1.8	1.3
195.	.8	.8	1.4	1.3	.8	.7	.3	.8	1.5	1.9	2.8	1.8	1.9	1.6
200.	.8	.9	1.3	1.3	1.0	.9	.5	1.0	1.6	1.7	2.7	2.1	1.9	1.8
205.	.9	.9	1.6	1.3	1.0	1.2	.9	1.1	1.4	2.0	2.5	2.1	2.3	1.6

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JOB: Central & McMillan Alt I PM

RUN: Central & McMillan Alt I PM

WIND * CONCENTRATION

ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14

210.	.8	.9	1.8	1.5	1.2	1.7	1.1	1.4	1.6	2.0	2.7	2.4	2.5	1.8
215.	.9	.9	2.0	1.6	1.5	1.8	1.2	1.5	2.0	2.1	2.4	2.6	2.4	2.0
220.	.9	1.1	2.2	1.8	1.4	1.8	1.5	1.4	1.8	2.2	2.5	2.6	2.3	2.0
225.	1.1	1.2	2.4	1.9	1.7	2.1	1.6	1.2	1.8	2.3	2.8	2.7	2.2	1.7
230.	1.3	1.3	2.6	2.0	1.7	2.4	1.6	1.4	1.9	2.2	2.6	2.6	2.1	1.9
235.	1.4	1.4	2.4	2.1	2.0	2.3	1.7	1.1	1.7	2.4	2.6	2.7	2.1	1.8

240.	*	1.5	1.5	2.6	2.1	2.0	2.3	1.8	1.4	1.7	2.2	2.5	2.7	2.0	1.8
245.	*	1.4	1.6	2.6	2.1	2.3	2.2	1.5	1.3	1.6	2.2	2.4	2.6	1.7	1.7
250.	*	1.7	1.7	2.6	2.1	2.3	2.4	1.6	1.3	1.6	2.3	2.3	2.7	1.7	1.7
255.	*	1.7	1.8	2.6	2.2	2.5	2.1	1.6	1.3	1.6	2.2	2.4	2.6	1.8	1.7
260.	*	1.7	1.8	2.6	2.2	2.6	2.1	1.4	1.1	1.3	2.1	2.4	2.5	1.8	1.6
265.	*	1.7	1.9	2.4	2.3	2.5	1.9	1.5	1.2	1.2	2.2	2.5	2.6	1.7	1.7
270.	*	1.6	1.7	2.7	2.3	2.4	2.1	1.3	1.2	1.4	1.9	2.4	2.4	1.7	1.6
275.	*	1.4	1.8	2.7	2.5	2.3	1.9	1.4	1.1	1.3	1.8	2.5	2.3	1.7	1.7
280.	*	1.5	2.2	3.0	2.1	2.3	1.9	1.4	1.2	1.3	1.7	2.4	2.1	1.8	1.7
285.	*	1.8	2.1	3.0	2.5	2.2	1.8	1.3	1.2	1.3	1.7	2.4	2.2	1.6	1.6
290.	*	1.7	2.1	3.1	2.3	2.1	1.7	1.3	1.2	1.3	1.7	2.4	1.9	1.7	1.7
295.	*	1.9	2.5	3.1	2.4	2.2	1.8	1.6	1.1	1.3	1.7	2.4	1.8	1.7	1.6
300.	*	2.0	2.7	3.2	2.3	2.2	1.4	1.5	1.2	1.4	1.3	2.4	1.8	1.6	1.6
305.	*	2.1	2.7	3.1	2.2	2.0	1.4	1.4	1.1	1.3	1.4	2.3	1.9	1.6	1.7
310.	*	1.9	2.5	3.3	1.9	2.0	1.5	1.2	1.1	1.3	1.4	2.4	2.0	1.7	1.6
315.	*	2.3	2.8	3.1	1.9	2.0	1.3	1.2	.9	1.2	1.6	2.4	1.8	1.7	1.6
320.	*	2.4	3.0	2.8	2.1	2.1	1.4	1.1	.7	1.2	1.3	2.4	1.7	1.6	1.4
325.	*	2.6	2.6	2.8	2.0	2.0	1.2	.9	.6	1.1	1.3	2.3	1.8	1.6	1.4
330.	*	2.4	2.5	2.6	1.7	1.3	1.1	.8	.4	.9	1.2	2.1	1.6	1.6	1.2
335.	*	2.0	2.3	2.3	1.8	1.2	1.0	.5	.3	.8	1.1	1.9	1.5	1.4	1.1
340.	*	1.9	2.2	2.2	1.6	1.0	.8	.6	.3	.7	1.0	1.7	1.4	1.3	1.2
345.	*	1.5	1.4	1.5	1.1	.7	.6	.3	.1	.5	.8	1.6	1.2	1.1	1.1
350.	*	.9	.8	1.1	.8	.5	.5	.3	.1	.4	.5	1.2	1.1	1.0	.9
355.	*	.8	.7	.9	.6	.4	.3	.3	.0	.3	.5	1.0	1.1	1.0	.9
360.	*	.1	.2	.5	.3	.3	.5	.3	.0	.1	.4	.9	.8	.8	.8

MAX * 2.6 3.0 3.3 2.5 2.6 2.4 1.8 1.5 2.0 2.4 3.0 2.7 2.5 2.0
DEGR. * 325 320 310 275 260 230 240 215 215 235 175 225 210 220

THE HIGHEST CONCENTRATION IS 3.30 PPM AT 310 DEGREES FROM REC3.
THE 2ND HIGHEST CONCENTRATION IS 3.00 PPM AT 175 DEGREES FROM REC11.
THE 3RD HIGHEST CONCENTRATION IS 3.00 PPM AT 320 DEGREES FROM REC2.
1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

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JOB: Central & McMillan No Bld AM RUN: Central & McMillan No Bld AM
DATE: 08/27/2010 TIME: 09:48:46.92

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 321. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT)				LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH (VEH)	EF	H	W	V/C	QUEUE
	X1	Y1	X2	Y2									
1. NB	Cen aprch	* 266300.0	298030.0	265981.0	298520.0	* 585.	327. AG	400.	12.1	.0	56.0		
2. NB	Cen aprch	* 265981.0	298520.0	265930.0	298621.0	* 113.	333. AG	400.	12.1	.0	56.0		
3. NB	Cen th+rt	* 265930.0	298621.0	265887.0	298770.0	* 155.	344. AG	250.	12.1	.0	44.0		
4. NB	Cen thru	* 265887.0	298770.0	265848.0	298926.0	* 161.	346. AG	240.	12.1	.0	44.0		
5. NB	Cen thru	* 265860.0	298880.0	265863.8	298864.7	* 16.	166. AG	145.	100.0	.0	24.0	.12	.8
6. NB	Cen right	* 265896.0	298777.0	265889.0	298867.0	* 90.	356. AG	10.	12.1	.0	32.0		
7. NB	Cen right	* 265890.0	298859.0	265890.1	298857.7	* 1.	176. AG	73.	100.0	.0	12.0	.01	.1
8. NB	Cen right	* 265889.0	298867.0	265913.0	298986.0	* 121.	11. AG	10.	12.1	.0	32.0		
9. NB	Cen left	* 265930.0	298621.0	265871.0	298749.0	* 141.	335. AG	150.	12.1	.0	44.0		
10. NB	Cen left	* 265871.0	298749.0	265834.0	298915.0	* 170.	347. AG	150.	12.1	.0	44.0		
11. NB	Cen left	* 265843.0	298876.0	265845.1	298866.4	* 10.	168. AG	145.	100.0	.0	24.0	.19	.5
12. NB	Cen depart	* 265848.0	298926.0	265835.0	299123.0	* 197.	356. AG	450.	12.1	.0	56.0		
13. NB	Cen depart	* 265835.0	299123.0	265854.0	299553.0	* 430.	3. AG	450.	12.1	.0	56.0		
14. NB	Cen depart	* 265854.0	299553.0	265853.0	299734.0	* 181.	360. AG	450.	12.1	.0	56.0		
15. NB	Cen depart	* 265853.0	299734.0	265840.0	299908.0	* 174.	356. AG	450.	12.1	.0	56.0		
16. SB	Cen aprch	* 265814.0	299905.0	265829.0	299697.0	* 209.	176. AG	720.	12.1	.0	44.0		
17. SB	Cen aprch	* 265829.0	299697.0	265831.0	299539.0	* 158.	179. AG	720.	12.1	.0	44.0		
18. SB	Cen aprch	* 265831.0	299539.0	265800.0	299112.0	* 428.	184. AG	720.	12.1	.0	44.0		
19. SB	Cen aprch	* 265800.0	299112.0	265807.0	298918.0	* 194.	178. AG	720.	12.1	.0	56.0		
20. SB	Cen aprch	* 265805.0	298976.0	265803.9	299007.5	* 31.	358. AG	218.	100.0	.0	36.0	.26	1.6
21. SB	Cen depart	* 265807.0	298918.0	265870.0	298694.0	* 233.	164. AG	1320.	12.1	.0	44.0		
22. SB	Cen depart	* 265870.0	298694.0	265929.0	298554.0	* 152.	157. AG	1320.	12.1	.0	44.0		
23. SB	Cen depart	* 265929.0	298554.0	266278.0	298019.0	* 639.	147. AG	1320.	12.1	.0	44.0		
24. EB	McM aprch	* 264648.0	299034.0	265403.0	298932.0	* 762.	98. BR	1540.	12.1	15.0	44.0		
25. EB	McM thru+lt	* 265403.0	298932.0	265612.0	298913.0	* 210.	95. BR	910.	12.1	15.0	44.0		
26. EB	McM thru+lt	* 265612.0	298913.0	265821.0	298881.0	* 211.	99. AG	910.	12.1	.0	44.0		
27. EB	McM thr+lt	* 265773.0	298888.0	265689.4	298900.9	* 85.	279. AG	206.	100.0	.0	24.0	.66	4.3
28. EB	McM right	* 265403.0	298932.0	265757.0	298877.0	* 358.	99. AG	630.	12.1	.0	32.0		
29. EB	McM right	* 265757.0	298877.0	265474.7	298920.9	* 280.	279. AG	103.	100.0	.0	12.0	1.01	14.2
30. EB	McM right	* 265757.0	298877.0	265798.0	298862.0	* 44.	110. AG	630.	12.1	.0	32.0		
31. EB	McM right	* 265798.0	298862.0	265827.0	298834.0	* 40.	134. AG	630.	12.1	.0	32.0		
32. EB	McM depart	* 265821.0	298884.0	265876.0	298929.0	* 71.	51. AG	710.	12.1	.0	44.0		
33. EB	McM depart	* 265876.0	298929.0	265913.0	298986.0	* 68.	33. AG	710.	12.1	.0	44.0		
34. EB	McM depart	* 265912.0	298988.0	265938.0	299116.0	* 131.	11. AG	720.	12.1	.0	44.0		
35. EB	McM depart	* 265938.0	299116.0	265975.0	299226.0	* 116.	19. AG	720.	12.1	.0	44.0		
36. EB	McM depart	* 265975.0	299226.0	266163.0	299539.0	* 365.	31. AG	720.	12.1	.0	44.0		
37. EB	McM depart	* 266163.0	299539.0	266220.0	299610.0	* 91.	39. AG	720.	12.1	.0	44.0		
38. EB	McM depart	* 266220.0	299610.0	266293.0	299664.0	* 91.	54. AG	720.	12.1	.0	44.0		
39. EB	McM depart	* 266293.0	299664.0	266414.0	299711.0	* 130.	69. AG	720.	12.1	.0	44.0		
40. WB	McM aprch	* 266380.0	299736.0	266244.0	299666.0	* 153.	243. AG	200.	12.1	.0	44.0		
41. WB	McM aprch	* 266244.0	299666.0	266173.0	299596.0	* 100.	225. AG	200.	12.1	.0	44.0		
42. WB	McM aprch	* 266173.0	299596.0	265969.0	299259.0	* 394.	211. AG	200.	12.1	.0	44.0		
43. WB	McM aprch	* 265969.0	299259.0	265933.0	299173.0	* 93.	203. AG	200.	12.1	.0	44.0		
44. WB	McM aprch	* 265933.0	299173.0	265909.0	299091.0	* 85.	196. AG	200.	12.1	.0	44.0		

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JOB: Central & McMillan No Bld AM RUN: Central & McMillan No Bld AM
DATE: 08/27/2010 TIME: 09:48:46.92

LINK VARIABLES

LINK DESCRIPTION		LINK COORDINATES (FT)				LENGTH	BRG	TYPE	VPH	EF	H	W	V/C	QUEUE
*	* X1	Y1	X2	Y2	(FT)	(DEG)	(G/MI)	(FT)	(VEH)					
45. WB	McM aprch	* 265909.0	299091.0	265892.0	299010.0	*	83.	192.	AG	200.	12.1	.0	44.0	
46. WB	McM aprch	* 265892.0	299010.0	265856.0	298942.0	*	77.	208.	AG	200.	12.1	.0	44.0	
47. WB	McM aprch	* 265892.0	299011.0	265880.1	298988.2	*	26.	208.	AG	284.	100.0	.0	24.0 .28 1.3	
48. WB	McM depart	* 265856.0	298942.0	265752.0	298914.0	*	108.	255.	AG	370.	12.1	.0	44.0	
49. WB	McM depart	* 265752.0	298914.0	264661.0	299060.0	*	1101.	278.	BR	370.	12.1	15.0	44.0	
50. EB	south loop	* 265447.0	298923.0	265645.0	298862.0	*	207.	107.	AG	760.	12.1	.0	32.0	
51. EB	south loop	* 265645.0	298862.0	265771.0	298755.0	*	165.	130.	AG	760.	12.1	.0	32.0	
52. EB	south loop	* 265771.0	298755.0	265821.0	298673.0	*	96.	149.	AG	760.	12.1	.0	32.0	
53. EB	south loop	* 265821.0	298673.0	265843.0	298597.0	*	79.	164.	AG	760.	12.1	.0	32.0	
54. EB	south loop	* 265843.0	298597.0	265839.0	298518.0	*	79.	183.	AG	760.	12.1	.0	32.0	
55. EB	south loop	* 265839.0	298518.0	265812.0	298456.0	*	68.	204.	AG	760.	12.1	.0	32.0	
56. EB	south loop	* 265812.0	298456.0	265766.0	298407.0	*	67.	223.	AG	760.	12.1	.0	32.0	
57. EB	south loop	* 265766.0	298407.0	265713.0	298377.0	*	61.	241.	AG	760.	12.1	.0	32.0	
58. EB	south loop	* 265713.0	298377.0	265652.0	298363.0	*	63.	257.	AG	760.	12.1	.0	32.0	
59. EB	south loop	* 265652.0	298363.0	265590.0	298367.0	*	62.	274.	AG	760.	12.1	.0	32.0	
60. EB	south loop	* 265590.0	298367.0	265531.0	298389.0	*	63.	290.	AG	760.	12.1	.0	32.0	
61. EB	south loop	* 265531.0	298389.0	265477.0	298437.0	*	72.	312.	AG	760.	12.1	.0	32.0	
62. EB	south loop	* 265477.0	298437.0	265443.0	298496.0	*	68.	330.	AG	760.	12.1	.0	32.0	
63. EB	south loop	* 265443.0	298496.0	265425.0	298562.0	*	68.	345.	AG	760.	12.1	.0	32.0	
64. EB	south loop	* 265425.0	298562.0	265430.0	298755.0	*	193.	1.	AG	760.	12.1	.0	32.0	
65. WB	north loop	* 265332.0	298608.0	265338.0	299177.0	*	569.	1.	AG	293.	12.1	.0	32.0	
66. WB	north loop	* 265338.0	299177.0	265353.0	299266.0	*	90.	10.	AG	293.	12.1	.0	32.0	
67. WB	north loop	* 265353.0	299266.0	265381.0	299332.0	*	72.	23.	AG	293.	12.1	.0	32.0	
68. WB	north loop	* 265381.0	299332.0	265459.0	299404.0	*	106.	47.	AG	293.	12.1	.0	32.0	
69. WB	north loop	* 265459.0	299404.0	265525.0	299426.0	*	70.	72.	AG	293.	12.1	.0	32.0	
70. WB	north loop	* 265525.0	299426.0	265605.0	299422.0	*	80.	93.	AG	293.	12.1	.0	32.0	
71. WB	north loop	* 265605.0	299422.0	265670.0	299394.0	*	71.	113.	AG	293.	12.1	.0	32.0	
72. WB	north loop	* 265670.0	299394.0	265724.0	299345.0	*	73.	132.	AG	293.	12.1	.0	32.0	
73. WB	north loop	* 265724.0	299345.0	265757.0	299282.0	*	71.	152.	AG	293.	12.1	.0	32.0	
74. WB	north loop	* 265757.0	299282.0	265766.0	299216.0	*	67.	172.	AG	293.	12.1	.0	32.0	
75. WB	north loop	* 265766.0	299216.0	265750.0	299137.0	*	81.	191.	AG	293.	12.1	.0	32.0	
76. WB	north loop	* 265750.0	299137.0	265713.0	299078.0	*	70.	212.	AG	293.	12.1	.0	32.0	
77. WB	north loop	* 265713.0	299078.0	265656.0	299025.0	*	78.	227.	AG	293.	12.1	.0	32.0	
78. WB	north loop	* 265656.0	299025.0	265590.0	298989.0	*	75.	241.	AG	293.	12.1	.0	32.0	
79. WB	north loop	* 265590.0	298989.0	265525.0	298971.0	*	67.	255.	AG	293.	12.1	.0	32.0	
80. WB	north loop	* 265525.0	298971.0	265373.0	298968.0	*	152.	269.	AG	293.	12.1	.0	32.0	
81. NB	I-75	* 265311.0	298053.0	265356.0	298545.0	*	494.	5.	AG	4892.	12.9	.0	68.0	
82. NB	I-75	* 265356.0	298545.0	265415.0	298994.0	*	453.	7.	AG	4892.	12.9	.0	68.0	
83. NB	I-75	* 265415.0	298994.0	265521.0	299559.0	*	575.	11.	AG	4892.	12.9	.0	68.0	
84. NB	I-75	* 265521.0	299559.0	265592.0	299877.0	*	326.	13.	AG	4892.	12.9	.0	68.0	
85. SB	I-75	* 265415.0	299817.0	265341.0	299495.0	*	330.	193.	AG	7674.	12.9	.0	68.0	
86. SB	I-75	* 265341.0	299495.0	265297.0	299275.0	*	224.	191.	AG	7674.	12.9	.0	68.0	
87. SB	I-75	* 265297.0	299275.0	265264.0	299008.0	*	269.	187.	AG	7674.	12.9	.0	68.0	
88. SB	I-75	* 265264.0	299008.0	265250.0	298765.0	*	243.	183.	AG	7674.	12.9	.0	68.0	
89. SB	I-75	* 265250.0	298765.0	265228.0	298107.0	*	658.	182.	AG	7674.	12.9	.0	68.0	

JOB: Central & McMillan No Bld AM
DATE: 08/27/2010 TIME: 09:48:46.92

RUN: Central & McMillan No Bld AM

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST	VOL	FLOW	EM	FAC	TYPE	RATE
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
5. NB	Cen thru	* 65	24	2.0	240	1691	73.30	1 3
7. NB	Cen right	* 65	24	2.0	10	1509	73.30	1 3
11. NB	Cen left	* 65	24	2.0	150	685	73.30	1 3
20. SB	Cen aprch	* 65	24	2.0	720	1630	73.30	1 3
27. EB	McM thr+lt*	65	34	2.0	910	1650	73.30	1 3
29. EB	McM right	* 65	34	2.0	630	1509	73.30	1 3
47. WB	McM aprch	* 65	47	2.0	200	1678	73.30	1 3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT)			
*	X	Y	Z	*
1. SE MID S	* 265957.0	298638.0		5.0 *
2. SE 164 S	* 265938.0	298713.0		5.0 *
3. SE 82 S	* 265912.0	298793.0		5.0 *
4. SE CNR	* 265918.0	298875.0		5.0 *
5. SE 82 E	* 265934.0	298958.0		5.0 *
6. SE 164 E	* 265949.0	299039.0		5.0 *
7. SE MID E	* 265999.0	299214.0		5.0 *
8. NE MID E	* 265976.0	299319.0		5.0 *
9. NE 164 E	* 265908.0	299163.0		5.0 *
10. NE 82 E	* 265886.0	299084.0		5.0 *
11. NE CNR	* 265865.0	298999.0		5.0 *
12. NE 82 N	* 265859.0	299083.0		5.0 *
13. NE 164 N	* 265860.0	299164.0		5.0 *
14. NE MID N	* 265871.0	299350.0		5.0 *

JOB: Central & McMillan No Bld AM

RUN: Central & McMillan No Bld AM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14
0.	.0	.0	.1	.3	.3	.5	.0	.1	.2	.4	.4	.4	.3	
5.	.0	.0	.1	.2	.3	.4	.5	.0	.0	.1	.3	.3	.3	.2
10.	.0	.0	.0	.2	.4	.4	.5	.0	.0	.0	.2	.3	.3	.1
15.	.0	.0	.0	.1	.3	.3	.5	.0	.1	.3	.3	.2	.2	.1
20.	.0	.0	.0	.1	.2	.3	.5	.0	.2	.3	.5	.3	.1	.1
25.	.0	.0	.0	.0	.2	.3	.4	.2	.2	.3	.6	.1	.1	.1
30.	.0	.0	.0	.0	.1	.3	.2	.4	.3	.5	.2	.2	.0	
35.	.0	.0	.0	.0	.0	.2	.2	.4	.4	.7	.2	.1	.0	
40.	.0	.0	.0	.0	.0	.2	.3	.4	.5	.7	.2	.1	.0	
45.	.0	.0	.0	.0	.0	.1	.3	.4	.5	.6	.2	.1	.0	
50.	.0	.0	.0	.0	.0	.1	.3	.4	.3	.8	.2	.1	.0	
55.	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.1	.2	.1	
60.	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.2	.2	.1	
65.	.0	.0	.0	.0	.0	.0	.3	.4	.3	.9	.2	.2	.1	
70.	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.2	.2	.1	
75.	.0	.0	.0	.0	.0	.0	.3	.3	.2	1.0	.2	.1	.1	
80.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1	
85.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1	
90.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.1	.1	.1	
95.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.1	.1	.1	.1	
100.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.2	.1	.1	
105.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.3	.1	.1	
110.	.0	.0	.0	.0	.0	.0	.3	.3	.3	1.0	.3	.1	.1	
115.	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.3	.1	.1	
120.	.0	.0	.0	.0	.0	.0	.3	.3	.3	.9	.3	.2	.1	
125.	.0	.0	.0	.0	.0	.0	.3	.3	.3	.8	.2	.2	.1	
130.	.0	.0	.0	.0	.0	.0	.3	.3	.3	.7	.2	.1	.1	
135.	.1	.0	.0	.0	.0	.0	.3	.4	.3	.6	.2	.1	.1	
140.	.2	.1	.0	.0	.0	.0	.3	.3	.3	.5	.3	.1	.0	
145.	.4	.1	.1	.0	.0	.0	.3	.3	.3	.5	.3	.1	.1	
150.	.4	.2	.1	.1	.0	.0	.3	.3	.3	.6	.4	.1	.1	
155.	.5	.3	.1	.1	.1	.0	.3	.3	.5	.6	.5	.1	.1	
160.	.5	.3	.3	.1	.1	.1	.0	.3	.5	.6	.5	.2	.2	
165.	.5	.5	.4	.1	.1	.1	.0	.3	.5	.5	.7	.5	.4	.1
170.	.5	.4	.3	.2	.1	.1	.1	.4	.4	.6	.7	.6	.6	.1
175.	.6	.5	.4	.2	.2	.1	.1	.5	.4	.6	.9	.6	.5	.1
180.	.6	.6	.4	.3	.2	.2	.1	.3	.4	.6	.9	.4	.4	.3
185.	.5	.5	.5	.3	.3	.3	.1	.3	.4	.5	.8	.5	.4	.4
190.	.5	.4	.4	.2	.2	.4	.2	.3	.5	.8	.5	.4	.4	
195.	.5	.5	.4	.2	.2	.3	.3	.4	.5	.7	.8	.6	.6	
200.	.4	.4	.5	.3	.1	.4	.5	.4	.6	.6	1.0	1.1	.8	.8
205.	.4	.4	.4	.5	.3	.6	.6	.3	.5	.8	1.1	1.0	1.1	.8

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JOB: Central & McMillan No Bld AM

RUN: Central & McMillan No Bld AM

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14
210.	.5	.4	.5	.5	.4	.7	.7	.4	.8	1.0	1.4	1.3	1.1	1.0
215.	.4	.5	.6	.6	.8	1.0	.8	.5	.9	1.1	1.3	1.3	1.3	1.1
220.	.5	.7	.9	.7	.8	1.4	1.0	.8	1.0	1.1	1.4	1.5	1.2	1.2
225.	.7	.9	.9	.8	1.0	1.3	1.0	.9	.9	1.2	1.6	1.6	1.4	1.1
230.	.9	.9	1.0	.9	1.1	1.7	1.1	.8	1.0	1.5	1.8	1.7	1.2	1.4
235.	.9	.9	1.2	1.0	1.3	1.8	.9	1.0	.9	1.3	1.9	1.5	1.2	1.5
240.	1.1	1.0	1.2	1.1	1.3	1.7	1.0	1.0	1.1	1.1	1.7	1.4	1.2	1.4
245.	1.1	1.2	1.3	1.1	1.4	1.7	1.1	1.1	1.1	.9	1.9	1.4	1.3	1.3
250.	1.2	1.2	1.2	1.4	1.6	1.6	1.3	1.0	1.1	1.1	1.9	1.4	1.4	1.4
255.	1.2	1.1	1.1	1.3	1.8	1.5	1.3	1.0	1.0	1.0	1.9	1.3	1.3	1.3
260.	1.2	1.1	1.2	1.6	1.9	1.6	1.3	.8	1.0	1.1	1.9	1.3	1.3	1.2
265.	1.1	1.2	1.2	1.6	1.8	1.5	1.3	.9	1.0	1.0	1.6	1.2	1.2	1.2
270.	1.2	1.2	1.3	1.9	1.5	1.4	1.1	.8	1.1	1.1	1.6	1.3	1.2	1.2
275.	1.2	1.3	1.3	1.9	1.4	1.4	1.3	.9	.9	1.1	1.5	1.3	1.2	1.3
280.	1.4	1.2	1.7	1.9	1.3	1.4	1.3	.8	.9	.9	1.5	1.1	1.2	1.3
285.	1.4	1.4	1.7	1.7	1.5	1.2	1.3	.9	.8	1.0	1.3	1.2	1.2	1.1
290.	1.4	1.2	1.7	1.7	1.2	1.3	1.2	.8	1.0	1.0	1.2	1.2	1.3	1.3
295.	1.4	1.4	1.6	1.6	1.4	1.3	1.3	.9	.8	1.0	1.2	1.1	1.3	1.2
300.	1.4	1.6	1.6	1.1	1.5	1.2	1.2	.8	.9	.9	1.2	1.2	1.1	1.3
305.	1.5	1.4	1.2	1.1	1.4	1.1	1.3	.8	.9	1.0	1.1	1.1	1.1	1.1
310.	1.3	1.2	1.4	1.1	1.5	1.1	1.0	.7	.9	1.1	1.2	1.1	1.2	1.1
315.	1.2	1.2	1.2	1.2	1.4	1.1	1.0	.6	.9	1.1	1.1	1.2	1.1	1.1
320.	1.1	1.1	1.3	1.2	1.3	1.1	.8	.5	.8	1.0	1.1	1.3	1.1	.9
325.	.9	1.0	1.3	1.0	1.3	1.0	.7	.5	.7	.8	1.0	1.2	.9	.8
330.	.9	1.0	1.0	1.1	1.0	.9	.5	.1	.5	.8	1.0	1.0	.9	.7
335.	.8	.6	1.0	.8	1.0	.8	.4	.1	.5	.7	.9	.8	.8	.6
340.	.5	.5	.7	.8	.8	.7	.4	.0	.3	.5	.9	.7	.8	.5
345.	.4	.4	.8	.7	.6	.7	.3	.0	.3	.3	.7	.6	.6	.6
350.	.1	.1	.3	.5	.5	.6	.4	.0	.2	.3	.5	.6	.6	.4
355.	.0	.0	.0	.4	.2	.3	.4	.0	.2	.2	.5	.6	.5	.4
360.	.0	.0	.1	.3	.3	.3	.5	.0	.1	.2	.4	.4	.4	.3

MAX * 1.5 1.6 1.7 1.9 1.9 1.8 1.3 1.1 1.1 1.5 1.9 1.7 1.4 1.5

DEGR. * 305 300 285 275 260 235 260 245 245 230 250 230 250 235

THE HIGHEST CONCENTRATION IS 1.90 PPM AT 250 DEGREES FROM REC11.
THE 2ND HIGHEST CONCENTRATION IS 1.90 PPM AT 275 DEGREES FROM REC4.
THE 3RD HIGHEST CONCENTRATION IS 1.90 PPM AT 260 DEGREES FROM REC5.

1 CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

PAGE 1

JOB: Central & McMillan No Bld PM

RUN: Central & McMillan No Bld PM

76. WB	north loop*	265750.0	299137.0	265713.0	299078.0	*	70.	212. AG	493.	12.1	.0	32.0
77. WB	north loop*	265713.0	299078.0	265656.0	299025.0	*	78.	227. AG	493.	12.1	.0	32.0
78. WB	north loop*	265656.0	299025.0	265590.0	298989.0	*	75.	241. AG	493.	12.1	.0	32.0
79. WB	north loop*	265590.0	298989.0	265525.0	298971.0	*	67.	255. AG	493.	12.1	.0	32.0
80. WB	north loop*	265525.0	298971.0	265373.0	298968.0	*	152.	269. AG	493.	12.1	.0	32.0
81. NB	I-75	* 265311.0	298053.0	265356.0	298545.0	*	494.	5. AG	7893.	12.9	.0	68.0
82. NB	I-75	* 265356.0	298545.0	265415.0	298994.0	*	453.	7. AG	7893.	12.9	.0	68.0
83. NB	I-75	* 265415.0	298994.0	265521.0	299559.0	*	575.	11. AG	7893.	12.9	.0	68.0
84. NB	I-75	* 265521.0	299559.0	265592.0	299877.0	*	326.	13. AG	7893.	12.9	.0	68.0
85. SB	I-75	* 265415.0	299817.0	265341.0	299495.0	*	330.	193. AG	6030.	12.9	.0	68.0
86. SB	I-75	* 265341.0	299495.0	265297.0	299275.0	*	224.	191. AG	6030.	12.9	.0	68.0
87. SB	I-75	* 265297.0	299275.0	265264.0	299008.0	*	269.	187. AG	6030.	12.9	.0	68.0
88. SB	I-75	* 265264.0	299008.0	265250.0	298765.0	*	243.	183. AG	6030.	12.9	.0	68.0
89. SB	I-75	* 265250.0	298765.0	265228.0	298107.0	*	658.	182. AG	6030.	12.9	.0	68.0

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JOB: Central & McMillan No Bld PM RUN: Central & McMillan No Bld PM
 DATE: 08/27/2010 TIME: 09:49:04.49

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE (SEC)	APPROACH (VPH)	SATURATION (VPH)	IDLE RATE (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
5. NB	Cen thru *	120	56	2.0	970	1691	73.30	1 3
7. NB	Cen right *	120	56	2.0	20	1509	73.30	1 3
11. NB	Cen left *	120	90	2.0	610	1638	73.30	1 3
20. SB	Cen aprch *	120	87	2.0	820	1630	73.30	1 3
27. EB	McM thr+lt *	120	76	2.0	430	1732	73.30	1 3
29. EB	McM right *	120	76	2.0	230	1687	73.30	1 3
47. WB	McM aprch *	120	87	2.0	610	1682	73.30	1 3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* X	* Y	* Z
1. SE MID S	* 265957.0	298638.0	5.0	*
2. SE 164 S	* 265938.0	298713.0	5.0	*
3. SE 82 S	* 265912.0	298793.0	5.0	*
4. SE CNR	* 265918.0	298875.0	5.0	*
5. SE 82 E	* 265934.0	298958.0	5.0	*
6. SE 164 E	* 265949.0	299039.0	5.0	*
7. SE MID E	* 265999.0	299214.0	5.0	*
8. NE MID E	* 265976.0	299319.0	5.0	*
9. NE 164 E	* 265908.0	299163.0	5.0	*
10. NE 82 E	* 265886.0	299084.0	5.0	*
11. NE CNR	* 265865.0	298999.0	5.0	*
12. NE 82 N	* 265859.0	299083.0	5.0	*
13. NE 164 N	* 265860.0	299164.0	5.0	*
14. NE MID N	* 265871.0	299350.0	5.0	*

1

JOB: Central & McMillan No Bld PM RUN: Central & McMillan No Bld PM

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	* REC1	* REC2	* REC3	* REC4	* REC5	* REC6	* REC7	* REC8	* REC9	* REC10	* REC11	* REC12	* REC13	* REC14
0.	.1	.2	.5	.3	.3	.5	.3	.0	.1	.4	.9	.8	.8	.8
5.	.0	.0	.2	.2	.2	.5	.4	.0	.2	.3	.8	.8	.7	.6
10.	.0	.0	.1	.0	.1	.2	.4	.1	.2	.2	.7	.6	.6	.5
15.	.0	.0	.0	.0	.2	.1	.4	.1	.3	.6	.6	.4	.4	.3
20.	.0	.0	.0	.0	.0	.1	.4	.1	.4	.5	.8	.3	.3	.2
25.	.0	.0	.0	.0	.0	.1	.2	.2	.4	.5	.7	.5	.3	.1
30.	.0	.0	.0	.0	.0	.2	.3	.5	.6	.8	.4	.3	.1	
35.	.0	.0	.0	.0	.0	.2	.4	.5	.6	.8	.4	.2	.1	
40.	.0	.0	.0	.0	.0	.1	.4	.5	.6	.8	.4	.3	.1	
45.	.0	.0	.0	.0	.0	.0	.5	.6	.4	.8	.2	.4	.1	
50.	.0	.0	.0	.0	.0	.0	.5	.6	.4	1.0	.2	.4	.2	
55.	.0	.0	.0	.0	.0	.0	.4	.3	1.1	.2	.3	.2		
60.	.0	.0	.0	.0	.0	.0	.4	.4	1.1	.1	.2	.1		
65.	.0	.0	.0	.0	.0	.0	.4	.4	1.0	.1	.1	.1		
70.	.0	.0	.0	.0	.0	.0	.4	.3	1.1	.2	.1	.1		
75.	.0	.0	.0	.0	.0	.0	.4	.3	1.1	.2	.1	.1		
80.	.0	.0	.0	.0	.0	.0	.4	.4	1.1	.2	.2	.1		
85.	.0	.0	.0	.0	.0	.0	.4	.4	1.2	.3	.3	.1		
90.	.0	.0	.0	.0	.0	.0	.3	.4	1.1	.3	.2	.1		
95.	.0	.0	.0	.0	.0	.0	.3	.3	1.1	.2	.1	.1		
100.	.0	.0	.0	.0	.0	.0	.3	.3	1.1	.2	.1	.1		
105.	.0	.0	.0	.0	.0	.0	.3	.4	1.1	.3	.1	.1		
110.	.0	.0	.0	.0	.0	.0	.3	.4	1.2	.4	.1	.1		
115.	.0	.0	.0	.0	.0	.0	.3	.4	1.4	.4	.1	.1		
120.	.0	.0	.0	.0	.0	.0	.3	.3	1.4	.4	.1	.1		
125.	.1	.0	.0	.0	.0	.0	.3	.3	1.4	.4	.2	.1		
130.	.2	.0	.0	.0	.0	.0	.3	.3	1.4	.4	.2	.1		
135.	.2	.1	.0	.0	.0	.0	.3	.4	1.4	.5	.2	.1		

140. * .5 .1 .1 .0 .0 .0 .3 .4 .4 1.4 .5 .2 .2
 145. * .6 .4 .2 .1 .0 .0 .3 .4 .4 1.4 .3 .3 .2
 150. * .7 .4 .5 .1 .1 .0 .3 .3 .5 1.6 .6 .3 .2
 155. * 1.0 .4 .5 .2 .1 .1 .0 .3 .4 .6 2.1 .7 .6 .2
 160. * 1.1 .8 .6 .3 .2 .1 .0 .3 .5 .6 2.1 1.2 .5 .1
 165. * 1.0 .7 .8 .4 .2 .2 .1 .4 .6 1.0 2.6 1.4 .8 .3
 170. * 1.1 .9 .9 .5 .2 .2 .1 .5 .7 1.2 2.9 1.6 1.1 .6
 175. * 1.0 .8 .9 .8 .5 .2 .1 .5 .8 1.3 3.0 1.7 1.3 .8
 180. * .9 .8 1.1 .9 .5 .3 .1 .4 1.1 1.3 3.0 2.0 1.6 1.0
 185. * 1.0 .9 1.0 1.0 .4 .4 .1 .5 1.1 1.6 2.9 1.9 1.8 1.3
 190. * .9 .9 1.3 .9 .6 .5 .2 .6 1.2 1.6 2.9 1.9 1.7 1.3
 195. * .8 .8 1.4 1.3 .8 .7 .3 .8 1.5 1.9 2.8 1.8 1.9 1.5
 200. * .8 .9 1.3 1.2 1.0 .9 .5 .9 1.4 1.5 2.7 2.1 1.9 1.8
 205. * .9 .9 1.6 1.3 1.0 1.0 .8 1.1 1.3 1.9 2.5 2.0 2.2 1.6

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JOB: Central & McMillan No Bld PM

RUN: Central & McMillan No Bld PM

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14

210. * .8 .9 1.8 1.5 1.2 1.6 1.0 1.3 1.6 1.9 2.6 2.4 2.4 1.7
 215. * .9 .9 2.0 1.6 1.4 1.8 1.1 1.4 1.9 1.9 2.4 2.5 2.5 2.0
 220. * .8 1.1 2.1 1.7 1.4 1.7 1.4 1.3 1.9 2.2 2.5 2.6 2.3 1.8
 225. * 1.1 1.1 2.4 1.9 1.5 2.0 1.6 1.2 1.8 2.2 2.7 2.6 2.2 1.8
 230. * 1.2 1.3 2.5 2.0 1.7 2.3 1.5 1.3 1.7 2.2 2.4 2.8 2.0 1.8
 235. * 1.4 1.3 2.4 2.0 1.9 2.3 1.8 1.2 1.7 2.3 2.6 2.6 2.1 1.8
 240. * 1.4 1.5 2.5 2.0 1.9 2.3 1.6 1.2 1.6 2.2 2.6 2.5 1.9 1.8
 245. * 1.4 1.6 2.5 2.1 2.2 2.2 1.6 1.2 1.8 2.2 2.2 2.6 1.8 1.7
 250. * 1.7 1.6 2.5 2.1 2.2 2.3 1.5 1.2 1.7 2.1 2.3 2.6 1.7 1.7
 255. * 1.5 1.7 2.5 2.2 2.3 2.1 1.4 1.4 1.5 2.2 2.4 2.5 1.7 1.6
 260. * 1.5 1.6 2.5 2.2 2.5 2.1 1.4 1.1 1.3 2.2 2.4 2.5 1.6 1.5
 265. * 1.6 1.8 2.5 2.2 2.5 1.9 1.4 1.1 1.3 2.0 2.3 2.4 1.8 1.6
 270. * 1.5 1.7 2.6 2.4 2.3 2.0 1.3 1.1 1.3 1.8 2.5 2.3 1.8 1.6
 275. * 1.5 1.6 2.6 2.4 2.2 1.9 1.3 1.2 1.2 1.8 2.4 2.3 1.7 1.7
 280. * 1.4 2.0 2.9 2.2 2.3 1.9 1.4 1.1 1.2 1.6 2.3 2.1 1.8 1.6
 285. * 1.6 2.2 2.9 2.4 2.2 1.7 1.4 1.1 1.2 1.6 2.4 2.1 1.7 1.7
 290. * 1.8 2.1 3.0 2.3 2.1 1.6 1.2 1.1 1.3 1.6 2.3 2.0 1.8 1.5
 295. * 1.8 2.3 3.0 2.4 2.1 1.6 1.5 1.1 1.2 1.7 2.3 1.8 1.6 1.6
 300. * 1.8 2.6 3.3 2.2 2.0 1.6 1.5 1.0 1.4 1.4 2.3 1.9 1.6 1.5
 305. * 2.1 2.6 3.1 2.0 2.2 1.3 1.3 .9 1.3 1.3 2.3 1.8 1.6 1.6
 310. * 1.8 2.6 3.0 1.9 1.9 1.4 1.2 1.0 1.3 1.4 2.3 1.8 1.6 1.5
 315. * 2.3 2.8 3.1 1.8 2.0 1.5 1.1 .8 1.1 1.4 2.3 1.8 1.6 1.5
 320. * 2.4 2.9 2.8 2.0 2.1 1.3 1.1 .8 1.1 1.2 2.4 1.8 1.5 1.3
 325. * 2.5 2.5 2.7 2.0 1.9 1.3 .9 .5 .9 1.4 2.4 1.6 1.5 1.4
 330. * 2.3 2.4 2.5 1.7 1.2 1.1 .7 .4 .9 1.2 2.1 1.6 1.4 1.2
 335. * 2.0 2.2 2.2 1.7 1.1 1.1 .6 .3 .8 1.1 1.9 1.4 1.5 1.1
 340. * 1.9 2.2 2.2 1.5 1.1 .7 .6 .3 .6 1.0 1.8 1.5 1.2 1.2
 345. * 1.5 1.5 1.6 1.1 .7 .6 .3 .1 .5 .8 1.6 1.1 1.1 1.1
 350. * .9 .8 1.1 .8 .5 .5 .3 .1 .4 .5 1.2 1.2 1.0 1.0
 355. * .8 .7 .9 .6 .4 .3 .3 .0 .3 .6 1.0 1.1 1.0 .9
 360. * .1 .2 .5 .3 .3 .5 .3 .0 .1 .4 .9 .8 .8 .8

MAX * 2.5 2.9 3.3 2.4 2.5 2.3 1.8 1.4 1.9 2.3 3.0 2.8 2.5 2.0
 DEGR. * 325 320 300 275 260 230 235 215 215 235 175 230 215 215

THE HIGHEST CONCENTRATION IS 3.30 PPM AT 300 DEGREES FROM REC3 .
 THE 2ND HIGHEST CONCENTRATION IS 3.00 PPM AT 175 DEGREES FROM REC11.
 THE 3RD HIGHEST CONCENTRATION IS 2.90 PPM AT 320 DEGREES FROM REC2 .

1

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000

JOB: Brent Spence Bridge T1altlpm.dat
 DATE: 08/31/2010 TIME: 08:03:18.51

RUN: Kyles Lane & Dixie Hwy-Trunc

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
 U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	* X1	Y1	LINK COORDINATES (FT)	* X2	Y2	(FT) (DEG)	* LENGTH (G/MI)	BRG (FT)	TYPE (FT)	VPH	EF	H	W	V/C	QUEUE
1. 01 Dixie NB Appr	* 264099.0	275553.0	264162.0	275726.0	*	184.	20.	AG	760.	11.5	.0	44.0			
2. 02 Dixie NB Appr	* 264162.0	275726.0	264197.0	275813.0	*	94.	22.	AG	760.	11.5	.0	44.0			
3. 03 Dixie NB Appr	* 264197.0	275813.0	264240.0	275916.0	*	112.	23.	AG	760.	11.5	.0	44.0			
4. 04 Dixie NB Queue	* 264228.0	275888.0	263898.8	275071.9	*	880.	202.	AG	295.	100.0	.0	24.0	1.20	44.7	
5. 05 Dixie NB @ Kyles	* 264240.0	275916.0	264280.0	276013.0	*	105.	22.	AG	540.	11.5	.0	44.0			
6. 06 Dixie NB Depart	* 264280.0	276013.0	264303.0	276071.0	*	62.	22.	AG	465.	11.5	.0	44.0			
7. 07 Dixie NB Depart	* 264303.0	276071.0	264360.0	276209.0	*	149.	22.	AG	1295.	11.5	.0	44.0			
8. 08 Dixie NB Depart	* 264360.0	276209.0	264406.0	276278.0	*	83.	34.	AG	1295.	11.5	.0	44.0			
9. 09 Dixie NB Depart	* 264406.0	276278.0	264446.0	276325.0	*	62.	40.	AG	1295.	11.5	.0	44.0			
10. 10 Dixie NB Depart	* 264446.0	276325.0	264529.0	276400.0	*	112.	48.	AG	1295.	11.5	.0	44.0			
11. 11 Dixie SB Appr	* 264499.0	276415.0	264439.0	276361.0	*	81.	228.	AG	1600.	11.5	.0	44.0			
12. 12 Dixie SB Appr	* 264439.0	276361.0	264381.0	276288.0	*	93.	218.	AG	1600.	11.5	.0	44.0			
13. 13 Dixie SB Appr	* 264381.0	276288.0	264351.0	276234.0	*	62.	209.	AG	1600.	11.5	.0	44.0			
14. 14 Dixie SB Appr	* 264351.0	276234.0	264252.0	275994.0	*	260.	202.	AG	1600.	11.5	.0	44.0			
15. 15 Dixie SB QTRUNC	* 264276.0	276054.0	264351.0	276234.0	*	195.	23.	AG	197.	100.0	.0	24.0			
16. 16 Dixie SB QTRUNC	* 264351.0	276234.0	264365.0	276261.0	*	30.	27.	AG	197.	100.0	.0	24.0			
17. 17 Dixie SB @ Kyles	* 264252.0	275994.0	264236.0	275956.0	*	41.	203.	AG	965.	11.5	.0	40.0			
18. 18 Dixie SB Depart	* 264236.0	275956.0	264179.0	275824.0	*	144.	203.	AG	1345.	11.5	.0	44.0			
19. 19 Dixie SB Depart	* 264179.0	275824.0	264143.0	275732.0	*	99.	201.	AG	1345.	11.5	.0	44.0			
20. 20 Dixie SB Depart	* 264143.0	275732.0	264083.0	275564.0	*	178.	200.	AG	1345.	11.5	.0	44.0			
21. 21 Dixie NB Rt.	* 264240.0	275916.0	264284.0	275929.0	*	46.	74.	AG	310.	11.5	.0	32.0			
22. 22 Kyles EB @ Dixie	* 264252.0	275994.0	264284.0	275929.0	*	72.	154.	AG	650.	11.5	.0	32.0			

23.	23	Kyles	EB Depart	* 264284.0	275929.0	264483.0	275522.0	*	453.	154.	AG	960.	11.5	.0	44.0
24.	24	Kyles	WB Appr	* 264516.0	275540.0	264468.0	275639.0	*	110.	334.	AG	1240.	11.5	.0	56.0
25.	25	Kyles	WB Appr	* 264468.0	275639.0	264359.0	275852.0	*	239.	333.	AG	1240.	11.5	.0	56.0
26.	26	Kyles	WB Rt.	* 264359.0	275852.0	264347.0	275900.0	*	49.	346.	AG	830.	11.5	.0	32.0
27.	27	Kyles	WB Rt.	* 264347.0	275900.0	264300.0	276003.0	*	113.	335.	AG	830.	11.5	.0	32.0
28.	28	Kyles	WB Rt. Qu*	264313.0	275975.0	265453.3	273432.6	*	2786.	156.	AG	116.	100.0	.0	12.0 1.40 141.6
29.	29	Kyles	WB Rt. @ D*	264300.0	276003.0	264303.0	276071.0	*	68.	3.	AG	830.	11.5	.0	32.0
30.	30	Kyles	WB Appr	* 264359.0	275852.0	264296.0	275980.0	*	143.	334.	AG	30.	11.5	.0	32.0
31.	31	WB Kyles L*	264307.0	275957.0	264311.3	275948.3	*	10.	154.	AG	116.	100.0	.0	12.0 .04 .5	
32.	32	Kyles	WB @ Dixie*	264296.0	275980.0	264280.0	276013.0	*	37.	334.	AG	15.	11.5	.0	32.0
33.	33	Kyles	WB Lt.	* 264296.0	275980.0	264252.0	275994.0	*	46.	288.	AG	15.	11.5	.0	32.0
34.	34	Kyles	WB Lt.	* 264359.0	275852.0	264325.0	275892.0	*	53.	320.	AG	380.	11.5	.0	32.0
35.	35	Kyles	WB Lt.	* 264325.0	275892.0	264287.0	275965.0	*	82.	333.	AG	380.	11.5	.0	32.0
36.	36	Kyles	WB Lt. Que*	264295.0	275951.0	264350.2	275838.5	*	125.	154.	AG	116.	100.0	.0	12.0 .76 6.4
37.	37	Kyles	WB Lt. @ D*	264287.0	275965.0	264236.0	275956.0	*	52.	260.	AG	380.	11.5	.0	32.0

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JOB: Brent Spence Bridge T1altlpm.dat RUN: Kyles Lane & Dixie Hwy-Trunc
DATE: 08/31/2010 TIME: 08:03:18.51

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	* CYCLE	RED	CLEARANCE	APPROACH	SATURATION	IDLE	SIGNAL	ARRIVAL
* LENGTH	TIME	LOST TIME	VOL	FLOW RATE	EM FAC	TYPE	RATE	
* (SEC)	(SEC)	(SEC)	(VPH)	(VPH)	(gm/hr)			
4. 04 Dixie NB Queue *	100	75	2.0	760	1511	73.30	1	3
28. 28 Kyles WB Rt. Qu*	100	59	2.0	830	1599	73.30	1	3
31. 31 WB Kyles L*	100	59	2.0	30	1881	73.30	1	3
36. 36 Kyles WB Lt. Que*	100	59	2.0	380	1357	73.30	1	3

RECEPTOR LOCATIONS

RECEPTOR	* COORDINATES (FT)	* Z
	* X Y	
1. R1 SB Mid	* 264384.0 276323.0	5.0 *
2. R2 SB 164	* 264321.0 276211.0	5.0 *
3. R3 SB 82	* 264290.0 276136.0	5.0 *
4. R4 SB Corner	* 264262.0 276069.0	5.0 *
5. R5 SB Corner	* 264230.0 275990.0	5.0 *
6. R6 SB 82	* 264193.0 275900.0	5.0 *
7. R7 SB 164	* 264151.0 275798.0	5.0 *
8. R8 SB Mid	* 264103.0 275678.0	5.0 *
9. R9 NB Mid	* 264155.0 275655.0	5.0 *
10. R10 NB 164	* 264184.0 275729.0	5.0 *
11. R11 NB 82	* 264215.0 275805.0	5.0 *
12. R12 NB Corner	* 264242.0 275872.0	5.0 *
13. R13 EB Corner	* 264272.0 275903.0	5.0 *
14. R14 EB 82	* 264340.0 275765.0	5.0 *
15. R15 EB 164	* 264378.0 275678.0	5.0 *
16. R16 EB Mid	* 264408.0 275600.0	5.0 *
17. R17 WB Mid	* 264455.0 275722.0	5.0 *
18. R18 WB 164	* 264399.0 275833.0	5.0 *
19. R19 WB 82	* 264362.0 275906.0	5.0 *
20. R20 WB Corner	* 264330.0 275971.0	5.0 *
21. R21 NB Corner	* 264319.0 276046.0	5.0 *
22. R22 NB 82	* 264343.0 276114.0	5.0 *
23. R23 NB 164	* 264376.0 276189.0	5.0 *
24. R24 NB Mid	* 264447.0 276280.0	5.0 *

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JOB: Brent Spence Bridge T1altlpm.dat RUN: Kyles Lane & Dixie Hwy-Trunc

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)	(DEGR)* REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* .1	.1	.2	.3	.2	.3	.2	2.3	2.4	2.0	1.3	1.6	1.3	1.2	.9	.1	.2	.4	.9	
5.	* .1	.3	.4	.4	.4	.3	.3	2.3	2.3	2.1	1.3	1.5	1.4	1.0	.9	.1	.0	.4	.7	
10.	* .1	.3	.6	.6	.5	.6	.6	2.2	2.2	2.0	1.3	1.5	1.3	1.0	.9	.1	.0	.1	.7	
15.	* .2	.7	.8	1.0	1.0	.9	.8	1.0	2.2	1.9	1.8	1.2	1.6	1.1	.9	.9	.1	.0	.0	.5
20.	* .2	.9	1.4	1.4	1.2	1.1	1.2	1.3	1.8	1.7	1.5	1.2	1.3	1.0	.9	.9	.1	.0	.0	.3
25.	* .4	1.1	1.7	2.0	1.4	1.3	1.5	1.6	1.4	1.4	1.3	1.1	1.2	.9	.9	.7	.1	.0	.0	.0
30.	* .5	1.6	2.1	2.2	1.5	1.4	1.6	1.9	1.1	1.0	.9	1.0	1.2	.9	.8	.7	.0	.0	.0	.0
35.	* .7	1.9	2.4	2.4	1.7	1.4	1.7	1.9	.7	.7	.8	.9	.8	.8	.8	.7	.0	.0	.0	.0
40.	* .8	2.1	2.7	2.6	1.6	1.4	1.5	2.0	.5	.5	.6	.9	.8	.7	.6	.0	.0	.0	.0	.0
45.	* .9	2.3	2.5	2.3	1.6	1.3	1.8	2.0	.5	.5	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
50.	* 1.0	2.2	2.4	2.2	1.4	1.3	1.8	1.9	.4	.3	.5	.7	.9	.8	.7	.7	.0	.0	.0	.0
55.	* 1.2	2.2	2.1	2.1	1.3	1.3	2.0	1.9	.4	.4	.4	.7	1.0	.8	.8	.6	.0	.0	.0	.0
60.	* 1.2	2.3	2.1	2.0	1.3	1.1	2.0	2.0	.4	.3	.3	.6	1.0	.8	.8	.7	.0	.0	.0	.0
65.	* 1.3	2.2	1.9	1.9	1.1	1.3	2.0	1.9	.4	.3	.4	.5	1.0	.8	.8	.7	.0	.0	.0	.0
70.	* 1.4	1.9	1.8	1.7	1.1	1.3	1.7	1.8	.3	.3	.4	.5	.9	.8	.8	.7	.0	.0	.0	.0
75.	* 1.3	1.8	1.8	1.8	1.0	1.3	1.9	1.8	.3	.3	.3	.6	.9	.8	.7	.6	.0	.0	.0	.0
80.	* 1.2	1.8	1.8	1.9	.9	1.3	1.7	1.7	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
85.	* 1.1	1.7	1.6	1.6	1.0	1.2	1.7	1.6	.3	.3	.3	.5	.9	.8	.7	.7	.0	.0	.0	.0
90.	* 1.1	1.6	1.6	1.6	1.0	1.1	1.6	1.6	.3	.3	.3	.6	1.0	.8	.7	.7	.0	.0	.0	.0

95. *	1.1	1.6	1.6	1.5	1.1	1.2	1.6	1.6	.3	.3	.4	.6	1.0	.8	.8	.7	.0	.0	.0	.0
100. *	1.0	1.7	1.6	1.6	1.0	1.4	1.6	1.5	.2	.3	.4	.6	1.0	.8	.9	.7	.1	.0	.0	.0
105. *	1.0	1.6	1.6	1.6	1.2	1.5	1.6	1.5	.2	.3	.5	.5	1.1	.9	.9	.7	.1	.1	.0	.0
110. *	.9	1.6	1.6	1.5	1.2	1.5	1.6	1.5	.2	.4	.5	.6	1.1	.9	.9	.8	.1	.1	.0	.1
115. *	.9	1.6	1.6	1.5	1.3	1.5	1.6	1.4	.1	.3	.4	.5	1.2	1.0	.9	.8	.1	.1	.0	.1
120. *	.9	1.6	1.6	1.4	1.4	1.6	1.6	1.4	.1	.2	.4	.5	1.3	1.0	1.0	.7	.1	.1	.0	.1
125. *	.9	1.6	1.6	1.4	1.6	1.7	1.5	1.4	.1	.2	.3	.6	1.1	1.1	1.0	.6	.1	.1	.0	.1
130. *	.9	1.6	1.6	1.4	1.7	1.7	1.5	1.4	.1	.1	.3	.6	1.1	1.2	1.0	.6	.1	.1	.0	.1
135. *	.9	1.6	1.6	1.4	1.7	1.7	1.4	1.4	.1	.1	.2	.5	1.2	1.1	.9	.6	.1	.2	.2	.2
140. *	1.0	1.6	1.6	1.5	1.8	1.6	1.5	1.4	.1	.2	.5	1.1	1.1	.8	.4	.4	.3	.2	.4	.4
145. *	.9	1.8	1.9	1.7	1.7	1.7	1.6	1.6	.1	.1	.2	.5	1.0	1.0	.7	.4	.4	.5	.5	.5
150. *	1.0	1.9	2.1	1.7	1.6	1.7	1.6	1.5	.1	.1	.1	.2	1.0	.9	.7	.3	.6	.9	.8	1.1
155. *	1.1	1.9	2.3	2.0	1.7	1.6	1.5	1.5	.1	.0	.1	.2	.8	.8	.5	.3	.9	1.0	1.0	1.3
160. *	1.1	2.2	2.4	1.9	1.6	1.6	1.7	1.7	.1	.0	.0	.2	.6	.5	.3	.2	1.0	1.2	1.4	1.5
165. *	1.3	2.4	2.5	2.0	1.2	1.8	1.9	1.7	.1	.0	.0	.1	.4	.4	.2	.1	1.1	1.3	1.3	1.6
170. *	1.3	2.5	2.8	1.9	1.2	1.9	1.9	1.7	.1	.0	.1	.1	.2	.2	.1	.0	1.2	1.4	1.4	1.6
175. *	1.9	2.4	2.6	1.8	1.2	1.9	2.0	1.7	.2	.2	.2	.2	.1	.1	.1	.0	1.3	1.2	1.4	1.7
180. *	1.7	2.5	2.4	1.6	1.3	2.2	2.1	1.7	.2	.2	.2	.2	.1	.1	.0	.0	1.1	1.2	1.5	1.8
185. *	2.1	2.6	2.5	1.6	1.6	2.2	2.1	1.8	.4	.4	.4	.4	.2	.1	.0	.0	1.1	1.3	1.4	1.7
190. *	2.2	2.6	2.3	1.7	1.7	2.1	2.0	1.6	.6	.8	.9	.8	.2	.1	.0	.0	1.1	1.1	1.4	1.5
195. *	2.2	2.3	2.1	1.8	1.6	2.0	1.8	1.4	1.1	1.2	1.1	1.3	.4	.0	.0	.0	1.0	1.0	1.4	1.5
200. *	2.2	2.0	1.6	1.7	1.5	1.8	1.5	1.3	1.4	1.6	1.5	1.7	.9	.1	.0	.0	1.0	1.0	1.4	1.6
205. *	2.0	1.6	1.4	1.3	1.4	1.5	1.4	.9	1.8	2.0	2.0	2.0	1.2	.1	.0	.0	1.0	1.1	1.4	1.8

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WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

210. *	1.6	1.3	1.1	.8	.9	.9	1.0	.6	2.0	2.2	2.1	2.3	1.5	.2	.1	.0	1.0	1.1	1.4	2.2
215. *	1.5	.8	.7	.5	.5	.7	.6	.4	2.1	2.4	2.4	2.4	1.6	.2	.1	.1	.9	1.2	1.5	2.3
220. *	.9	.4	.5	.4	.3	.5	.4	.3	2.3	2.4	2.5	2.5	1.5	.3	.2	.1	.9	1.1	1.6	2.0
225. *	.7	.3	.2	.2	.2	.2	.2	.1	2.2	2.3	2.4	2.4	1.5	.4	.2	.1	1.0	1.3	1.8	2.0
230. *	.4	.2	.2	.1	.1	.2	.2	.1	2.1	2.1	2.3	2.4	1.3	.5	.2	.2	1.0	1.3	1.8	1.8
235. *	.3	.1	.1	.1	.0	.1	.1	.1	2.0	2.0	2.1	2.2	1.4	.5	.2	.2	1.1	1.4	1.7	1.7
240. *	.1	.1	.1	.1	.0	.1	.1	.1	2.1	2.0	2.0	2.1	1.3	.5	.2	.2	1.1	1.4	1.7	1.6
245. *	.1	.1	.1	.1	.0	.1	.1	.1	1.9	1.8	1.8	2.0	1.1	.5	.3	.2	1.1	1.5	1.8	1.6
250. *	.1	.1	.1	.1	.0	.1	.1	.1	1.8	1.9	1.8	1.9	1.0	.5	.3	.2	1.2	1.5	1.9	1.5
255. *	.1	.1	.1	.1	.0	.1	.1	.1	1.7	1.8	1.7	1.7	.9	.6	.4	.2	1.1	1.3	1.5	1.3
260. *	.1	.1	.1	.1	.0	.1	.1	.1	1.7	1.8	1.7	1.7	.7	.6	.4	.2	1.1	1.3	1.6	1.2
265. *	.1	.1	.1	.1	.0	.1	.1	.0	1.6	1.7	1.7	1.7	.6	.6	.4	.3	1.1	1.3	1.6	1.1
270. *	.1	.0	.0	.0	.0	.1	.1	.0	1.6	1.6	1.5	1.6	.6	.5	.4	.3	1.2	1.5	1.5	1.1
275. *	.1	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.6	.7	.5	.3	.4	1.2	1.4	1.5	1.0
280. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.5	.3	.4	1.2	1.4	1.3	1.0
285. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.7	.6	.4	.3	1.3	1.4	1.3	1.0
290. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.6	.3	.3	1.2	1.6	1.4	1.1
295. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.6	.6	.5	.3	.3	1.3	1.5	1.6	.8
300. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.5	.6	.5	.3	.3	1.3	1.3	1.5	.8
305. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.5	1.4	.6	.5	.4	.3	1.3	1.3	1.4	1.0
310. *	.0	.0	.0	.0	.0	.0	.0	.0	1.6	1.6	1.6	1.3	.5	.5	.4	.3	1.3	1.3	1.3	1.1
315. *	.0	.0	.0	.0	.0	.1	.0	1.6	1.6	1.6	1.2	.5	.5	.4	.2	1.3	1.3	1.3	1.0	.9
320. *	.0	.1	.1	.1	.0	.1	.1	1.6	1.7	1.7	1.2	.6	.5	.3	.3	1.2	1.1	1.0	.9	.9
325. *	.0	.1	.1	.1	.0	.1	.1	1.7	1.7	1.7	1.1	.8	.6	.4	.3	1.2	1.0	1.0	1.0	1.0
330. *	.0	.1	.1	.1	.0	.1	.1	1.7	1.7	1.7	1.0	.9	.5	.5	.4	1.0	.9	1.0	1.2	1.2
335. *	.1	.1	.1	.1	.0	.1	.1	1.9	1.8	1.8	1.0	.9	.7	.7	.5	.9	.9	1.0	1.2	1.2
340. *	.1	.1	.1	.1	.0	.1	.1	2.0	2.0	1.8	1.0	.9	.7	.9	.6	.6	.8	.9	1.1	1.1
345. *	.1	.1	.1	.1	.0	.1	.1	2.1	2.1	1.8	1.2	1.1	1.0	1.0	.8	.5	.6	.9	1.1	1.1
350. *	.1	.1	.1	.1	.1	.1	.1	2.2	2.1	1.9	1.1	1.1	1.1	1.1	.9	.4	.4	.7	1.0	1.0
355. *	.1	.1	.2	.2	.1	.1	.3	.1	2.4	2.3	2.0	1.1	1.4	1.3	1.1	1.0	.1	.4	.5	.9
360. *	.1	.1	.2	.3	.2	.2	.3	.2	2.3	2.4	2.0	1.3	1.6	1.3	1.2	.9	.1	.2	.4	.9

MAX * 2.2 2.6 2.8 2.6 1.8 2.2 2.1 2.0 2.4 2.4 2.5 2.5 1.6 1.4 1.2 1.0 1.3 1.6 1.9 2.3
 DEGR. * 190 185 170 40 140 180 180 40 355 215 220 220 0 5 0 355 315 290 250 215

1

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (PPM)

(DEGR)* REC21 REC22 REC23 REC24

0. *	1.6	1.7	1.3	.9
5. *	1.7	1.7	1.3	.9
10. *	1.6	1.5	1.3	.8
15. *	1.4	1.5	1.3	.8
20. *	1.1	1.4	1.1	.7
25. *	.7	1.2	1.1	.7
30. *	.4	.8	.7	.5
35. *	.2	.4	.7	.5
40. *	.1	.4	.5	.4
45. *	.0	.1	.3	.2
50. *	.0	.1	.2	.1
55. *	.0	.1	.1	.1
60. *	.0	.1	.0	.0

65. * .0 .1 .0 .0
70. * .0 .1 .0 .0
75. * .0 .1 .0 .0
80. * .0 .0 .0 .0
85. * .0 .0 .0 .0
90. * .0 .0 .0 .0
95. * .0 .0 .0 .0
100. * .0 .0 .0 .0
105. * .0 .0 .0 .0
110. * .0 .0 .0 .0
115. * .0 .0 .0 .0
120. * .0 .0 .0 .0
125. * .0 .0 .0 .0
130. * .0 .0 .0 .0
135. * .0 .0 .0 .0
140. * .0 .0 .0 .0
145. * .2 .0 .0 .0
150. * .3 .2 .0 .0
155. * .5 .3 .2 .0
160. * .6 .5 .2 .1
165. * .9 .5 .3 .1
170. * 1.0 .5 .4 .1
175. * .9 .6 .4 .1
180. * 1.0 .6 .4 .3
185. * .9 .8 .6 .3
190. * .9 .9 .6 .4
195. * 1.4 1.1 .8 .3
200. * 1.5 1.3 1.1 .5
205. * 1.6 1.4 1.4 .6

1

JOB: Brent Spence Bridge T1altlpm.dat

RUN: Kyles Lane & Dixie Hwy-Trunc

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24

210. * 1.8 1.5 1.6 .7
215. * 1.7 1.5 1.7 .9
220. * 1.5 1.7 1.8 1.0
225. * 1.2 1.6 1.8 1.2
230. * 1.3 1.5 1.7 1.3
235. * 1.3 1.6 1.7 1.2
240. * 1.2 1.6 1.7 1.2
245. * .9 1.5 1.6 1.3
250. * 1.0 1.4 1.5 1.0
255. * 1.0 1.4 1.4 1.2
260. * 1.0 1.4 1.4 1.1
265. * 1.1 1.4 1.4 .9
270. * 1.1 1.4 1.4 1.0
275. * 1.1 1.4 1.4 .9
280. * 1.1 1.4 1.4 .9
285. * 1.2 1.4 1.4 .9
290. * 1.3 1.4 1.4 .8
295. * 1.3 1.4 1.4 .7
300. * 1.3 1.4 1.5 .8
305. * 1.5 1.4 1.3 .8
310. * 1.4 1.4 1.3 .9
315. * 1.4 1.4 1.4 .9
320. * 1.5 1.4 1.4 .8
325. * 1.5 1.4 1.5 .8
330. * 1.5 1.5 1.4 .8
335. * 1.5 1.5 1.4 .8
340. * 1.6 1.5 1.4 .9
345. * 1.6 1.5 1.4 .9
350. * 1.7 1.7 1.4 .8
355. * 1.7 1.9 1.4 .9
360. * 1.6 1.7 1.3 .9

MAX * 1.8 1.9 1.8 1.3
DEGR. * 210 355 225 230

THE HIGHEST CONCENTRATION IS 2.80 PPM AT 170 DEGREES FROM REC3 .
THE 2ND HIGHEST CONCENTRATION IS 2.60 PPM AT 40 DEGREES FROM REC4 .
THE 3RD HIGHEST CONCENTRATION IS 2.60 PPM AT 185 DEGREES FROM REC2 .

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JOB: Brent Spence Bridge T1altlpm.dat
DATE: 08/31/2010 TIME: 08:03:18.51

RUN: Kyles Lane & Dixie Hwy-Trunc

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
* ANGLE (DEGREES)
* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18
REC19 REC20
LINK # * 190 185 170 40 140 180 180 40 355 215 220 220 0 5 0 355 315 290 250 215

1 * .0 .0 .0 .0 .0 .0 .2 .1 .4 .4 .1 .1 .0 .0 .0 .0 .0 .0 .0 .0
2 * .0 .0 .0 .0 .0 .1 .1 .1 .1 .1 .4 .1 .0 .0 .0 .0 .0 .0 .0 .0
3 * .0 .0 .0 .0 .0 .2 .0 .1 .0 .0 .3 .0 .0 .0 .0 .0 .0 .1 .1 .1
4 * .1 .1 .0 .0 .0 .9 .9 .7 1.3 1.5 1.5 .0 .0 .0 .0 .0 .1 .3 .5
5 * .0 .0 .0 .0 .2 .0 .0 .0 .0 .0 .2 .0 .0 .0 .0 .0 .0 .0 .0 .0
6 * .0 .0 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

7 *	.2	.4	.3	.4	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.0	.0
8 *	.3	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12 *	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13 *	.4	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14 *	.3	1.0	.9	1.0	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.0	.0	.0	.0
15 *	.2	.8	.8	.9	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.0
16 *	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17 *	.0	.0	.0	.0	.4	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0
18 *	.0	.0	.0	.0	.1	.7	.0	.1	.1	.0	.0	.2	.0	.0	.0	.0	.1	.1	.1	.1
19 *	.0	.0	.0	.0	.2	.6	.2	.2	.0	.3	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1
20 *	.0	.0	.0	.0	.1	.3	.6	.3	.4	.2	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1
21 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
22 *	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0
23 *	.1	.1	.1	.0	.3	.0	.0	.1	.0	.0	.0	.2	.5	.5	.4	.2	.2	.2	.2	.2
24 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.0	.2	.3	.3	.6	.4	.0	.0	.0
26 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.1	.2	.0	.0
27 *	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.4	.4
28 *	.0	.1	.2	.0	.2	.0	.0	.0	.0	.0	.0	.1	.2	.2	.3	.3	.3	.3	.4	.4
29 *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0
30 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
32 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
34 *	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0
35 *	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1
36 *	.0	.0	.1	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.1	.2	.2	.2	.2	.2
37 *	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0

1

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RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

* CO/LINK (PPM)
 * ANGLE (DEGREES)
 * REC21 REC22 REC23 REC24
 LINK # * 210 355 225 230

1 *	.0	.0	.0	.0
2 *	.0	.0	.0	.0
3 *	.1	.0	.0	.0
4 *	.4	.0	.1	.0
5 *	.1	.0	.0	.0
6 *	.1	.0	.0	.0
7 *	.0	.7	.7	.2
8 *	.0	.1	.0	.3
9 *	.0	.0	.0	.1
10 *	.0	.0	.0	.0
11 *	.0	.0	.0	.0
12 *	.0	.0	.0	.0
13 *	.0	.1	.0	.1
14 *	.1	.5	.6	.3
15 *	.0	.4	.4	.2
16 *	.0	.1	.0	.1
17 *	.1	.0	.0	.0
18 *	.2	.0	.0	.0
19 *	.1	.0	.0	.0
20 *	.1	.0	.0	.0
21 *	.0	.0	.0	.0
22 *	.1	.0	.0	.0
23 *	.0	.0	.0	.0
24 *	.0	.0	.0	.0
25 *	.0	.0	.0	.0
26 *	.0	.0	.0	.0
27 *	.1	.0	.0	.0
28 *	.0	.0	.0	.0
29 *	.3	.0	.0	.0
30 *	.0	.0	.0	.0
31 *	.0	.0	.0	.0
32 *	.0	.0	.0	.0
33 *	.0	.0	.0	.0
34 *	.0	.0	.0	.0
35 *	.0	.0	.0	.0
36 *	.0	.0	.0	.0
37 *	.0	.0	.0	.0